



OC DANA POINT HARBOR REVITALIZATION PROJECT

HYDROLOGY AND HYDRAULIC REPORT LINE LOOP01

City of Dana Point
County of Orange, California

Prepared For:

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Dana Point, CA 92629*

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Date Prepared: May 3, 2013
Job Number: 307-008-01



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1.0 INTRODUCTION

1.1 INTRODUCTION AND PURPOSE

This drainage study provides analysis to establish runoff discharge rates for Line LOOP01, a significant storm drain collection system in the center of the City of Dana Point, and to determine if the Line LOOP01 storm drain has available hydraulic capacity to continue to receive and convey runoff from tributary areas originating within the Orange County Dana Point Harbor project boundary (Harbor). The Harbor is currently planning major renovations within its commercial core area south of Dana Point Harbor Drive (formerly Del Obispo Street), west of Puerto Place, and east of Casitas Place. Land use characteristics of the renovation will be similar to those in the existing condition. Line LOOP01 originates approximately one mile upstream of the Harbor and captures 234 acres of tributary within the City of Dana Point before entering the Harbor, capturing an additional 4.5 acres of Harbor tributary and outletting through a sea wall into the Dana Point Harbor marina. Refer to Figure 1 for the alignment and tributary boundary of Line LOOP01. The portion of Line LOOP01 storm drain which resides within the harbor was constructed circa 1968 when the original harbor construction was undertaken and has historically received and conveyed runoff from tributaries within the Harbor project limits. With the planned renovations, the Harbor will continue to send runoff to the existing LOOP01 storm drain.

1.2 BACKGROUND

The Line LOOP01 storm drain was originally constructed circa 1968 as part of the original Dana Point Harbor grading and infrastructure construction and extended 900-feet between its sea wall outlet into the Dana Point Harbor marina and Dana Point Harbor Drive (formerly Del Obispo Street). The storm drain is a 60" RCP through the Harbor except for a short 25-foot transition to an RC Box at the sea wall outlet. Line LOOP01 storm drain originally terminated just north of Dana Point Harbor Drive as a basin impoundment created by the fill construction for Dana Point Harbor Drive (see Exhibit 1 in Appendix A). At the time of construction, areas upstream of the basin impoundment between Dana Point Harbor Drive and Pacific Coast Highway were open space and areas north of Pacific Coast Highway were moderately populated. Research for this report did not produce a hydrology report for the original harbor grading and infrastructure construction and discharge values or a hydraulic grade line does not appear on the as-built drawings.

On-site improvements were made in the Harbor soon after the original grading and infrastructure improvements (including the 60" RCP) were completed. On-site improvements in the vicinity of Line LOOP01 included building structures housing retail space and Harbor services as well as paved parking lots. Research for this report did not produce as-built drawings for the on-site Harbor improvements. However, because surface evidence indicates inlet locations in the parking lot near the alignment of the 60" RCP, camera probe work was performed to determine if the inlets connect to Line LOOP01. The results of the camera probe work indicate five inlets and three connection pipes join the 60" RCP storm drain and drain an on-site

tributary of 4.5 acres. The inlets, connector pipes, and their respective tributary areas are shown on Figure 2. It should be noted that the City of Dana Point Master Plan of Drainage (refer to Appendix A-Exhibit 2-Sheet 8) does not indicate the presence of on-site Harbor tributary connections to Line LOOP01, and the City of Dana Point Storm Drain Atlas (refer to Appendix A-Exhibit 3-Sheet D9) indicates the presence of two inlets and one connector pipe connection to Line LOOP01.

Between the mid 1970's and late 1980's areas to the north of the Harbor were built out and Line LOOP01 was extended north from Dana Point Harbor Drive to Selva Road capturing 100 percent of the present day hydrologic boundary. Refer to Appendix A-Exhibits 4 and 5 for Line LOOP01 mainline extension as-built drawings. This off-site tributary (upstream of the Harbor) covers 233.6 acres and mainline LOOP01 pipe sizes range between 33-inches and 66-inches. Hydrologic information for off-site LOOP01 was unavailable although hydraulic data tables presented on Exhibit 4 indicate the segment of LOOP01 between Dana Point Harbor Drive and Pacific Coast Highway was originally designed to convey a 10-year storm event.

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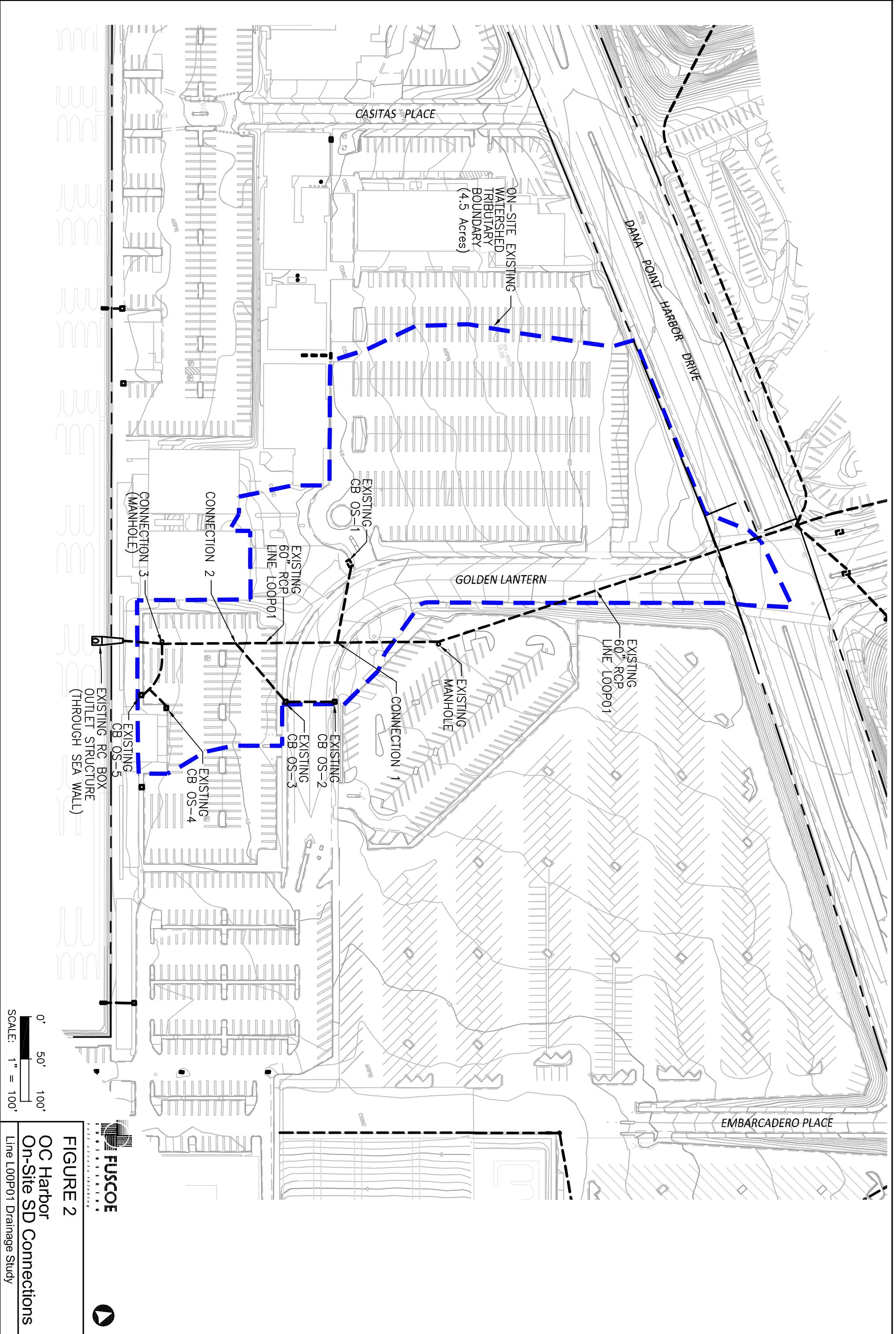


FIGURE 2

**OC Harbor
On-Site SD Connections**

Line L00P01 Drainage Study

2.0 HYDROLOGIC ASSESSMENT

2.1 ANALYSIS FRAMEWORK

A hydrologic analysis has been prepared for Line LOOP01 existing and proposed conditions utilizing the methodology described in the Orange County Hydrology Manual, October, 1986 (Hydrology Manual) and methods accepted by the Orange County Public Works/Flood Division. Three separate models have been prepared for the two conditions (existing and proposed). Model 1 studies existing condition runoff and assumes no inclusion of tributary from Dana Point Harbor on-site areas (consistent with the City of Dana Point Master Plan of Drainage document, Appendix A-Exhibit 2). Model 2 also studies existing condition runoff but provides for 4.5 acres of Harbor on-site tributary area contributing to the system. This model is the baseline condition model. Model 3 studies proposed condition runoff and assumes no changes to development conditions north of Dana Point Harbor Drive while providing for planned Dana Point Harbor on-site renovation conditions. Proposed condition modeling was based on the Orange County Harbor Revitalization site plan shown on Figure 3. The analysis used in this study is based on the storm frequency of a ten-year high confidence event as specified in the Orange County Local Drainage Manual.

2.2 METHODOLOGY

The hydrologic study limits consist of an area entirely within the incorporated City limits of Dana Point and encompasses a range of tributary acreage between 233.6 acres and 238.1 acres depending on the model. Watershed drainage areas and drainage patterns were defined based upon a review of the City of Dana Point Master Plan of Drainage document and Storm Drain Atlas document, electronic contour mapping obtained from Intermap Technologies, Inc., an on-line vendor, and a field reconnaissance survey. A comprehensive inventory of existing drainage facilities was prepared through a review of record drawings from the City of Dana Point and the County of Orange. A proposed storm drain facility planned for the "Town Center Pacific Coast Highway and Del Prado Streetscape Improvement Project" was also integrated into the models. This storm drain will replace an existing facility which currently traverses private property east of Street of the Golden Lantern and north and south of Pacific Coast Highway. Surface flow conveyance data was derived by takeoff from the electronic contour mapping. Pipe flow conveyance data was taken directly from storm drain as-built drawings for Line LOOP01 (see Appendix A-Exhibits 4 and 5). Data on land use was taken from a review of the City of Dana Point Land Use Map, November, 1993 and Zoning Map June, 2008 (refer to Appendix A-Exhibits 6 and 7). Where the two documents were in conflict or were non-specific, a review of aerial photography was utilized to determine the land use. Figure 4, Existing Land Use Map, summarizes the existing land use factors used in the hydrologic models. Land use factors used in the proposed condition model were identical to the existing condition, including the use of a "commercial" factor for all on-site areas in the Harbor south of Dana Point Harbor Drive. Soil Type D conforming to the soil classifications published in the Hydrology Manual were used throughout the watershed. Soil Type D is the most conservative of the four soil groups listed in the Hydrology Manual and has high runoff potential characteristics (slow infiltration rates).

The rational hydrologic method, conforming to the 1986 Orange County Hydrology Manual, was used in this study investigation. This method and the data and criteria it incorporates, is consistent with accepted methods of analyzing storm water runoff in Orange County. The rational method is used when drainage areas are less than 640 acres (one square mile). The rational method relates rainfall intensity, the ratio of runoff to rainfall expressed as a runoff coefficient, and the drainage area size to the peak runoff. Rational method hydrologic computations were made using computer analysis techniques of the RATSCx program by Advanced Engineering Software, Version 19.0, June, 2012.

2.3 HYDROLOGIC RESULTS

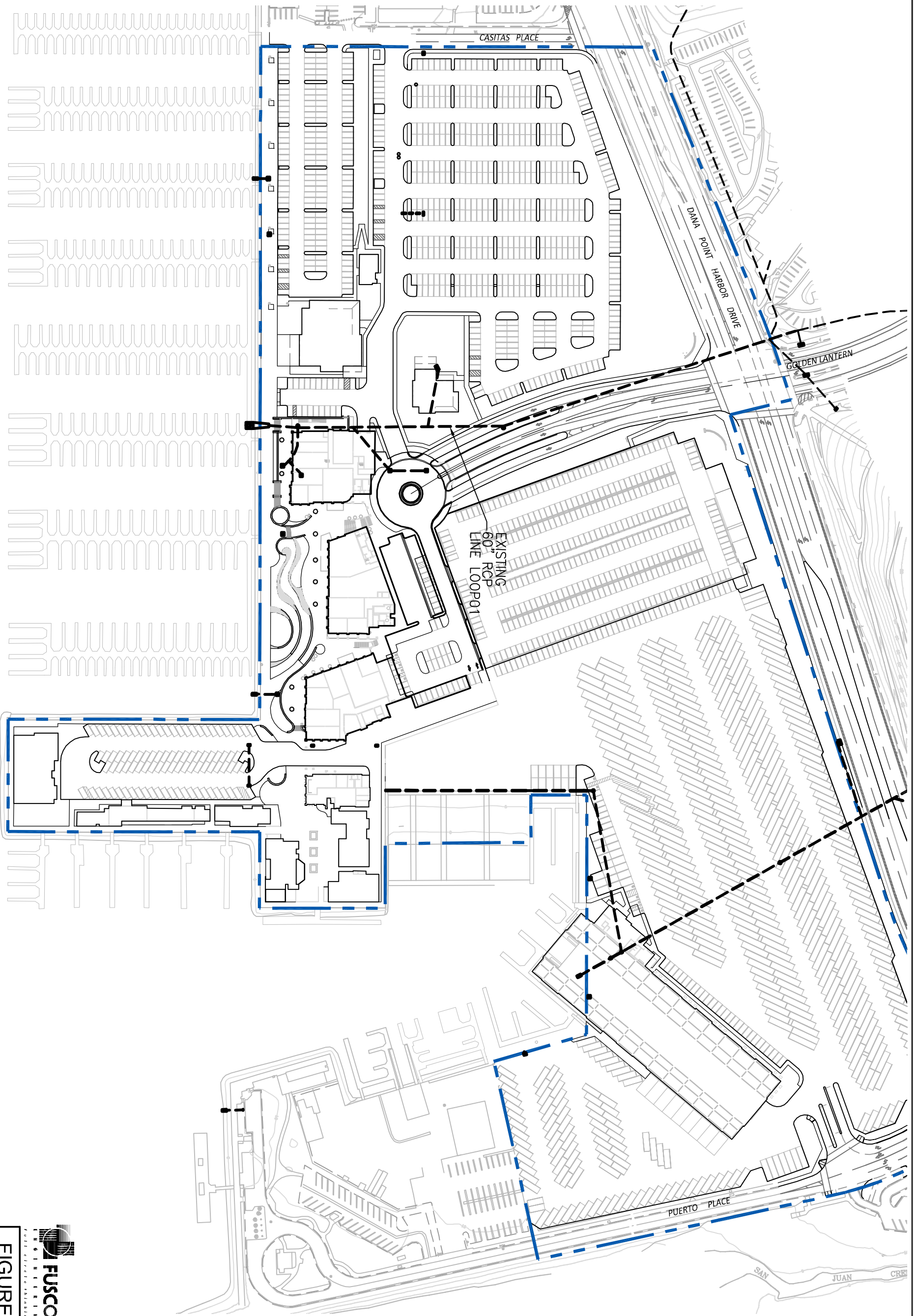
Watershed hydrology calculations for a 10-year high confidence storm event have been prepared for two existing condition models and one proposed condition model utilizing the methodologies and variables described in Sections 2.1 and 2.2. All three models have identical watershed characteristic upstream of hydrologic Node 191 located at the intersection of Dana Point Harbor Drive and Street of the Golden Lantern and variable watershed characteristics downstream of Node 191. Refer to the study hydrology maps for significant hydrologic model locations in the watershed. Existing condition (w/o Harbor) hydrology calculations and hydrology maps can be found in Appendices B.1 and C.1, respectively. Existing condition (w/Harbor) hydrology calculations and hydrology maps can be found in Appendices B.2 and C.2, respectively. Proposed condition (w/Harbor) hydrology calculations and hydrology maps can be found in Appendices B.3 and C.3, respectively. Table 2.1 summarizes the hydrologic results at Nodes 191 and 214 (Dana Point Harbor Marina) for all three models.

Table 2.1: Watershed Hydrologic Summary

Model No.	Model Description	Tributary Area at Node 191 ⁽¹⁾ (acres)	Discharge at Node 191 (cfs)	Tributary Area at Node 214 ⁽²⁾ (acres)	Discharge at Node 214 (cfs)
1	Existing 10-year minus harbor tributary	233.6	401.3	233.6	401.3
2	Existing 10-year with harbor tributary	233.6	401.3	238.1	410.5
3	Proposed 10-year with harbor tributary	233.6	401.3	237.1	408.4

(1) Intersection of Dana Point Harbor Drive and Street of the Golden Lantern.

(2) Outlet into Marina.

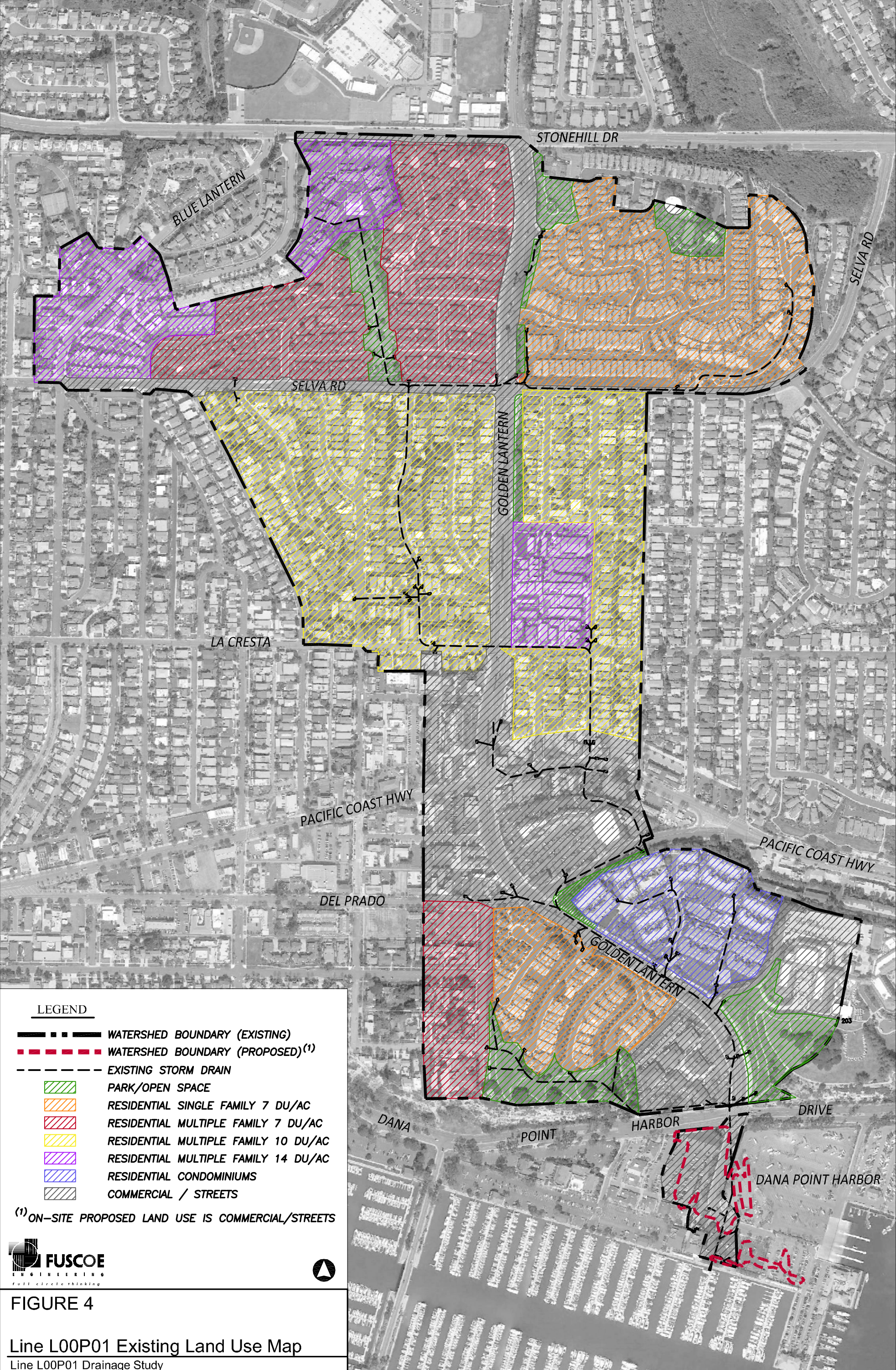


0' 75' 150'
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FIGURE 3
OC Harbor Revitalization
Site Plan
Line L00P01 Drainage Study

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LEGEND

-  WATERSHED BOUNDARY (EXISTING)
-  WATERSHED BOUNDARY (PROPOSED)⁽¹⁾
-  EXISTING STORM DRAIN
-  PARK/OPEN SPACE
-  RESIDENTIAL SINGLE FAMILY 7 DU/AC
-  RESIDENTIAL MULTIPLE FAMILY 7 DU/AC
-  RESIDENTIAL MULTIPLE FAMILY 10 DU/AC
-  RESIDENTIAL MULTIPLE FAMILY 14 DU/AC
-  RESIDENTIAL CONDOMINIUMS
-  COMMERCIAL / STREETS

⁽¹⁾ ON-SITE PROPOSED LAND USE IS COMMERCIAL/STREETS



FIGURE 4

Line L00P01 Existing Land Use Map
Line L00P01 Drainage Study

3.0 HYDRAULIC ASSESSMENT

3.1 ANALYSIS FRAMEWORK AND METHODOLOGY

Hydraulic modeling analysis has been performed for a portion of Line LOOP01 storm drain mainline to determine the hydraulic grade line (HGL) of the system and to determine the sensitivity of Dana Point Harbor on-site tributary runoff inclusion on the system HGL. Line LOOP01 traverses 6,850-feet between its origin at the Golden Lantern/Selva Road intersection and its outlet into Dana Point Harbor marina, however, the hydraulic modeling does not extend north of Pacific Coast Highway because the hydraulic flow regime in the pipe system between Dana Point Harbor Drive and Del Prado is supercritical and backwater effects from the downstream system are absent. Three hydraulic models were prepared for the three conditions described in Chapter 2, including existing condition 10-year event without Harbor tributary inclusion (Model 1), existing condition 10-year event with Harbor tributary inclusion (Model 2), and proposed condition 10-year event with Harbor tributary inclusion (Model 3). 10-year event discharges utilized in the hydraulic modeling were taken from the hydrologic results presented in Chapter 2. Hydraulic modeling analysis was performed utilizing the Water Surface Pressure Gradient (WSPG) computer modeling software Version 14.06 from Civil Design Corporation, originally the Los Angeles County Flood Control District program FO515P. Storm drain system stationing, invert elevations, and conduit sizes were taken directly from as-built drawings of the existing LOOP01 system (see Appendix A-Exhibits 1 and 4). Because station and vertical datum control were different between the two sets of as-built plans, stations and inverts were converted on the Dana Point Harbor drainage plan (Exhibit 1) to agree with the LOOP01 drainage plan (Exhibit 4). Conversion data can be seen on Figures 5a, 5b, and 5c. Hydraulic models 1, 2, and 3 can be found in Appendices D1, D2, and D3 respectively.

3.2 HYDRAULIC RESULTS

Hydraulic grade line results from the three WSPG models described in Section 3.2 are summarized in Tables 3.1, 3.2, and 3.3 respectively.

Table 3.1 HGL Summary-Existing Condition, No Harbor Tributary (Model 1)

Storm Drain Station ⁽¹⁾	Description	Conduit/ Size ⁽¹⁾	Invert Elev ⁽¹⁾	Depth of Flow (ft)	HGL Elev	Finished Surface Elev
1+99.39	Marina Outlet	5x10' RCB	-12.22	17.26	5.04	7.2
2+80.66	MH in Parking Lot	60" RCP	-0.26	4.89	4.63	9.0
6+10.66	MH in Parking Lot	60" RCP	3.28	9.58	12.86	14.0
10+54.00	MH/JS @ Golden Lantern/DPHD Intersection	60" RCP	5.29	20.95	26.24	26.6
11+00.66	MH/JS to CB on Goldern Lantern	60" RCP	5.69	21.39	27.08	26.5
11+94.98 (Downstream)	Hydraulic Jump	60" RCP	15.68	13.45	29.14	29.2
11+94.98 (Upstream)	Hydraulic Jump	60" RCP	15.68	2.43	18.11	29.2
12+92.50	JS to CB on Golden Lantern	60" RCP	22.89	2.40	25.29	33.5
15+72.50	JS Lateral to Marriot	60" RCP	47.04	2.35	49.39	56.5
16+22.50	MH/JS Lateral to Tr. 11153	60" RCP	52.00	2.32	54.32	61.0
18+62.50	MH/JS Lateral to Tr. 11153	60" RCP	74.54	2.65	77.19	83.2
23+67.50	MH/JS Lateral to Tr.	60" RCP	92.19	3.85	96.04	122.3
25+46.29	JS Lateral to CB at GL/Del Prado Int.	66" RCP	94.54	3.84	98.38	132.0
26+88.61	JS/MH Lateral to CB on Del Prado	66" RCP	96.41	4.16	100.57	133.1

⁽¹⁾ Refer to Exhibits 1 and 4 in Appendix A.

Table 3.2 HGL Summary-Existing Condition, Including Harbor Tributary (Model 2)

Storm Drain Station ⁽¹⁾	Description	Conduit /Size ⁽¹⁾	Invert Elev ⁽¹⁾	Depth of Flow (ft)	HGL Elev	Finished Surface Elev
1+99.39	Marina Outlet	5'x10' RCB	-12.22	17.26	5.04	7.2
2+56.50	JS Lateral to Lower Parking Lot Pickup	60" RCP	-5.74	3.37	-2.37	8.5
2+80.66	MH in Parking Lot	60" RCP	-0.26	4.89	4.63	9.0
3+56.16	JS Lateral to On-Site Golden Lantern CB's	60" RCP	0.55	6.18	6.73	9.7
5+06.16	JS Lateral to On-Site Westerly Parking Lot	60" RCP	2.16	8.55	10.71	12.7
6+10.66	MH in Parking Lot	60" RCP	3.28	10.45	13.73	14.0
10+54.00	MH/JS @ Golden Lantern/DPHD Intersection	60" RCP	5.29	21.83	27.12	26.6
11+00.66	MH/JS to CB on Golden Lantern	60" RCP	5.69	22.27	27.96	26.5
12+09.85 (Downstream)	Hydraulic Jump	60" RCP	16.79	13.49	30.28	30.1
12+09.85 (Upstream)	Hydraulic Jump	60" RCP	16.79	2.42	19.21	30.1
12+92.50	JS to CB on Golden Lantern	60" RCP	22.89	2.40	25.29	33.5
15+72.50	JS Lateral to Marriot	60" RCP	47.04	2.35	49.39	56.5
16+22.50	MH/JS Lateral to Tr. 11153	60" RCP	52.00	2.32	54.32	61.0
18+62.50	MH/JS Lateral to Tr. 11153	60" RCP	74.54	2.65	77.19	83.2
23+67.50	MH/JS Lateral to Tr.	60" RCP	92.19	3.85	96.04	122.3
25+46.29	JS Lateral to CB at GL/Del Prado Int.	66" RCP	94.54	3.84	98.38	132.0
26+88.61	JS/MH Lateral to CB on Del Prado	66" RCP	96.41	4.16	100.57	133.1

⁽¹⁾ Refer to Exhibits 1 and 4 in Appendix A.

Table 3.3 HGL Summary-Proposal Condition, Including Harbor Tributary (Model 3)

Storm Drain Station ⁽¹⁾	Description	Conduit /Size ⁽¹⁾	Invert Elev ⁽¹⁾	Depth of Flow (ft)	HGL Elev	Finished Surface Elev
1+99.39	Marina Outlet	5'x10' RCB	-12.22	17.26	5.04	7.2
2+65.77	JS/MH Lateral to Westerly Parking Lot	60" RCP	-3.64	3.64	0.00	10.5
2+80.66	MH in Parking Lot	60" RCP	-0.26	4.89	4.63	10.5
4+23.74	JS/MH Lateral to Terrace Area	60" RCP	1.27	7.32	8.59	9.5
6+10.66	MH in Parking Lot	60" RCP	3.28	10.29	13.57	15.0
10+54.00	MH/JS @ Golden Lantern/DPHD Intersection	60" RCP	5.29	21.66	26.96	26.6
11+00.66	MH/JS to CB on Golden Lantern	60" RCP	5.69	22.10	27.79	26.5
12+07.08 (Downstream)	Hydraulic Jump	60" RCP	16.58	13.49	30.07	30.0
12+07.08 (Upstream)	Hydraulic Jump	60" RCP	16.58	2.43	19.01	30.0
12+92.50	JS to CB on Golden Lantern	60" RCP	22.89	2.40	25.29	33.5
15+72.50	JS Lateral to Marriot	60" RCP	47.04	2.35	49.39	56.5
16+22.50	MH/JS Lateral to Tr. 11153	60" RCP	52.00	2.32	54.32	61.0
18+62.50	MH/JS Lateral to Tr. 11153	60" RCP	74.54	2.65	77.19	83.2
23+67.50	MH/JS Lateral to Tr.	60" RCP	92.19	3.85	96.04	122.3
25+46.29	JS Lateral to CB at GL/Del Prado Int.	66" RCP	94.54	3.84	98.38	132.0
26+88.61	JS/MH Lateral to CB on Del Prado	66" RCP	96.41	4.16	100.57	133.1

⁽¹⁾ Refer to Exhibits 1 and 4 in Appendix A.

The analysis results identify several key items;

- Except for a short segment of open channel flow between stations 2+35 and 2+85, flow passing through the Harbor is under pressure in all three model scenarios.

- Although pressure flow is prevalent in Line LOOP01 as it passes through the Harbor, the hydraulic grade line stays below ground and provides freeboard under all three model conditions.
- The mainline junction structure at station 10+54 located at the intersection of Golden Lantern and Dana Point Harbor Drive receives substantial lateral flow from tributaries to the west. The flow regime is pressurized and the hydraulic grade line is near or above finished surface at this location under all three model conditions.
- A significant grade break in the pipe invert occurs at station 11+00 transitioning from a steep invert gradient upstream of the location to a flat invert gradient downstream of the location. This grade break causes a hydraulic jump in the hydraulic grade line generally around station 12+00 in all three models. Downstream of the hydraulic jump, flow in the pipe system becomes pressurized and the hydraulic grade line is above ground at station 11+00.66 likely creating an outflow condition during a ten-year peak flow storm even at the catch basin on the west side of Golden Lantern just north of the intersection. The contribution of runoff to the system from Dana Point Harbor on-site tributaries does not change this condition in any of the models.
- An open channel flow regime with supercritical flow is present upstream of the hydraulic jump (upstream of station 12+00) in all three models.

3.3 CONCLUSIONS

The Orange County Dana Point Harbor Revitalization Project is planning renovations to the harbor's commercial core area south of Dana Point Harbor Drive, east of Casitas Place, and west of Puerto Place in the City of Dana Point. The Harbor was originally constructed in the late 1960's and early 1970's and included a 60" RCP storm drain conduit to drain off-site areas upstream of the Harbor and to drain portions of the commercial core area in the Harbor. The conduit (Line LOOP01) outlets into the Dana Point Harbor marina and was originally constructed 835-feet north to a terminus just north of Dana Point Harbor Drive (formerly Del Obispo Street). Between the mid-1970's and late 1980's, Line LOOP01 was extended northerly in phases to its terminus at the intersection of Selva Road and Street of The Golden Lantern. Drainage planning for the Harbor Revitalization Project allows for Line LOOP01 to continue receiving runoff from up to 4.5 acres of tributary area from the on-site Harbor watershed which is consistent with historical drainage usage patterns. Due to the absence of reliable hydrologic and hydraulic information for Line LOOP01, analysis has been prepared and presented in this report to confirm that the continued flow of Harbor tributary to Line LOOP01 will not have an adverse effect to the hydraulic performance of the pipe system. Results presented throughout the report lead to the following conclusions:

- Runoff from 4.5 acres of on-site Harbor tributary watershed has historically flowed into and been conveyed to the marina outlet by the Line LOOP01 storm drain system.
- The City of Dana Point Master Plan of Drainage Document (Appendix A-Exhibit 2) has omitted the 4.5 acre Harbor watershed from inclusion into Line LOOP01's overall tributary watershed.
- Model 1 results presented in this report do not represent the current hydrologic and hydraulic condition of the storm drain system because the model does not include runoff from the 4.5 acres of Harbor tributary.
- With the inclusion of 10-year storm event runoff from up to 4.5 acres of Harbor tributary, the hydraulic grade line of Line LOOP01 remains below finished ground through the Harbor area and provides freeboard in existing (Model 2) and proposed (Model 3) modeling conditions.
- Existing condition (Model 2) hydraulic modeling results indicate runoff from a 10-year peak flow storm event will be purged from a catch basin inlet on the Street of The Golden Lantern just north of the intersection with Dana Point Harbor Drive (around storm drain station 11+00). Proposed condition (Model 3) hydraulic modeling results indicate this condition will not be changed and the inclusion of on-site Harbor runoff into the system will not otherwise adversely affect the LOOP01 storm drain system.

Results and conclusions stated above and throughout this analysis and report confirm that storm flow runoff from up to 4.5 acres of Harbor tributary watershed can be conveyed through the Harbor by Line LOOP01 without any adverse effect to the hydraulic grade line.

4.0 REFERENCES

1. Orange County Hydrology Manual, October, 1986
2. Orange County Local Drainage Manual, January, 1986

APPENDIX A. EXHIBITS

EXHIBIT 1 – DANA POINT HARBOR DRAINAGE PLAN (CIRCA 1968)

EXHIBIT 2 – CITY OF DANA POINT MASTER PLAN OF DRAINAGE
DOCUMENT

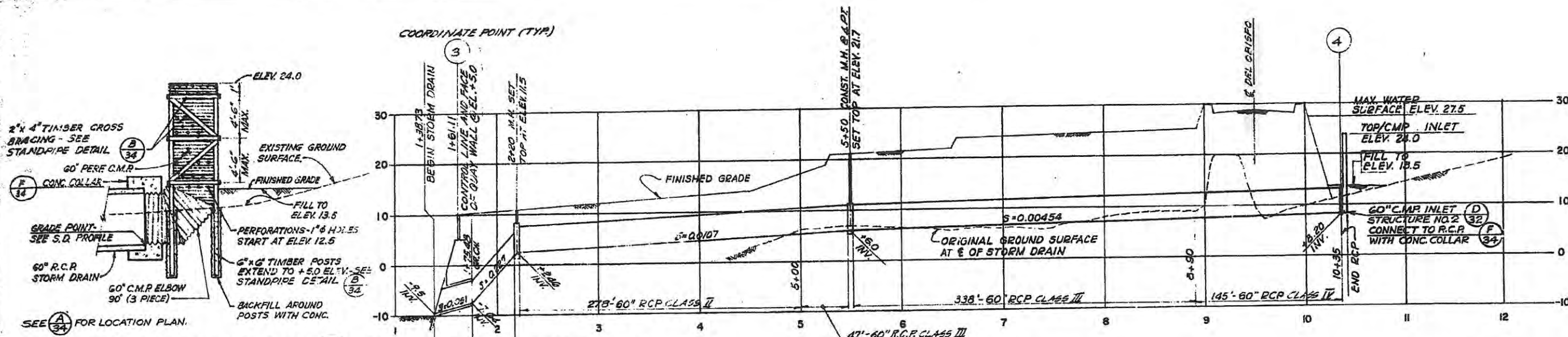
EXHIBIT 3 – CITY OF DANA POINT STORM DRAIN ATLAS

EXHIBIT 4 - FACILITY LOOP01 AS-BUILT PLAN, DANA POINT HARBOR
DRIVE TO PCH

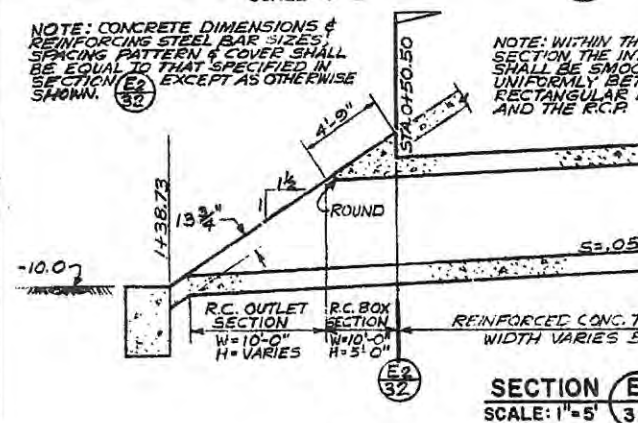
EXHIBIT 5 – GOLDEN LANTERN STORM DRAIN (FACILITY LOOP01), PCH
TO SELVE ROAD

EXHIBIT 6 – CITY OF DANA POINT LAND USE MAP (NOVEMBER 23, 1993)

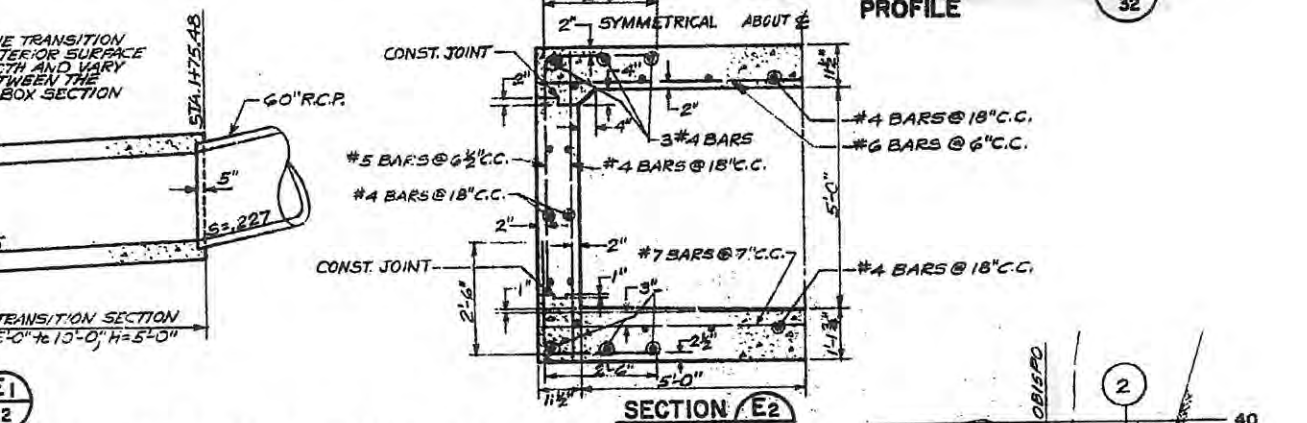
EXHIBIT 7 – CITY OF DANA POINT ZONING MAP (JUNE 3, 2008)



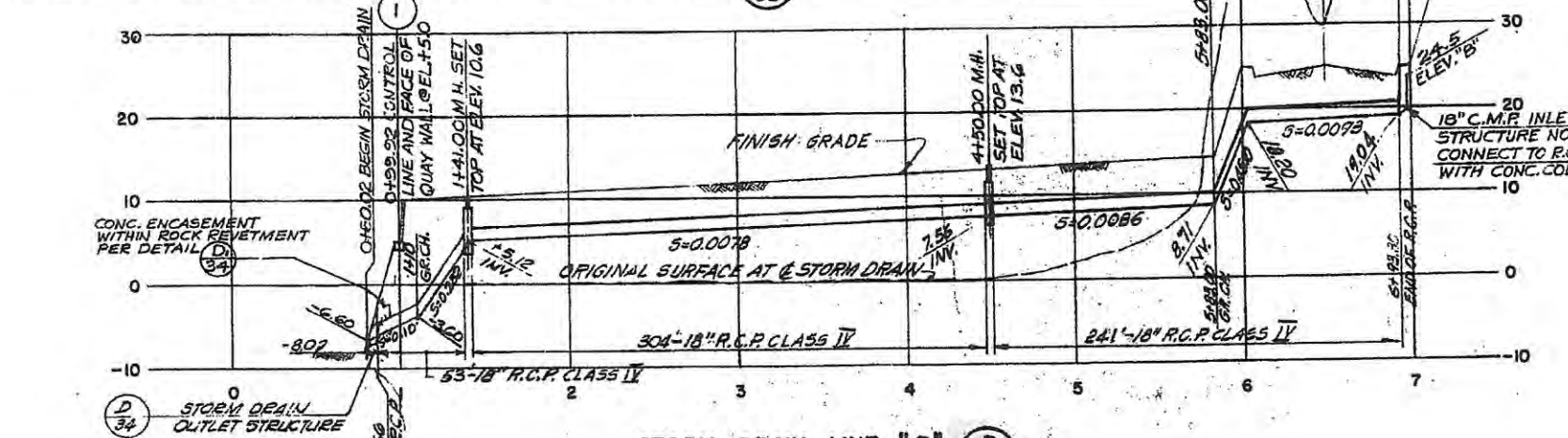
STORM DRAIN INLET STRUCTURE NO. 2 (D) 32
SCALE: 1"=5'



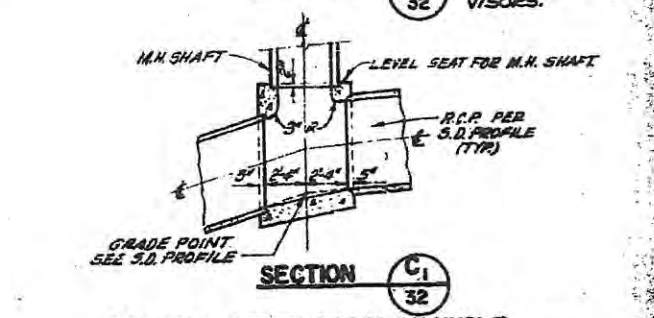
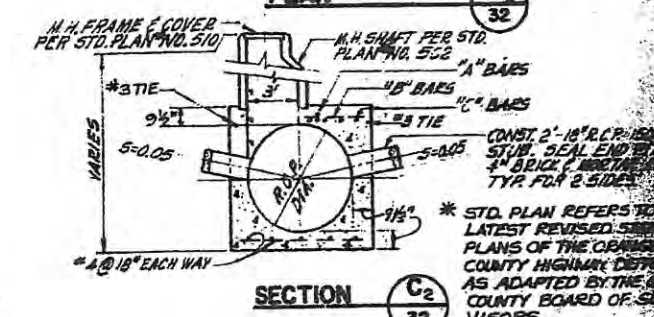
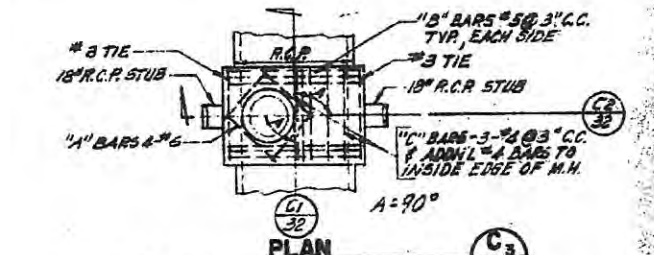
STORM DRAIN LINE 'C' PROFILE (A) 32 10,11,31,34



SPECIAL OUTLET STRUCTURE FOR STORM DRAIN LINE 'C' (E) 31



STORM DRAIN LINE 'B' PROFILE (B) 32 10,11,31

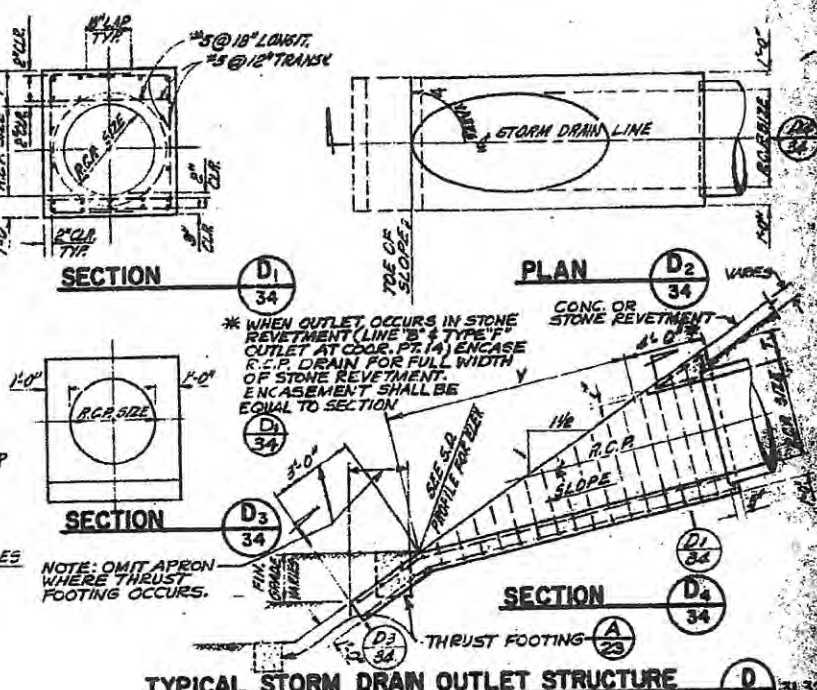
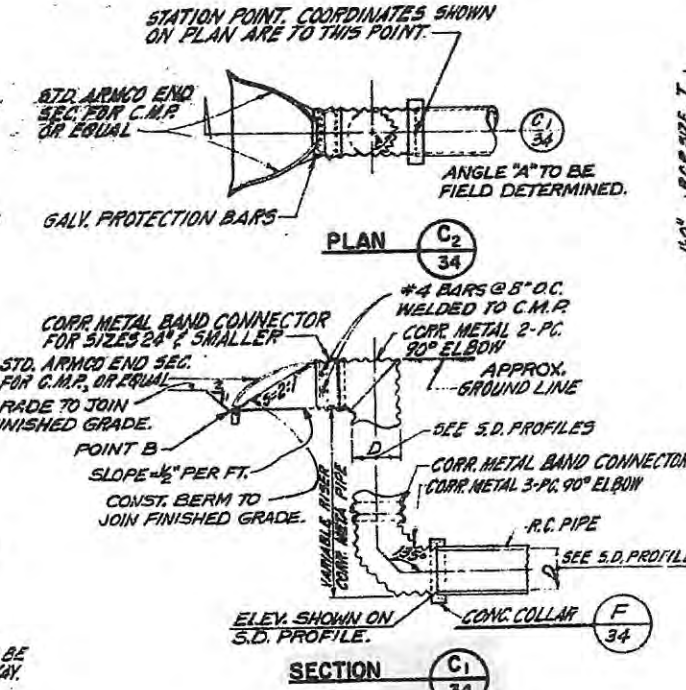
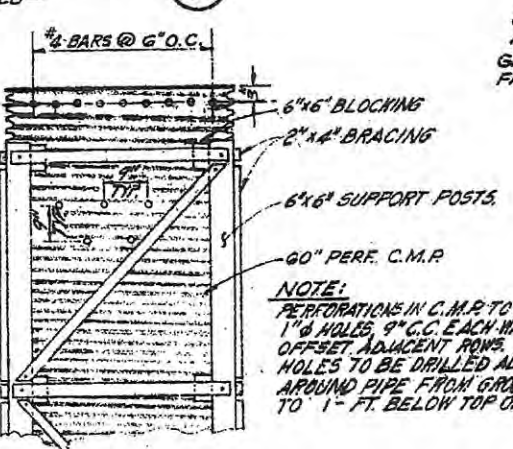
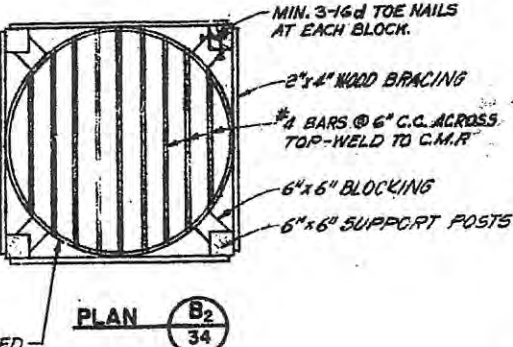
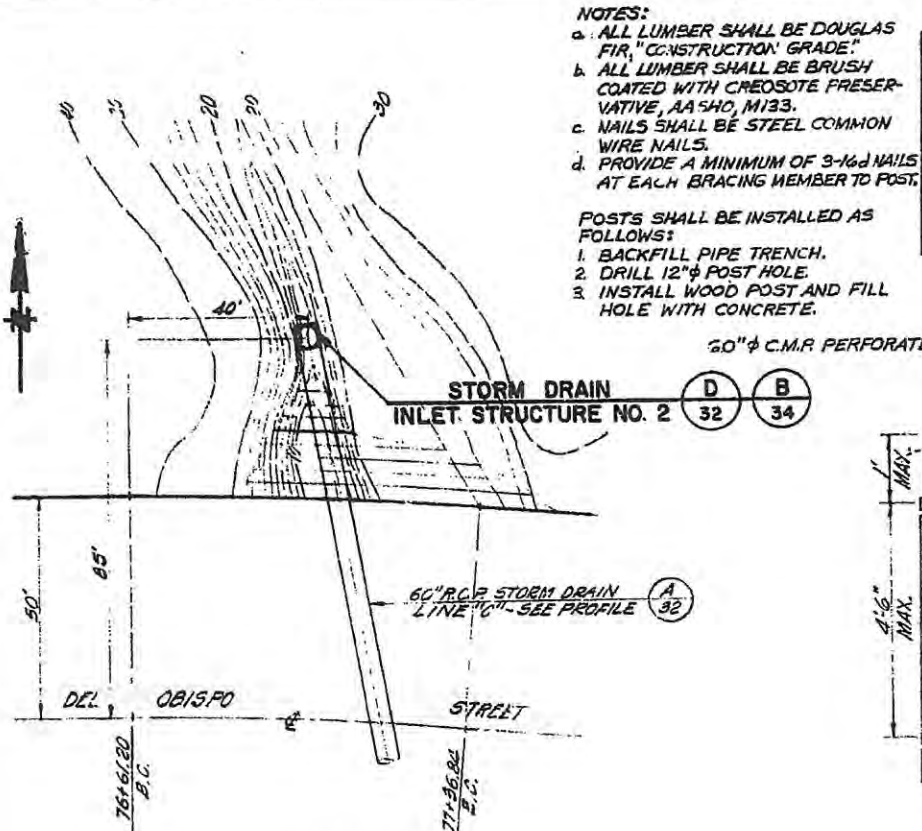


TYPICAL STORM DRAIN MANHOLE FOR DIAMETER LARGER THAN 24\"/>

ORANGE COUNTY HARBOUR DISTRICT 1801 BAYSIDE DRIVE DANFORTH BEACH, CALIFORNIA 92626	
PLANS PREPARED BY KORRING & KORRING, INC. ENGINEERS AND ARCHITECTS LOS ANGELES, CALIFORNIA 213 / 688-2000	
DANA POINT HARBOR DANFORTH, CALIFORNIA HEAVY CONSTRUCTION DRAINAGE PROFILES I	
PLAN NO. 1-417 SHEET NO. 32 OF 50	DATE: OCTOBER, 1988 SCALE: AS SHOWN
Plan 89796 Dana Point Harbor Sheet 32 of 50 Red 22.511 Elevation Scale - As Shown	MICROFILMED JUN 6 1989

- NOTES:**
- ALL LUMBER SHALL BE DOUGLAS FIR, "CONSTRUCTION GRADE"
 - ALL LUMBER SHALL BE BRUSH COATED WITH CREOSOTE PRESERVATIVE, AASHO, M133.
 - NAILS SHALL BE STEEL COMMON WIRE NAILS.
 - PROVIDE A MINIMUM OF 3-16d NAILS AT EACH BRACING MEMBER TO POST.

- POSTS SHALL BE INSTALLED AS FOLLOWS:
- BACKFILL PIPE TRENCH.
 - DRILL 12" ϕ POST HOLE.
 - INSTALL WOOD POST AND FILL HOLE WITH CONCRETE.



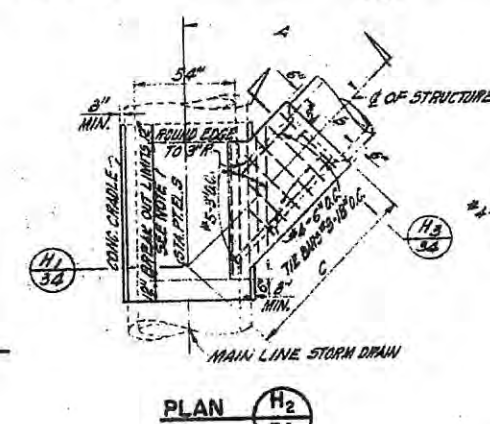
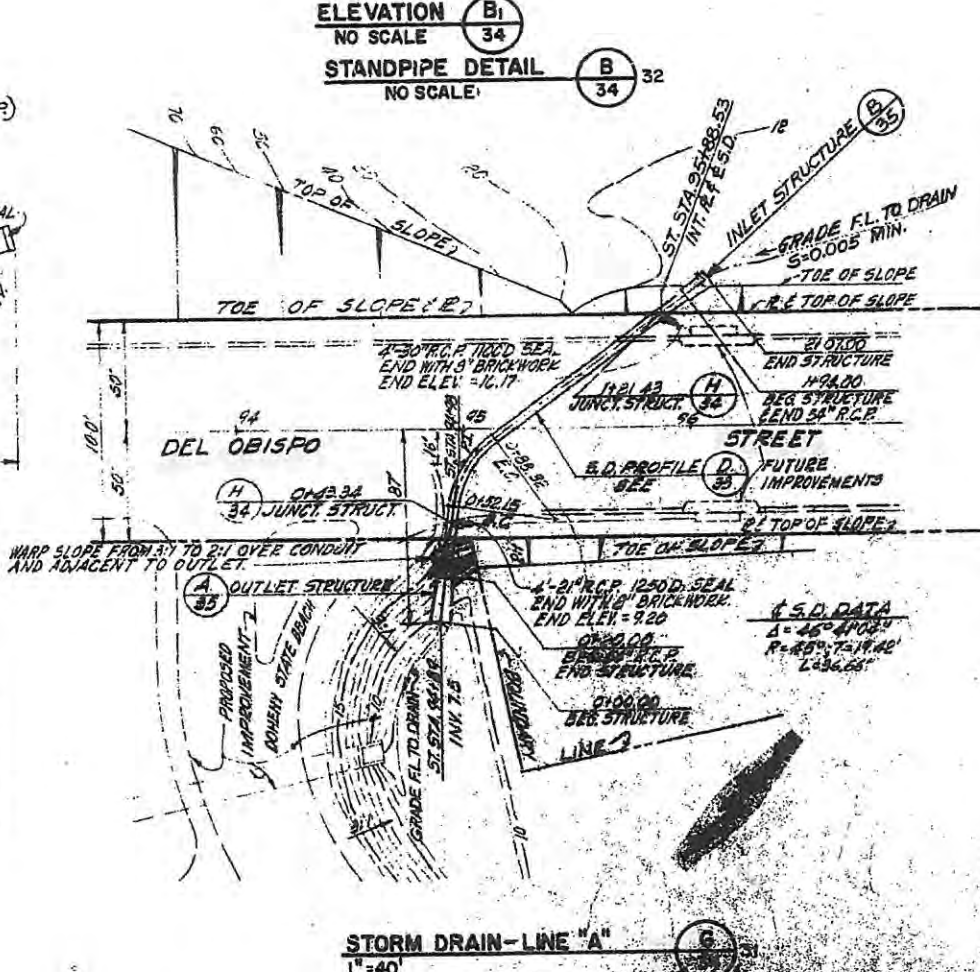
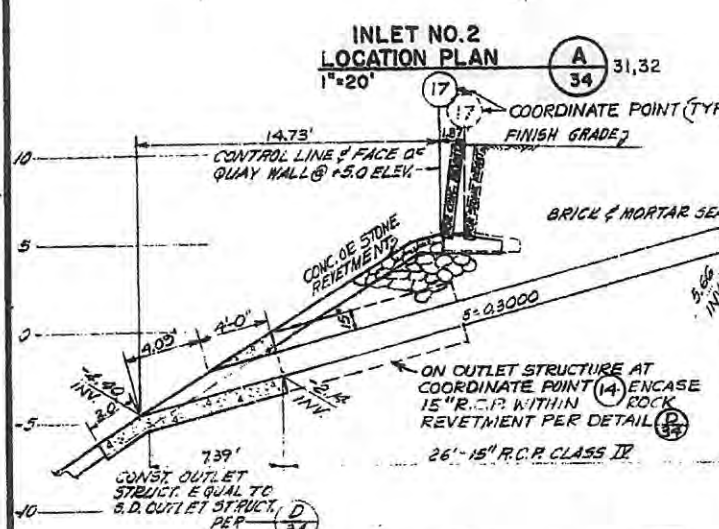
INLET STRUCTURE NO. 1
NO SCALE
C 31, 32, 34

TYPICAL STORM DRAIN OUTLET STRUCTURE
NO SCALE
D 31, 32, 34

S.D. LINE	R.C.P. SIZE	SLOPE	ELEV. INV.	Y	T
"B"	18" ϕ	0.100	-0.60	2'-10"	2'-1"
"C"					SPECIAL STRUCTURE-SEE (E)
"D"	18" ϕ	0.200	-5.2	3'-7 3/4"	1'-7 3/4"
"E"	18" ϕ	0.200	-4.82	3'-0 7/8"	1'-7 3/4"
"F"	5" ϕ	0.100	-2.0	8'-0"	2'-7 3/8"
TYPICAL OUTLET STRUCT.	15" ϕ	0.300	-4.2	4'-1"	1'-3"

INLET NO. 2 LOCATION PLAN
1"=20'
A 31, 32, 34

ELEVATION STANDPIPE DETAIL
NO SCALE
B 34

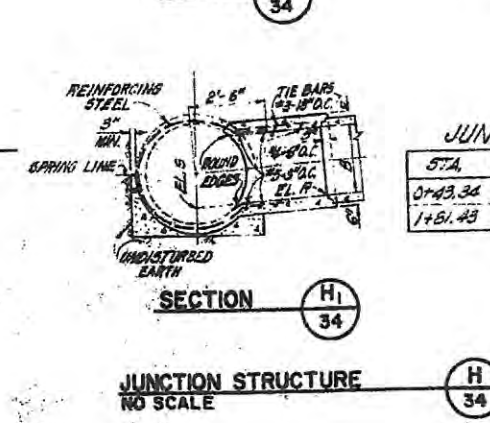


JUNCTION STRUCTURE NOTES

- BREAKOUT LIMITS SHALL BE DETERMINED AS FOLLOWS:
UPSTREAM LIMIT - AT THE INTERSECTION OF THE OUTSIDE OF THE SPUR WALL WITH THE MAIN LINE. PIPE WALL.
DOWNSTREAM LIMIT - 6 INCHES DOWNSTREAM OF THE INTERSECTION OF THE SPUR WALL WITH THE MAIN LINE PIPE WALL.
THE OPENING SHALL BE RECTANGULAR, CUT NORMAL TO PIPE SURFACE AND WITHOUT DAMAGING REINFORCING STEEL. IF A JOINT IN THE MAIN LINE PIPE FALLS WITHIN THE LIMITS OF THE CONCRETE CRADLE, PROVIDE AN ENCASUREMENT ONE FOOT ABOVE THE TOP OF THE MAIN LINE PIPE TO THE LIMITS OF THE CRADLE.
- THE TRANSVERSE REINFORCEMENT IN PIPE SHALL BE CUT AT CENTER OF OPENING AND BENT INTO TOP AND BOTTOM SLABS OF SPUR.
- CONCRETE STRENGTH SHALL BE 3,000 PSI AT 28 DAYS.

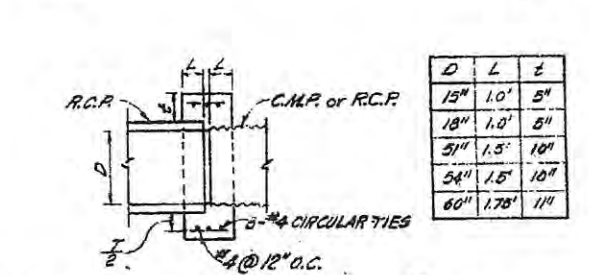
JUNCTION STRUCTURE DATA

STA.	A	B	C	EL.P.	EL.S.
0+43.34	82° 45' 32"	2"	4.5'	9.14	9.07
1+51.43	63° 48' 14"	30"	5'10"	9.60	8.97



JUNCTION STRUCTURE
NO SCALE
H 34

TYPICAL TYPE "F" OUTLET STRUCTURE
1"=5'
E 31, 34



TYPICAL CONCRETE COLLAR DETAIL
NO SCALE
F 32, 33, 34

STORM DRAIN-LINE "A"
1"=40'
G 34

ORANGE COUNTY HARBOR DISTRICT
REPORT BECH, CALIFORNIA
1801 BAYSIDE DRIVE 714/664-2200

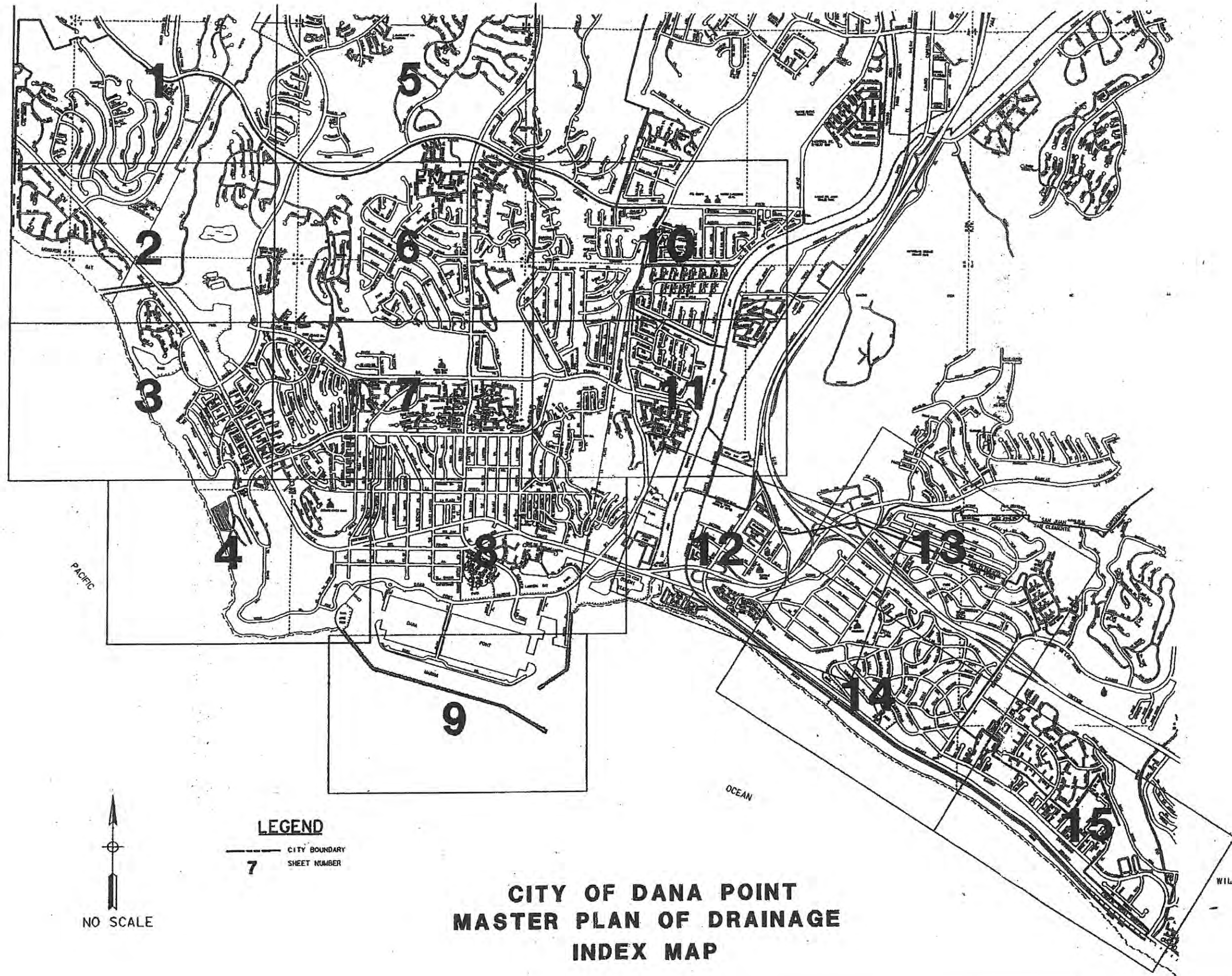
PLANS PREPARED BY
K KOBAS & KOBAS, INC.
CIVIL ENGINEERING ARCHITECTURE PLANNING
LONG BEACH, CALIFORNIA
213/650-5100

DANA POINT HARBOR
DANA POINT, CALIFORNIA
HEAVY CONSTRUCTION
DRAINAGE DETAILS I

ACID NO. 1-417 APPROVED: [Signature] DATE: OCTOBER, 1968
SCALE: AS SHOWN SHEET: 34 OF 30 D 10-531

Plan 69796
Dana Point Harbor
Sheet 34 of 30
Red 22-51
Titleblock
Scale - As Shown

RECORDED
JUN 6 1969
EXHIBIT 1



LEGEND
— CITY BOUNDARY
7 SHEET NUMBER

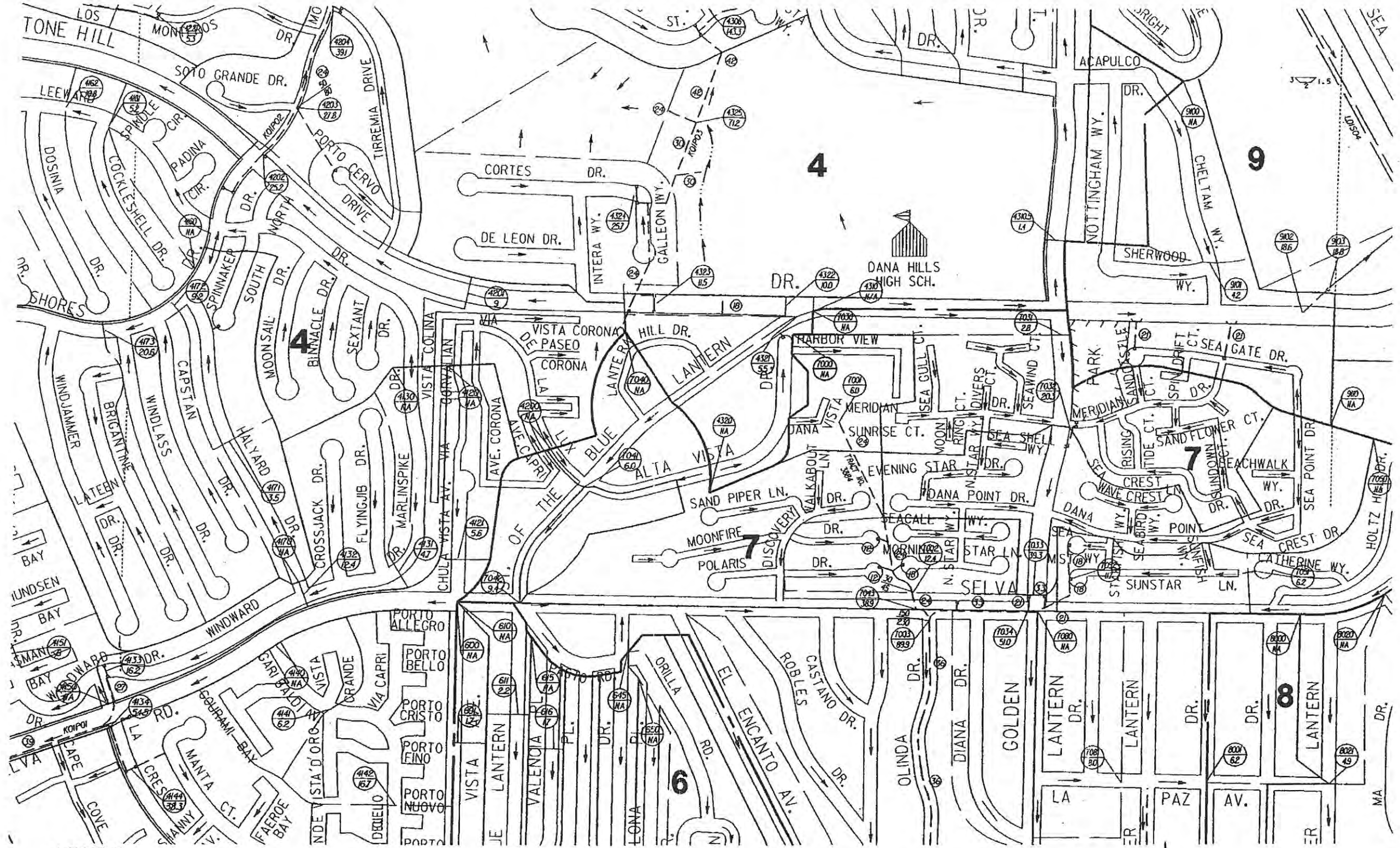
**CITY OF DANA POINT
MASTER PLAN OF DRAINAGE
INDEX MAP**



EXHIBIT 2

(SEE SHEET 6)

(SEE SHEET 3)



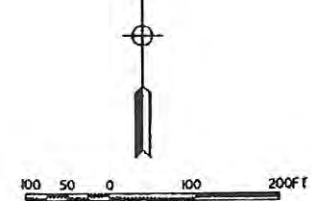
(SEE SHEET 11)

(SEE SHEETS 4 & 8)

LEGEND

- CITY BOUNDARY
- MAJOR DRAINAGE AREA BOUNDARY
- DRAINAGE AREA BOUNDARY
- SUBDRAINAGE AREA BOUNDARY
- EXISTING STORM DRAIN
- EXISTING CONCRETE CHANNEL AND BOX
- PROPOSED STORM DRAIN
- FLOW DIRECTION
- 4 MAJOR DRAINAGE AREA DESIGNATION
- ⊙ NODE NUMBER
- ⊙ TOTAL TRIBUTARY AREA
- ⊙ EXISTING CONCRETE CHANNEL (FEET)
- ⊙ EXISTING RCP (INCHES)
- ⊙ PROPOSED RCP (INCHES)
- 25 10 YEAR STORM RUNOFF (cfs)
- 60 100 YEAR STORM RUNOFF (cfs)
- ⊙ EXISTING VERTICAL WALL CHANNEL
- ⊙ EXISTING PIPE ARCH BASE x DEPTH (INCHES)
- ⊙ EXISTING REINFORCED CONCRETE BOX CULVERT

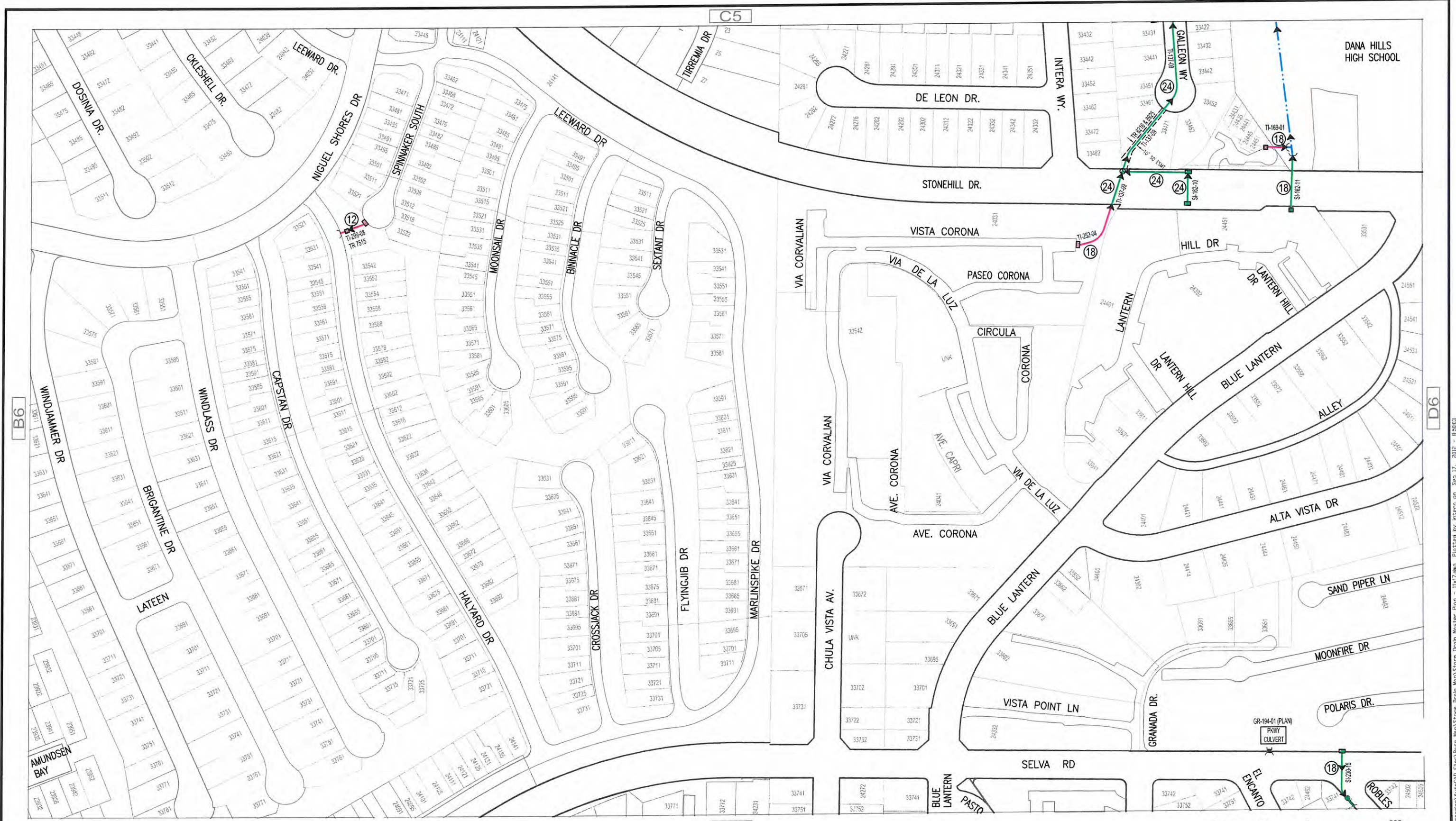
**CITY OF DANA POINT
MASTER PLAN OF DRAINAGE**



SHEET 7

EXHIBIT 2

12/84



DRAFT (IN REVIEW)

LEGEND	
	DANA POINT MAINTAINED STORM DRAIN LINE
	COUNTY MAINTAINED STORM DRAIN LINE
	PRIVATE STORM DRAIN LINE
	CALTRANS MAINTAINED STORM DRAIN LINE
	LAGUNA NIGUEL MAINTAINED STORM DRAIN LINE
	SAN JUAN CAPISTRANO MAINTAINED STORM DRAIN LINE
	SAN CLEMENTE MAINTAINED STORM DRAIN LINE
	AT&SF RAILROAD MAINTAINED STORM DRAIN LINE
	FUTURE STORM DRAIN LINE
	ABANDONED STORM DRAIN LINE
	OPEN CHANNEL
	CITY LIMITS
	PUBLIC STREET CITY MAINTAINED
	PRIVATE STREETS
	STORM DRAIN FILE #
	FACILITY #
	MAN HOLES
	PIPE DIAMETER
	DRAIN OUTLETS
	HEADWALL INLETS
	CATCH BASINS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	GRATE INLETS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	SD CLEANOUT (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)

REVISED:

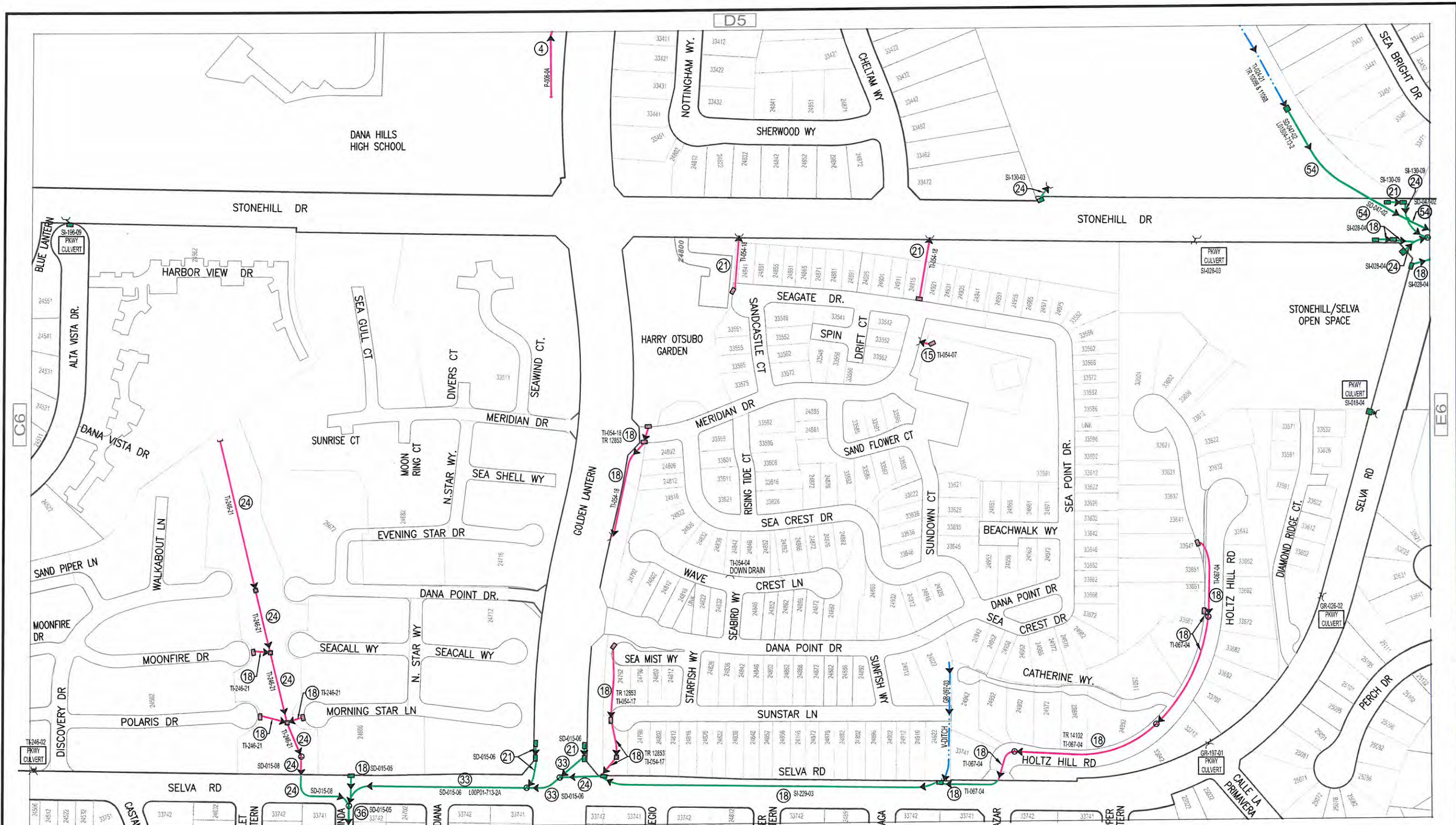
B5	C5	D5
B6	C6	D6
B7	C7	D7

200 100 0 200
scale SCALE: 1" = 200' feet

CITY OF DANA POINT
STORM DRAIN ATLAS

SHEET
C6
OF 53

EXHIBIT 3



DRAFT (IN REVIEW)

LEGEND		PUBLIC STREET CITY MAINTAINED		MAN HOLES		CATCH BASINS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)	
	DANA POINT MAINTAINED STORM DRAIN LINE		SAN CLEMENTE MAINTAINED STORM DRAIN LINE		18		GRATE INLETS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	COUNTY MAINTAINED STORM DRAIN LINE		AT&SF RAILROAD MAINTAINED STORM DRAIN LINE		36		GRATE INLETS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	PRIVATE STORM DRAIN LINE		FUTURE STORM DRAIN LINE		24		SD CLEANOUT (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	CALTRANS MAINTAINED STORM DRAIN LINE		ABANDONED STORM DRAIN LINE		33		SD CLEANOUT (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	LAGUNA NIGUEL MAINTAINED STORM DRAIN LINE		OPEN CHANNEL		21		SD CLEANOUT (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	SAN JUAN CAPISTRANO MAINTAINED STORM DRAIN LINE		CITY LIMITS		18		
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DRAFT (IN REVIEW)

LEGEND		PUBLIC STREET CITY MAINTAINED		MAN HOLES		CATCH BASINS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)	
	DANA POINT MAINTAINED STORM DRAIN LINE		SAN CLEMENTE MAINTAINED STORM DRAIN LINE		MAN HOLES		CATCH BASINS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	COUNTY MAINTAINED STORM DRAIN LINE		AT&SF RAILROAD MAINTAINED STORM DRAIN LINE		PIPE DIAMETER		GRATE INLETS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	PRIVATE STORM DRAIN LINE		FUTURE STORM DRAIN LINE		DRAIN OUTLETS		SD CLEANOUT (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	CALTRANS MAINTAINED STORM DRAIN LINE		ABANDONED STORM DRAIN LINE		HEADWALL INLETS		
	LAGUNA NIGUEL MAINTAINED STORM DRAIN LINE		OPEN CHANNEL				
	SAN JUAN CAPISTRANO MAINTAINED STORM DRAIN LINE		CITY LIMITS				

REVISED:
09/10/12

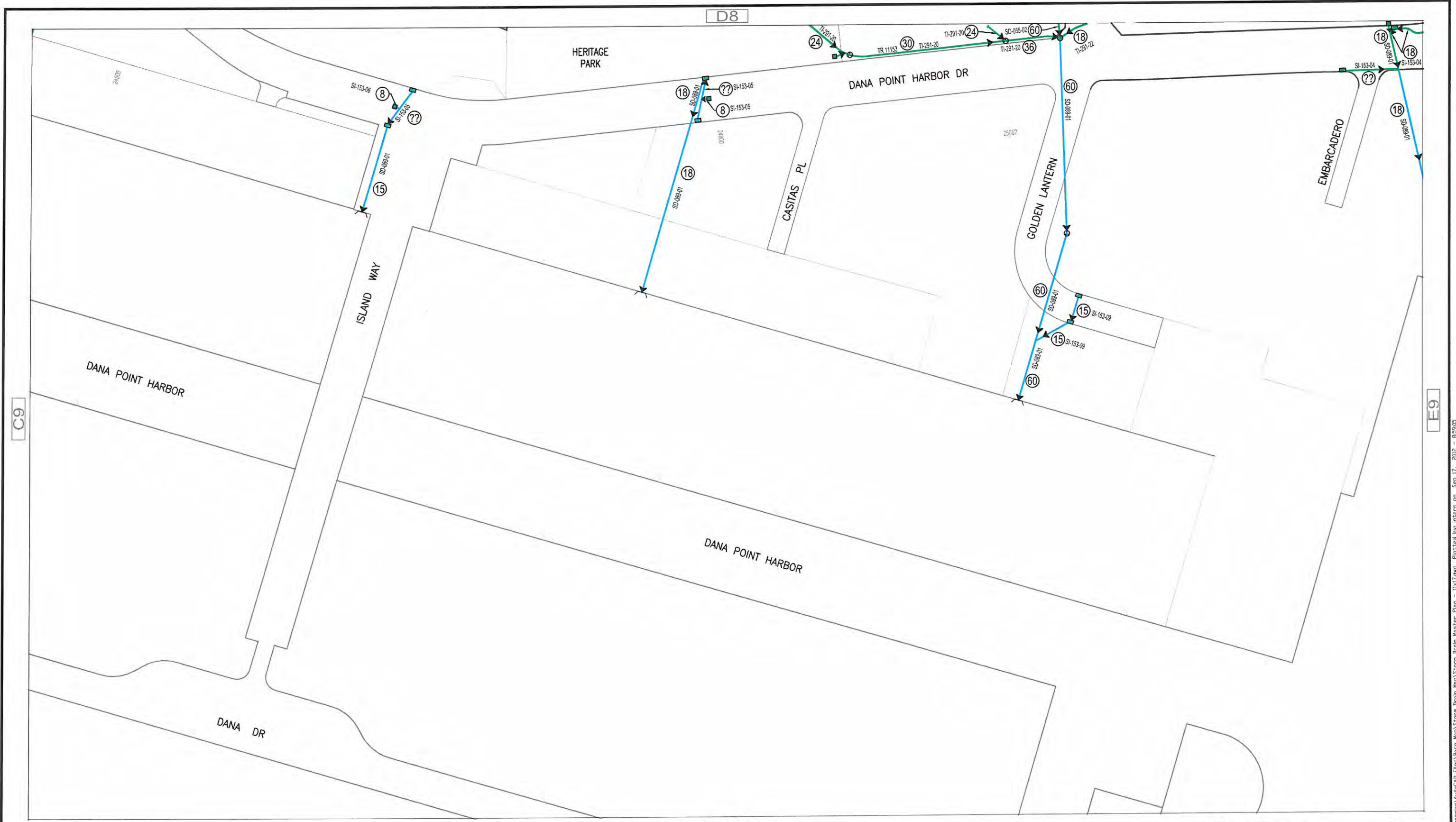
C6	D6	E6
C7	D7	E7
C8	D8	E8

200 100 0 200
scale SCALE: 1" = 200' feet

CITY OF DANA POINT
STORM DRAIN ATLAS

SHEET
D7
OF 53

EXHIBIT 3

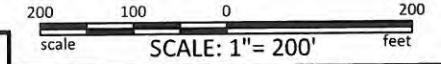


DRAFT (IN REVIEW)

LEGEND		PUBLIC STREET CITY MAINTAINED		MAN HOLES		CATCH BASINS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)	
	DANA POINT MAINTAINED STORM DRAIN LINE		SAN CLEMENTE MAINTAINED STORM DRAIN LINE		MAN HOLES		CATCH BASINS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	COUNTY MAINTAINED STORM DRAIN LINE		AT&SF RAILROAD MAINTAINED STORM DRAIN LINE		PIPE DIAMETER		GRATE INLETS (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	PRIVATE STORM DRAIN LINE		FUTURE STORM DRAIN LINE		DRAIN OUTLETS		SD CLEANOUT (COLOR REPRESENTS AGENCY RESPONSIBLE FOR MAINTENANCE)
	CALTRANS MAINTAINED STORM DRAIN LINE		ABANDONED STORM DRAIN LINE		HEADWALL INLETS		
	LAGUNA NIGUEL MAINTAINED STORM DRAIN LINE		OPEN CHANNEL				
	SAN JUAN CAPISTRANO MAINTAINED STORM DRAIN LINE		CITY LIMITS				
		SD-XX-XX	STORM DRAIN FILE #				
		K01-XXX-XX	FACILITY #				

REVISED:

C8	D8	E8
C9	D9	E9
	D10	



CITY OF DANA POINT
STORM DRAIN ATLAS

SHEET
D9
OF 53

EXHIBIT 3

ORANGE COUNTY ENVIRONMENTAL MANAGEMENT AGENCY

SANTA ANA, CALIFORNIA
M. STORM, DIRECTOR

PLANS FOR CONSTRUCTION OF FACILITY NO. LOOP01

FROM DEL OBISPO ST. TO P.C.H. GENERAL NOTES: (CONTINUED)
DANA POINT HARBOR DRIVE

GENERAL NOTES

- ALL WORK TO BE DEDICATED TO THE COUNTY OF ORANGE SHALL BE IN CONFORMANCE WITH THE DISTRICT'S STD. SPECS. WHICH MAY BE PURCHASED FROM THE DISTRICT AND SHALL BE KEPT ON THE JOB SITE AT ALL TIMES.
- THE CONTRACTOR SHALL NOTIFY THE DISTRICT'S INSPECTOR AT LEAST 24 HOURS PRIOR TO COMMENCEMENT OF ANY CONSTRUCTION BY TELEPHONING 934-3410, OR BY WRITING THE ORANGE COUNTY FLOOD CONTROL DISTRICT, 400 WEST CIVIC CENTER DRIVE, SANTA ANA, CALIF.
- ALL CONC. IN REINF. CONC. STRUCTURES SHALL BE 3000 POUNDS PER SQ. INCH. IN 28 DAYS, PORTLAND CEMENT CONC., CLASS A.
- ALL PIPE LENGTHS ARE HORIZONTAL PROJECTIONS, UNLESS OTHERWISE SHOWN.
- LOCATIONS OF PUBLIC UTILITIES SHOWN HAVE BEEN DETERMINED FROM AVAILABLE INFORMATION. HOWEVER IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO DETERMINE THE TRUE LOCATION OF ANY EXISTING UTILITIES AND TO EXERCISE PROPER PRECAUTIONS TO AVOID INJURY OR DAMAGE THERE TO.
- ALL FILL SHALL BE COMPACTED TO 90% RELATIVE COMPACTION AS DETERMINED BY THE CALIFORNIA TEST METHOD NO. Z16-F1963 "FIVE LAYER METHOD" ALL BACKFILL MATERIAL SHALL BE FREE FROM VEG-TABLE MATTER.
- PIPE CONSTRUCTION SHALL BE COORDINATED WITH THE GRADING WORK SO THAT WHEN THE FILL OPERATION HAS BEEN COMPLETED TO A GRADE A MIN. OF (4") FEET ABOVE THE TOP OF THE PIPE. THE STORM DRAIN TRENCH SHALL BE EXCAVATED AND THE PIPE INSTALLED.
- ALL REINF. CONC. PIPE SHALL BE BEDDED IN ACCORDANCE WITH OCEMA, STD. PLAN 319.
- REINFORCEMENT IN REIF. CONC. PIPE SHALL HAVE A MIN. CONC. COVER OF 1 1/2" FROM INSIDE FACE OF PIPE WHERE NOTED ON PLANS.
- ALL MATERIALS TESTING FOR THE STORM DRAIN FACILITIES AND RELATED CONSTRUCTION SHALL BE PROVIDED BY THE CONTRACTOR OR DEVELOPER IN ACCORDANCE WITH THE NUMBER, LOCATION AND FREQUENCY REQUESTED BY THE FLOOD CONTROL DISTRICT'S INSPECTOR.
- ALL SURVEYING REQUIRED FOR VERTICAL AND HORIZONTAL ALIGNMENT SHALL BE PROVIDED BY THE CONTRACTOR OR DEVELOPER AND SUFFICIENT REFERENCE STAKING SHALL BE IN ACCORDANCE WITH THE REQUEST OF THE DISTRICT'S INSPECTOR.
- ALL PIPE JOINTS SHALL BE Banded AND GROUTED.
- A PERMIT FOR WORK WITHIN EXISTING OR PROPOSED STREET RIGHT OF WAY IS REQUIRED FROM THE ORANGE COUNTY ROAD DEPT. FOR ANY ENCROACHMENT NECESSARY FOR CONSTRUCTION IN PUBLIC RIGHT OF WAY. STORM DRAIN BACKFILL FOR ALL FACILITIES WITHIN STREET RIGHT OF WAY IS TO BE PLACED AND COMPACTED UNDER ROAD DEPT. INSPECTION, AND MEET OR EXCEED ROAD DEPT. MINIMUM STANDARDS.

- THE CONTRACTOR SHALL NOTIFY THE ORANGE COUNTY ENVIRONMENTAL MANAGEMENT AGENCY, CONSTRUCTION DIVISION (934-3488) 48 HOURS PRIOR TO BEGINNING ANY WORK WITHIN DISTRICT'S RIGHT OF WAY.
- THE CONTRACTOR SHALL CONDUCT CONSTRUCTION OPERATIONS IN SUCH A MANNER THAT STORM OR OTHER WATERS MAY PROCEED UNINTERRUPTED ALONG THEIR EXISTING STREET OR DRAINAGE COURSES.
- IN THE COURSE OF WATER CONTROL, THE CONTRACTOR SHALL CONDUCT CONSTRUCTION OPERATIONS TO PROTECT WATERS FROM POLLUTION WITH FUELS, OILS, BITUMENS OR OTHER HARMFUL MATERIALS.
- ALL CONSTRUCTION SHALL BE IN ACCORDANCE WITH O.C.E.M.A. STANDARD SPECIFICATIONS. (PUBLIC WORKS CONSTRUCTION, 1979 EDITION.)
- CONTRACTOR SHALL PROVIDE FOR MATERIAL TESTING AT DIRECTION OF COUNTY ENGINEER.

ID	ITEM	QUANTITIES
	18" RCP - 1500 D	12 LF.
	18" RCP - 1750 D	19 LF.
	18" RCP - 2250 D	4 LF.
	18" RCP - 2550 D	16 LF.
	REMOVE EX. 36" RCP	15 LF.
	21" RCP - 1750 D	4 LF.
	24" RCP - 1250 D	4 LF.
	60" RCP - 1000 D	110 LF.
	60" RCP - 1000 D (1 1/2" EXTRA CONC. OVER STEEL)	646 LF.
	60" RCP - 1200 D	135 LF.
	60" RCP - 1700 D	150 LF.
	60" RCP - 1500 D	145 LF.
	60" RCP - 2000 D	103 LF.
	66" RCP - 1950 D	175 LF.
	66" RCP - 2400 D	1014 LF.
	JUNCTION STRUCTURE TYPE II - OCEMA STD. N° 311	2 EA.
	JUNCTION STRUCTURE TYPE VI - OCEMA STD. N° 315	5 EA.
	INLET TYPE I - OCEMA STD. N° 301	1 EA.
	PLUG WITH BECK AND MOLTAR (SIZE PER PLAN)	10 EA.
	REMOVE 170 LF. EX. 60" RCP & OUTLET FACILITY	1 EA.
	REMOVE EX. 60" CMP RISER AND CONC. COLLAR	1 EA.
	72" MANHOLE WITH PUMP STATION PER DETAIL SHT #15	1 EA.
	REINFORCED CONC. COLLAR - OCEMA STD. N° 317	2 EA.
	JCT. STR. TYPE II STD. N° 311 WITH PATENTED POLY. STD. N° 505	4 EA.
	JUNCT. STR. PER DETAIL OF SHEET #14	1 EA.

APPROVED FOR MAIN LINE STORM DRAIN ONLY
Jack Schwarz 9/26/81
JACK SCHWARZ DATE

MAINTAINED BY THE COUNTY OF ORANGE

PREPARED BY:
VTN CONSOLIDATED INC.
2501 CAMPUS DRIVE,
IRVINE, CALIFORNIA 92713
PHONE: (714) 851-5200

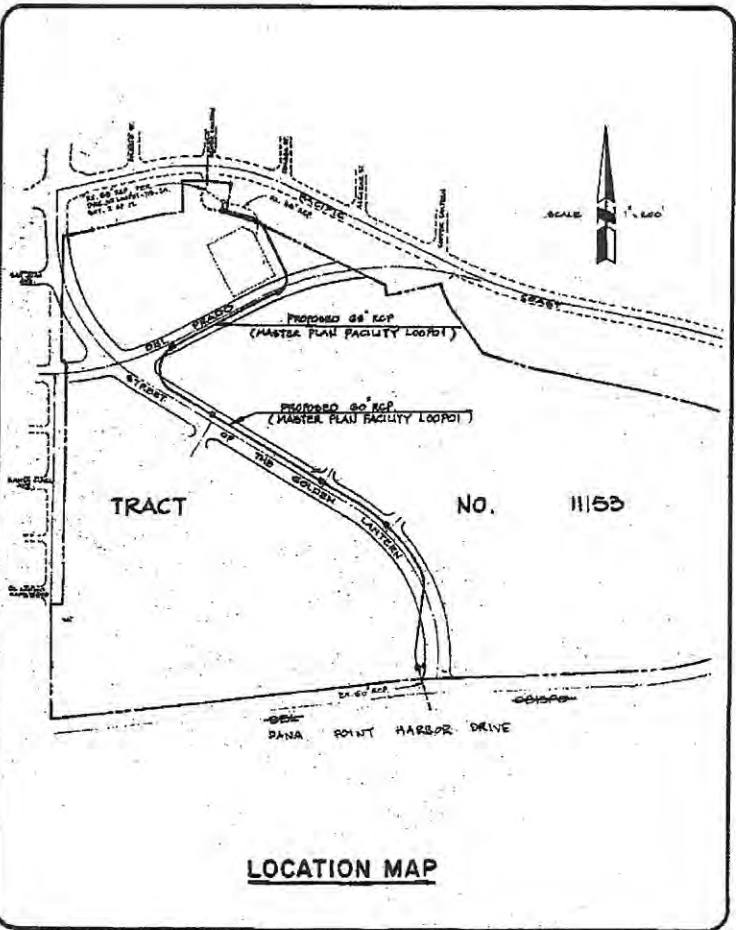
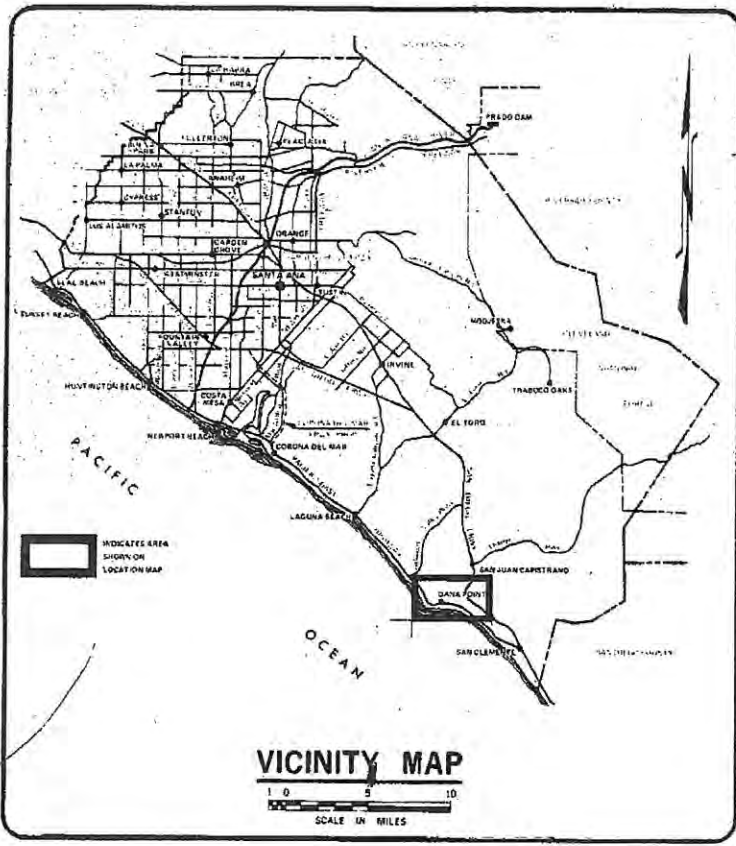
BY: *Lawrence Raskfield*
DATE: 6-29-81 RCE 28763

EMA REGULATION
THIS PLAN IS SIGNED BY EMA/REGULATION FOR CONCEPT AND ADHERENCE TO COUNTY STANDARDS AND REQUIREMENTS ONLY. EMA/REGULATION IS NOT RESPONSIBLE FOR DESIGN, ASSUMPTIONS, OR ACCURACY.

APPROVED: *J.W. Schwanz*
DATE: 10-30-81 RCE 8856

FACILITY NO. LOOP01 IS A COUNTY OF ORANGE MASTER PLAN OF DRAINAGE FACILITY BEING CONSTRUCTED IN ACCORDANCE WITH THE SAN JUAN CAPISTRANO AREA MASTER PLAN OF DRAINAGE UNDER THE ADMINISTRATION AND SUPERVISION OF THE ENVIRONMENTAL MANAGEMENT AGENCY.

AGREEMENT NO. D-21-081



SHEET	DESCRIPTION
1	TITLE SHEET
2	PLAN AND PROFILE
3	PLAN AND PROFILE
4	PLAN AND PROFILE
5	AUXILIARY PUMP STATION (DETAILS)
6	AUXILIARY PUMP STATION (SPECIFICATIONS)

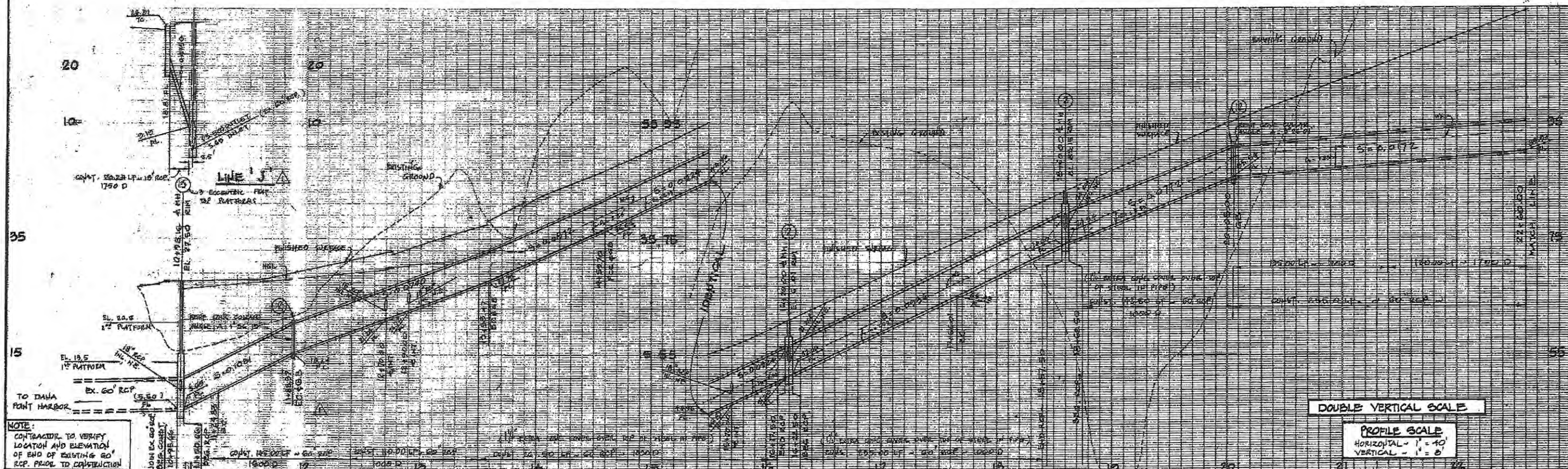
UTILITY	PHONE NO.
SOUTHERN CAL. GAS CO. UNDERGROUND SERVICE ALERT	800-422-1133
DANA POINT SANITARY DISTRICT	714-496-9382
CAPISTRANO BEACH COUNTY WATER DISTRICT	714-496-5261
SAN DIEGO GAS & ELECTRIC CO.	714-498-1100
STORER CABLE TELEVISION	714-881-3142
PACIFIC TELEPHONE CO.	714-951-0545

BENCH MARK (92-24-68) 510.005
ADDITIONAL CAP POSITIONING WAS PLACED ALONG THE PACIFIC COAST HIGHWAY (AS NOTED) FROM THE A.T. & S.F. RAILWAY OVERPASS OF THE HWY. IN CAPISTRANO BRANCH TO ITS INTERSECTION WITH DEL OBISPO STREET, ABOUT 245 FT. W. OF THE 9/4 OF THE HWY. 38 FT. 5/2 OF THE 9/4 OF THE STREET, 91.5 FT. 1/2 OF THESE 101.5 FT. 24 FT. 5/4 OF STREET LIGHT POLE IS 28249.8 ABOVE 80 FT. S.W. OF THE W. SIDE OF HOUSE # 3421 AND ACROSS THE STREET SET IN THE SAN JUAN CAPISTRANO AREA. (ELEV. 16.701 (1976 ADJ.) THAN THE GUTTER ELEV. 16.701 (1976 ADJ.))

BASIS OF BEARING:
N 77° 59' 44" E. FOR THE CENTERLINE OF PACIFIC COAST HIGHWAY AS SHOWN ON R.S. 91/27 & 28. RECORDS OF ORANGE COUNTY, CALIFORNIA.

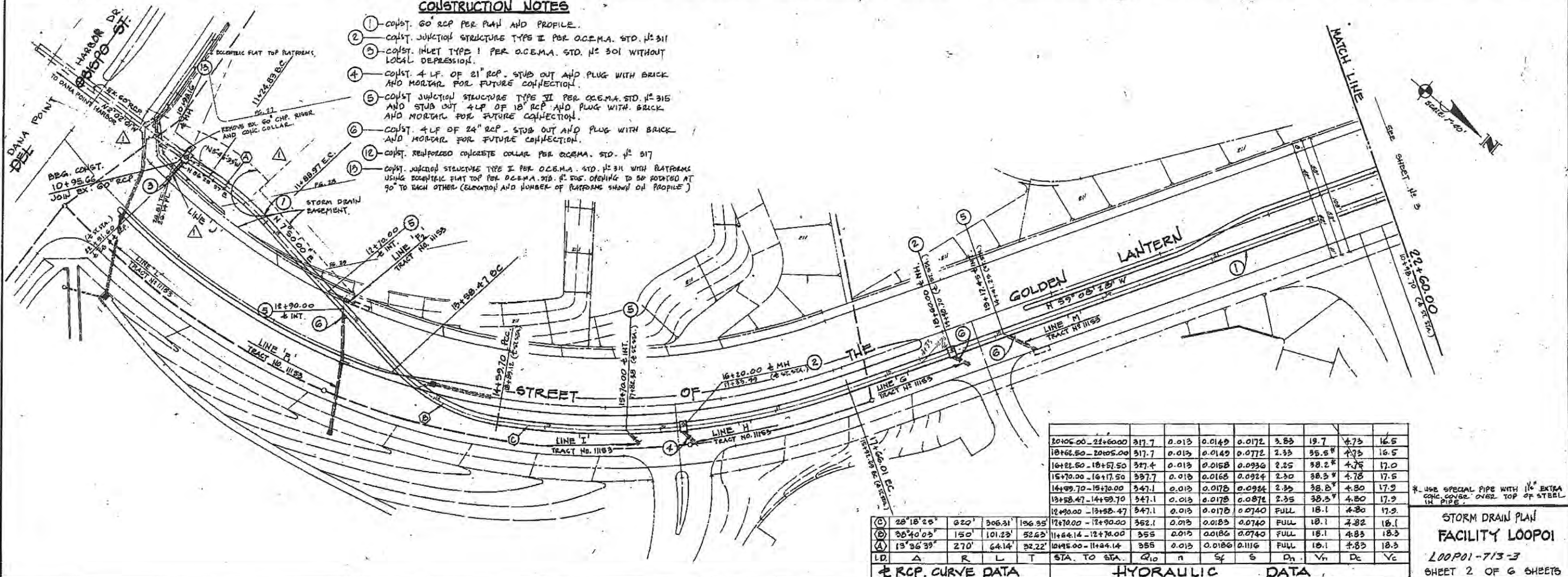
NO.	DESCRIPTION	SHT.	APPROVED	DATE

DWG. NO. LOOP01-713-3 SHEET 1 OF 6



CONSTRUCTION NOTES

1. CONST. 60" RCP PER PLAN AND PROFILE.
2. CONST. JUNCTION STRUCTURE TYPE II PER O.C.E.M.A. STD. # 311
3. CONST. INLET TYPE I PER O.C.E.M.A. STD. # 301 WITHOUT LOCAL DEPRESSION.
4. CONST. 4 LF. OF 21" RCP. STUB OUT AND PLUG WITH BRICK AND MORTAR FOR FUTURE CONNECTION.
5. CONST. JUNCTION STRUCTURE TYPE II PER O.C.E.M.A. STD. # 315 AND STUB OUT 4 LF. OF 18" RCP. AND PLUG WITH BRICK AND MORTAR FOR FUTURE CONNECTION.
6. CONST. 4 LF. OF 24" RCP. STUB OUT AND PLUG WITH BRICK AND MORTAR FOR FUTURE CONNECTION.
7. CONST. REINFORCED CONCRETE COLLAR PER O.C.E.M.A. STD. # 317
8. CONST. JUNCTION STRUCTURE TYPE I PER O.C.E.M.A. STD. # 311 WITH PATIENRUS USING SCHEMATIC FLAT TOP PER O.C.E.M.A. STD. # 305. OPENING TO BE ROTATED AT 90° TO EACH OTHER (ELEVATION AND NUMBER OF PATIENRUS SHOWN ON PROFILE)



RCP CURVE DATA

LINE	Δ	R	L	T	STA. TO STA.	G ₁₀	n	S _f	S	D _n	V _n	D _c	V _c
(C)	28°18'26"	820'	306.31'	196.95'	12+70.00 - 12+90.00	352.1	0.015	0.0133	0.0740	FULL	18.1	4.32	18.1
(D)	35°40'03"	150'	101.23'	52.23'	11+64.14 - 12+70.00	355	0.015	0.0186	0.0740	FULL	18.1	4.83	18.3
(A)	13°36'39"	270'	64.14'	32.22'	10+15.00 - 11+24.14	355	0.015	0.0186	0.1116	FULL	18.1	4.83	18.3

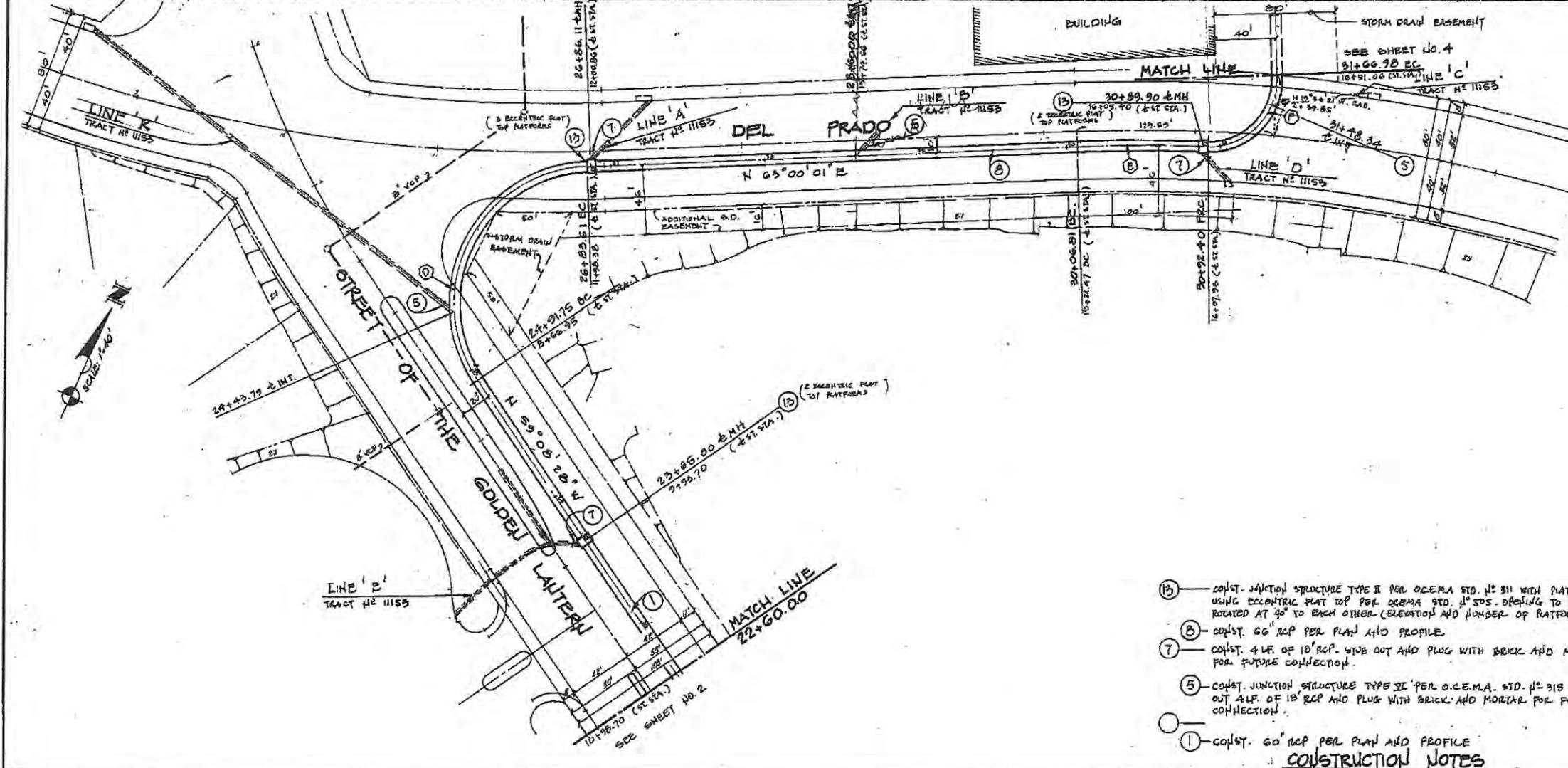
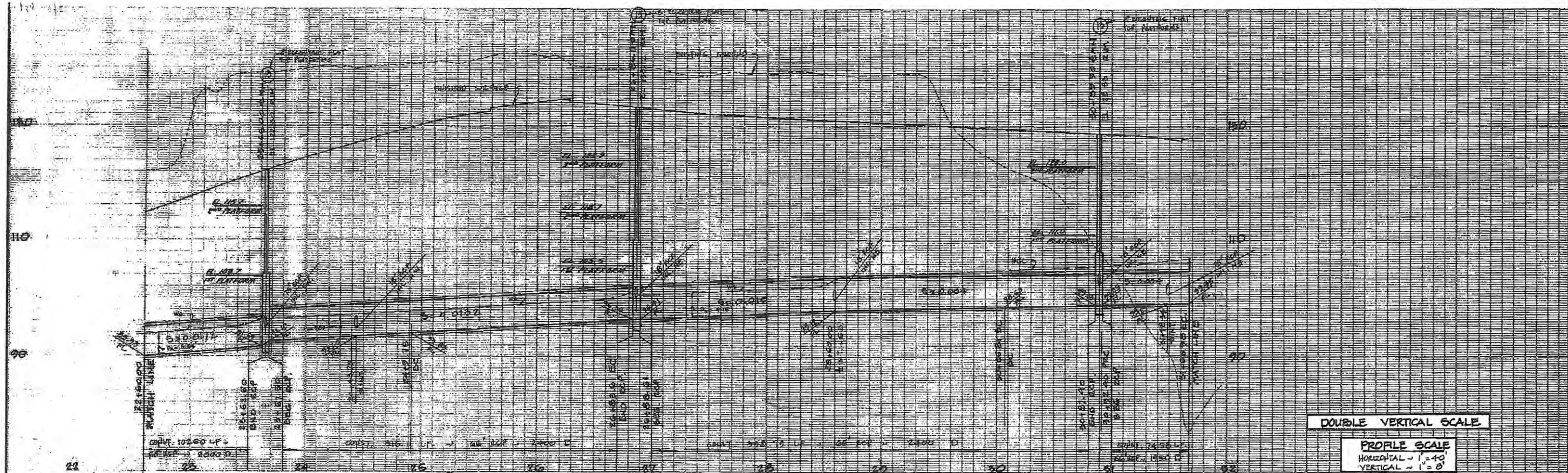
HYDRAULIC DATA

STA.	Q ₁₀	n	S _f	S	D _n	V _n	D _c	V _c
20+05.00 - 21+60.00	317.7	0.013	0.0149	0.0172	3.83	19.7	4.73	16.5
18+65.00 - 20+05.00	317.7	0.013	0.0149	0.0172	2.33	35.5	4.73	16.5
16+25.50 - 18+65.00	327.4	0.013	0.0158	0.0236	2.25	38.2	4.78	17.0
15+70.00 - 16+25.50	337.7	0.013	0.0168	0.0284	2.30	38.3	4.78	17.5
14+09.70 - 15+70.00	347.1	0.013	0.0178	0.0284	2.35	38.8	4.80	17.9
13+58.47 - 14+09.70	347.1	0.013	0.0178	0.0284	2.35	38.3	4.80	17.9
12+90.00 - 13+58.47	347.1	0.013	0.0178	0.0740	FULL	18.1	4.80	17.9
12+70.00 - 12+90.00	352.1	0.013	0.0133	0.0740	FULL	18.1	4.32	18.1
11+64.14 - 12+70.00	355	0.015	0.0186	0.0740	FULL	18.1	4.83	18.3
10+15.00 - 11+24.14	355	0.015	0.0186	0.1116	FULL	18.1	4.83	18.3

* USE SPECIAL PIPE WITH 1/2" EXTRA CONC. COVER OVER TOP OF STEEL IN PIPE.

**STORM DRAIN PLAN
FACILITY LOOP 01
LOOP 01-713-3
SHEET 2 OF 6 SHEETS**

EXHIBIT 4



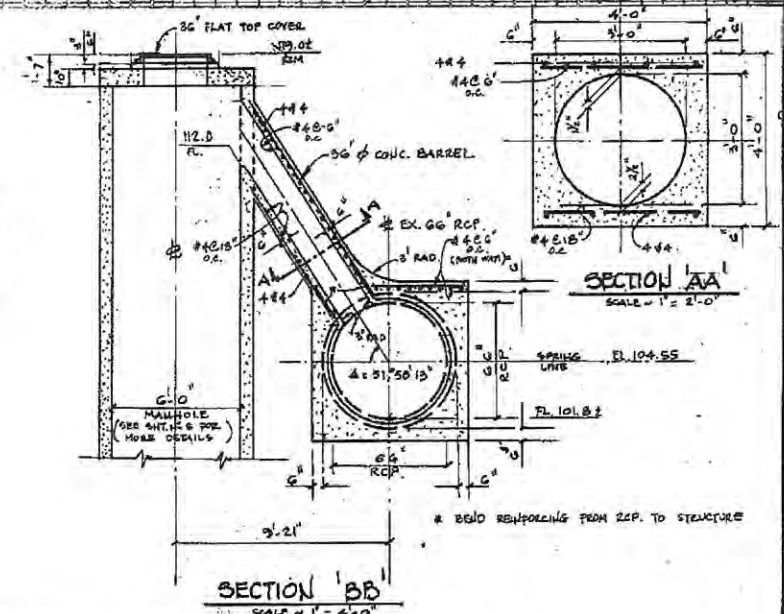
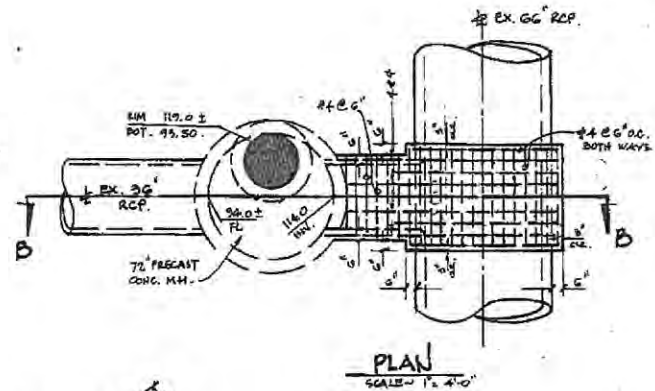
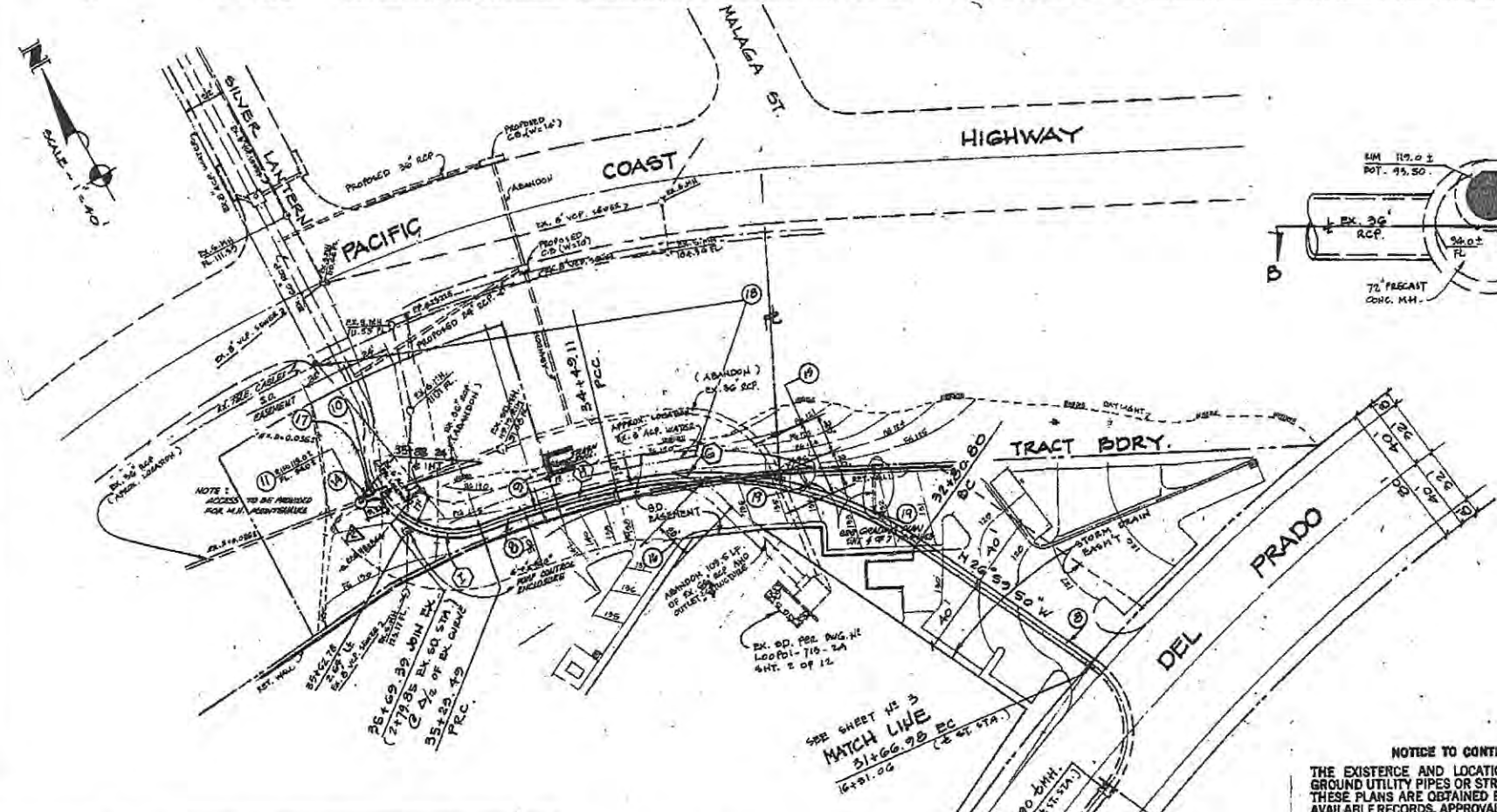
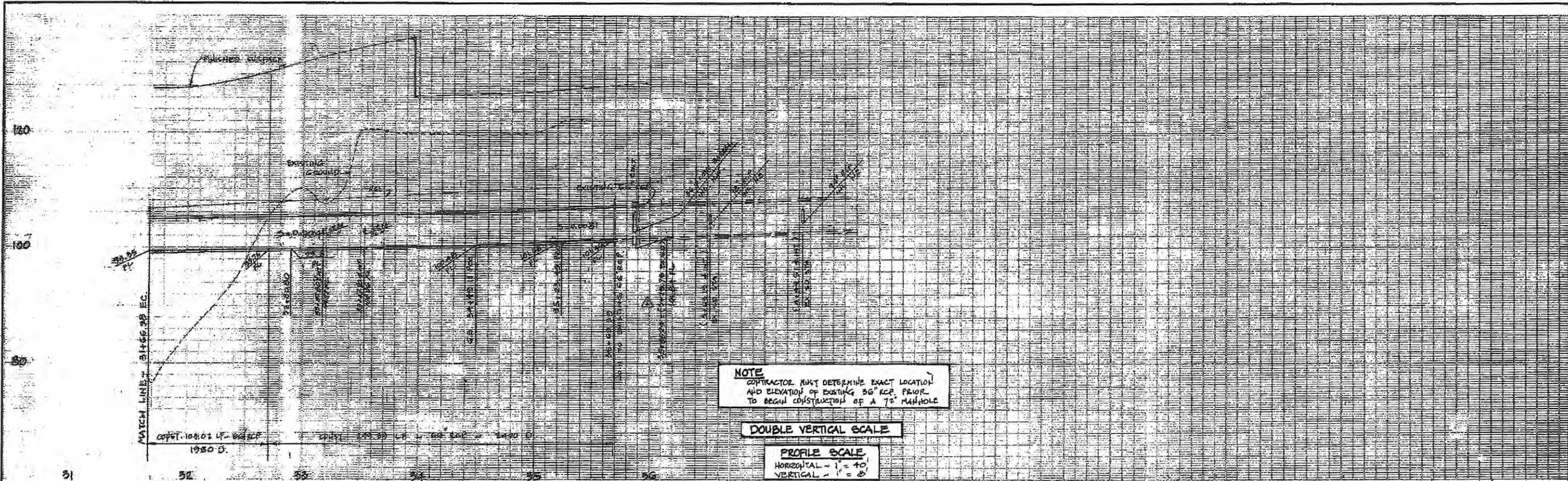
HYDRAULIC DATA									
STA. TO STA.	210	n	sf	s	Dn	Vn	Dc	Vc	Vc
22+60.00 - 23+62.50	317.7	0.013	0.0149	0.0172	3.83	19.7	4.73	16.5	
23+67.50 - 26+89.61	316.1	0.013	0.0089	0.0192	3.80	18.1	4.87	14.2	
26+88.61 - 28+60.00	307.9	0.013	0.0084	0.0100	4.15	16.0	4.81	14.0	
28+60.00 - 30+87.40	304.1	0.013	0.0082	0.0040	FULL	12.8	4.79	13.9	
30+92.40 - 31+68.34	303.0	0.013	0.0081	0.0040	FULL	12.8	4.79	13.8	
31+68.34 - 31+66.78	300.0	0.013	0.0081	0.0040	FULL	12.6	4.76	13.7	

- 15) CONST. JUNCTION STRUCTURE TYPE II PER O.C.E.M.A. STD. # 311 WITH PLATFORMS USING ECCENTRIC FLAT TOP PER O.C.E.M.A. STD. # 305. OPENING TO BE ROTATED AT 90° TO EACH OTHER (ELEVATION AND NUMBER OF PLATFORM SHOWN ON PROFILE)
 8) CONST. 66" RCP PER PLAN AND PROFILE
 7) CONST. 4 LF OF 18" RCP. STUB OUT AND PLUG WITH BRICK AND MORTAR FOR FUTURE CONNECTION.
 5) CONST. JUNCTION STRUCTURE TYPE II PER O.C.E.M.A. STD. # 315 AND STUB OUT ALL OF 18" RCP AND PLUG WITH BRICK AND MORTAR FOR FUTURE CONNECTION.
 1) CONST. 60" RCP PER PLAN AND PROFILE
- CONSTRUCTION NOTES**

R.C.P. CURVE DATA			
LO	A	R	L
(P)	24°57'13"	45'	74.58'
(E)	4°57'19"	920'	85.50'
(D)	122°06'35"	90'	191.80'

STORM DRAIN PLAN
 FACILITY LOOP 01
 LOOP 01-713-3
 SHEET 3 OF 6 SHEETS
 SD-CSS-03 177-33

EXHIBIT 4



JUNCTION STRUCTURE DETAILS
 @ STA: 3125.75 PRC OF EX. LINE (GG RCP) (14)

- (19) CONST. JUNCTION STRUCTURE TYPE II PER OCEANA STD. NO. 88 AND STRENGTH OUT 4 L.F. OF 8\"/>
- (18) CONTRACTOR SHALL REMOVE, SALVAGE & REPLACE EXIST. 6\"/>
- (17) INSTALL 1\"/>
- (16) REMOVE EXIST. 66\"/>
- (15) REMOVE 40 L.F. OF EXIST. 36\"/>
- (14) CONST. JUNCTION STR. PER DETAIL HEREOF.
- (11) CONST. 72\"/>
- (10) REMOVE 15 L.F. OF EX. 36\"/>
- (9) REMOVE 185 L.F. OF EX. 66\"/>
- (8) CONST. 66\"/>

CONSTRUCTION NOTES

STORM DRAIN PLAN
 FACILITY LOOP
 LOOP 713-3
 SHEET 4 OF 6 SHEETS
 SB-055-04

STA. TO STA.	Q ₁₀	n	Sf	S	D _n	Dc	Vc	T	R	L	T	
34+49.11 - 34+97.50	300	0.015	0.0081	0.0081	FULL	12.0	4.76	13.7	58'26.99'	75	45.90'	26.17'
31+22.95 - 34+49.11	300	0.015	0.0081	0.0040	FULL	12.0	4.76	13.7	7'49'10"	5+6'	74.55'	\$7.25'
31+22.95 - 34+49.11	300	n	Sf	S	D _n	Dc	Vc	T	R	L	T	

NOTICE TO CONTRACTOR
 THE EXISTENCE AND LOCATION OF ANY UNDERGROUND UTILITY PIPES OR STRUCTURES SHOWN ON THESE PLANS ARE OBTAINED BY A SEARCH OF THE AVAILABLE RECORDS. APPROVAL OF THIS PLAN BY THE ORANGE COUNTY ENVIRONMENTAL MANAGEMENT AGENCY DOES NOT CONSTITUTE A REPRESENTATION AS TO THE ACCURACY OR COMPLETENESS OF THE LOCATION OR THE EXISTENCE OR NON-EXISTENCE OF ANY UNDERGROUND UTILITY PIPE OR STRUCTURE WITHIN THE LIMITS OF THIS PROJECT. THE CONTRACTOR IS REQUIRED TO TAKE ALL DUE PRECAUTIONARY MEANS TO PROTECT THE UTILITY LINES NOT OF RECORD OR NOT SHOWN ON THIS PLAN.

1. STORM WATER PUMP STATION:

1.1 General: The Contractor shall furnish and install in the structure as described by specifications, and as shown in the plans, one factory-built automatic pumping unit as manufactured by the Clow Corporation, or equal. The principle items of the pumping unit shall include one submersible centrifugal sewage pump; motor control panel with fully magnetic type circuit breaker, magnetic motor starter, and automatic liquid level control system.

1.2 Pump:

- a. The pump must have the necessary characteristics and be properly selected to pump unscreened storm water at design conditions as shown on the contract drawings. The pump/motor unit must be non-overloading across the complete head/capacity range of the pump.
- b. The pump shall have a 4-inch discharge with 125 pound standard cast iron flange fitting.
- c. All pump openings and passages shall be of adequate size to pass spheres 3 inches in diameter and any trash or stringy material which can pass through the storm drain.
- d. The impeller shall be of cast iron, enclosed, and non-clog type shall be dynamically balanced.
- e. Pump shall include impeller and suction cover wear rings. Impeller wear ring shall be of cast polymer material.
- f. All exposed fasteners and lock washers shall be of 316 stainless steel.
- g. The pump shaft shall be sealed against leakage by an oil-filled double mechanical seal. Both the stationary sealing member and mated rotating member shall be of tungsten-titanium carbide alloy.

1.3 Pump Motor:

- a. The submersible pump motor shall be as called for on the contract drawings. The pump and motor furnished shall be an integral unit. Motor shall be suitable for Class 1, Division 1, Group D hazardous locations.
- b. Motor frame and end shield shall be of corrosion-resistant cast iron with stainless steel hardware and shaft.
- c. The oil filled seal chamber shall contain a moisture sensing probe through which signs of impending seal failure may be signalled to the motor control panel. This seal chamber shall also contain a labyrinth flame path slinger which serves as a protective slinger for the upper seal.
- d. Motor shall have an internal pressure capability of 280 psi.

1.4 Quick Lift Assembly

- a. General: Furnish one "quick lift" slide rail mechanism to guide submersible pump from 5 feet above the concrete base to its operational location in the sump base.
- b. Elbow: The base elbow shall be cast in accordance with A.S.T.M. Specification No. A46-76, Class 30. All pipe flanges shall be faced and to the thickness required for compliance with 125 lb. American Standard. Bolt slots are acceptable in lieu of drilled holes. Bolt slots in the base are to be provided for mounting the elbow to the concrete floor or sole plate. The base elbow is specifically designed to permit the slide mechanism to link up the pump with the base elbow.
- c. Rail: The guide rail is to be constructed from standard structural angle and anti-rust coated to prevent corrosion and maintain a smooth surface for the guide shoes. The guide rail is to be attached to the discharge pipe with pipe straps every 12" o/c.
- d. Guide Shoes: Two teflon coated shoes are to guide the pump assembly down the guide rail until the shoes contact the discharge elbow. The pump then fulcrums about this point and positions the pump discharge flange to properly engage it with the discharge elbow.
- e. Jam Washer: A neoprene jam washer shall fit in the slide plate to minimize leakage between the pump casing and base elbow.
- f. Slide: The pump discharge is to be bolted to the slide on one side and the guide shoes are to be attached to the other side. The slide is to be guided in its descent and ascent by the rail and guide shoes.

1.5 Lift Cable:

A 1/2 inch diameter stainless steel braided wire lift cable shall be permanently attached to the pump. Provision shall be made for attaching upper end of this cable to the wet wall access frame.

1.6 Hardware:

All bolts, machine screws, nuts, washers, and lockwashers for complete assembly of access cover, guide rails, and discharge elbow shall be furnished by manufacturer in 316 stainless steel.

1.7 Control:

- a. Enclosure: A NEMA type 4, UL listed, dead-front enclosure, key-lockable, shall house all control equipment. The panel shall be fully gasketed and dust tight and shall include test push buttons (one for each level control), and moisture sensing alarm system consisting of necessary relays and warning light. In the event of a seal failure alarm the pump shall be shut down and remain inoperative until the seal is corrected. Circuit breaker, motor starter, reset buttons, and pump control H.O.A. switches shall be surface mounted for accessible operation without opening the high voltage panel. The low voltage pump control section shall be enclosed in a hinged section of the

panel and isolated from the high voltage section. All low voltage control wiring shall be accessible by a hinged drop shelf covering the control section. All external wiring shall terminate behind this panel. A grounding type convenience outlet shall be provided for operation of 127 volt AC devices and shall be protected by a 15 amp thermal magnetic circuit breaker.

- b. Circuit Breakers: Magnetic circuit breakers shall be provided for branch disconnect service and over-current protection against short circuits or grounds of motor branch circuit conductors, motor, controls and auxiliary equipment. Magnetic across-the-line starters with under voltage release and overload coils for each phase shall be provided for each pump motor to give positive protection against single phasing. All equipment control switches shall be labeled and a color coded wiring diagram shall be provided.
- c. Level Controls: The automatic operation of the pump shall be controlled by wet well mounted electrodes as manufactured by Warrick Co., or equal. Electrodes shall be series 3W brass, with 32 lb suspension wire, 32 lb adaptors, 3 x 38 fitting, Series 2 low voltage control relays shall be included in the control panel.
- d. Motor High Temperature Shutdown: The control shall be equipped with high temperature shutdown for motor and shall utilize the temperature switches embedded in the motor windings. In a high motor temperature condition, the switch shall open, de-energize the motor starter and stop the pump motor. The high motor temperature shutdown device shall be automatic reset.
- e. Seal Failure Shutdown: The control panel shall be equipped with a moisture detector control for pump which senses moisture in the oil cavity should the lower seal fail. Sensor probes located in the oil cavity will detect the influx of moisture and disrupt the motor starter circuit of the particular pump involved. Should this condition occur, the pump motor shall remain inoperative until the problem is corrected and the control circuit has been manually reset.

1.8 Running Light:

Include in the motor control panel a pilot light for pump motor which shall illuminate red light when the motor is running.

1.9 Wiring:

- a. The lift station shall be completely wired at the factory, except for the power feeder lines, in accordance with applicable wiring standards set forth by the National Electric Code (NEC). All wiring in the lift station shall be color coded and numbered as indicated on the wiring diagram.
- b. All components shall be electrically grounded to a common ground lug mounted on the control panel sub plate. Upon installation of the lift station, and before connection of any power feeder lines, Contractor shall extend grounding wire from lug to external ground in accordance with local electrical code.

2.0 Operational Test:

The pump, motor and controls shall be given an operational test in accordance with the standards of the Hydraulic Institute. Recordings of the test shall substantiate the operation of equipment at the design head, capacity, speed and horsepower as herein specified.

2.1 Operation and Maintenance Manuals:

Contractor shall provide 4 sets hardbound manuals to include the following for each component:

- a. Catalog
- b. Parts list
- c. Price list
- d. Wiring diagram
- e. Plan and details
- f. Performance curves
- g. Copies of operational test

100P01-713-3

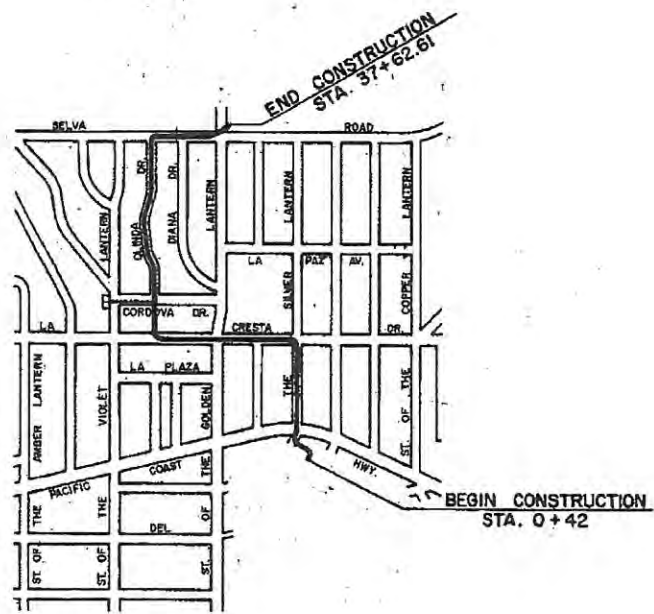
STORM DRAIN
AUXILIARY PUMP
STATION FOR
FACILITY LOOP01
SHEET 6 OF 6SHEETS

SD-095-06

EXHIBIT 4

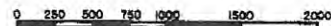
INDEX OF DRAWINGS

SHEET NO.	DRAWING TITLE
1.	TITLE SHEET
2.	PLAN & PROFILE, STA. 0+42 TO STA. 9+20
3.	PLAN & PROFILE, STA. 9+20 TO STA. 18+40
4.	PLAN & PROFILE, STA. 18+40 TO STA. 25+40
5.	PLAN & PROFILE, STA. 25+40 TO STA. 32+60
6.	PLAN & PROFILE, STA. 32+60 TO STA. 37+62.61
7.	INTERSECTION DETAILS - LA CRESTA DRIVE AT SILVER LANTERN CORDOVA DRIVE AT OLINDA DRIVE
8.	INTERSECTION DETAILS - SELVA ROAD AT OLINDA DRIVE CORDOVA DRIVE AT VIOLET LANTERN
9.	MAINLINE CONNECTOR PROFILES & DETAILS
10.	MAINLINE CONNECTOR PROFILES & DETAILS SEWER CONSTRUCTION DETAILS
11.	OUTLET STRUCTURE PLAN & DETAILS
12.	LOG OF BORINGS & BEDDING DETAIL



LOCATION MAP

SCALE: 1" = 600'



SCALE IN FEET

UTILITY OWNERS

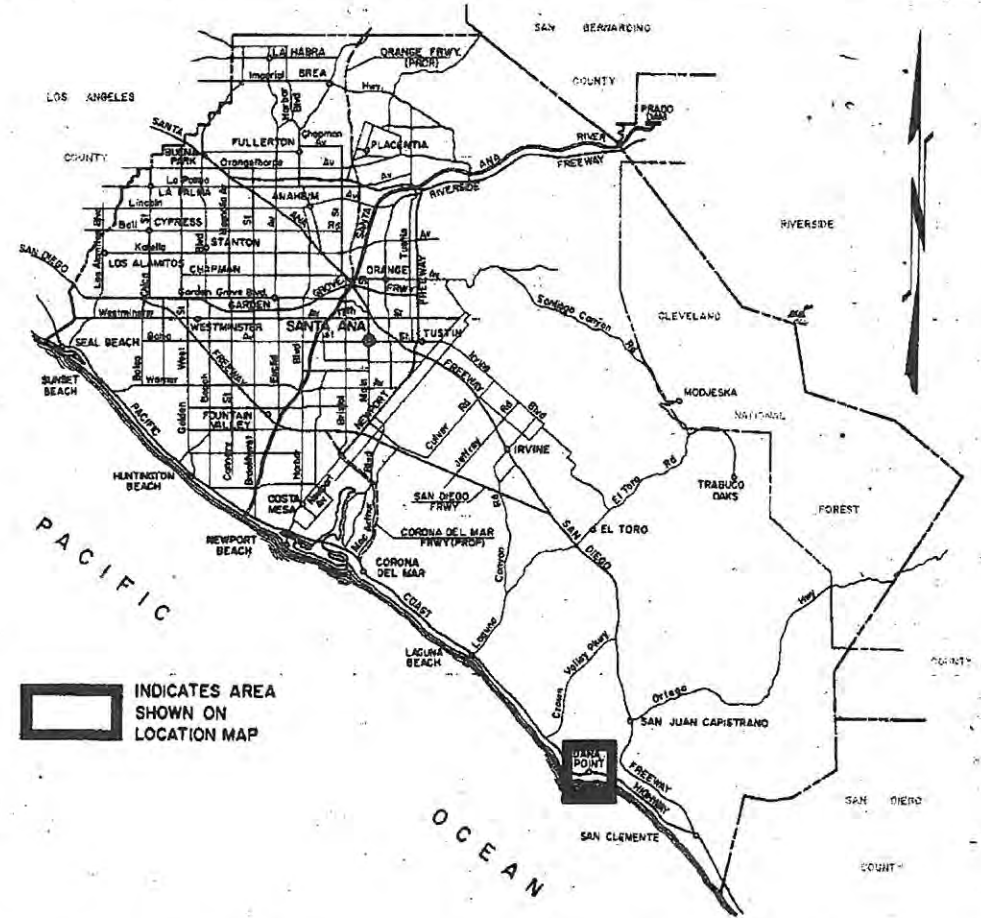
NAME	PHONE NO.
DANA POINT SANITARY DISTRICT	(714) 496-9322
SAN DIEGO GAS & ELECTRIC COMPANY	(714) 492-5111
SOUTHERN CALIFORNIA GAS COMPANY	(714) 538-0211
PACIFIC TELEPHONE COMPANY	(714) 557-1224
CAPISTRANO BEACH COUNTY WATER DISTRICT	(714) 496-5261
STORER CABLE TV INC.	(714) 493-1600

PREPARED BY THE STAFF OF



TOUPS CORPORATION
1010 NORTH MAIN STREET
SANTA ANA, CALIFORNIA 92711
TELEPHONE (714) 835-4447

SUBMITTED BY: *Donald Talley*
DONALD TALLEY R.E. 13,151



ORANGE COUNTY, CALIFORNIA VICINITY MAP



SCALE IN MILES

PLANS FOR
THE CONSTRUCTION OF
THAT PORTION OF

GOLDEN LANTERN STORM DRAIN

FROM
PACIFIC COAST HIGHWAY
TO
STREET OF THE GOLDEN LANTERN AT SELVA ROAD
FACILITY NO. LOOP01
AUGUST, 1975

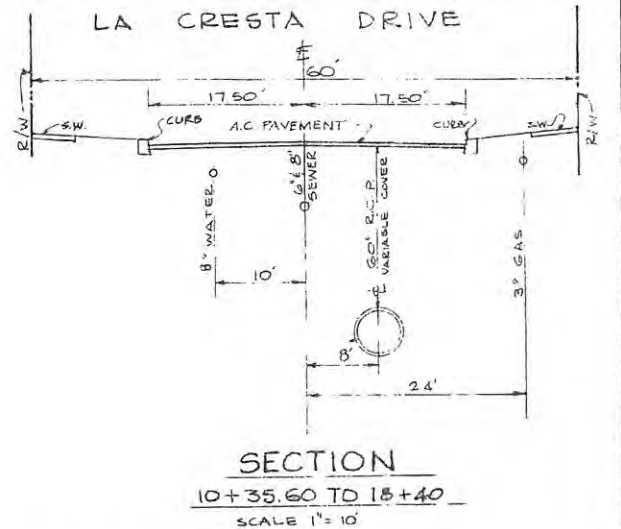
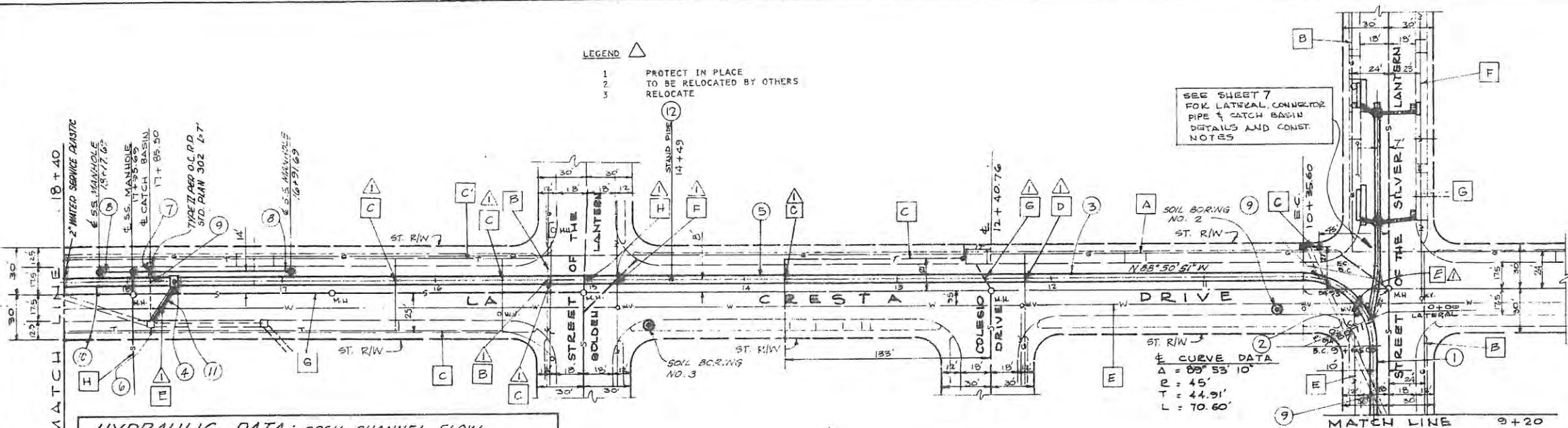
APPROVED: *C.R. Nelson*
ASSISTANT DIRECTOR

COUNTY OF ORANGE PROJECT
ADMINISTERED BY
ORANGE COUNTY FLOOD CONTROL DISTRICT
SANTA ANA CALIFORNIA

DWG. NO. LOOP01-713-2A

SHEET 1 OF 12 SHEETS
SP-015-01

EXHIBIT 5
SEP-1975



HYDRAULIC DATA: OPEN CHANNEL FLOW

STATION TO STATION	Q25 cfs	R.C.P. SIZE	S ₀	D _c	V _c	D _n	V _n
9+20 TO 9+80.30	285	51" φ	.0412	4.17'	20.2	2.96'	27.0
9+91.30 TO 10+35.60	240	60" φ	.0905	4.35'	13.2	1.90'	35.0
10+35.60 TO 17+65.00	240	60" φ	.0100	4.35'	13.2	3.79'	15.1
17+70.5 TO 17+95.00	230	54" φ	.0253	4.19'	14.9	3.87'	15.8

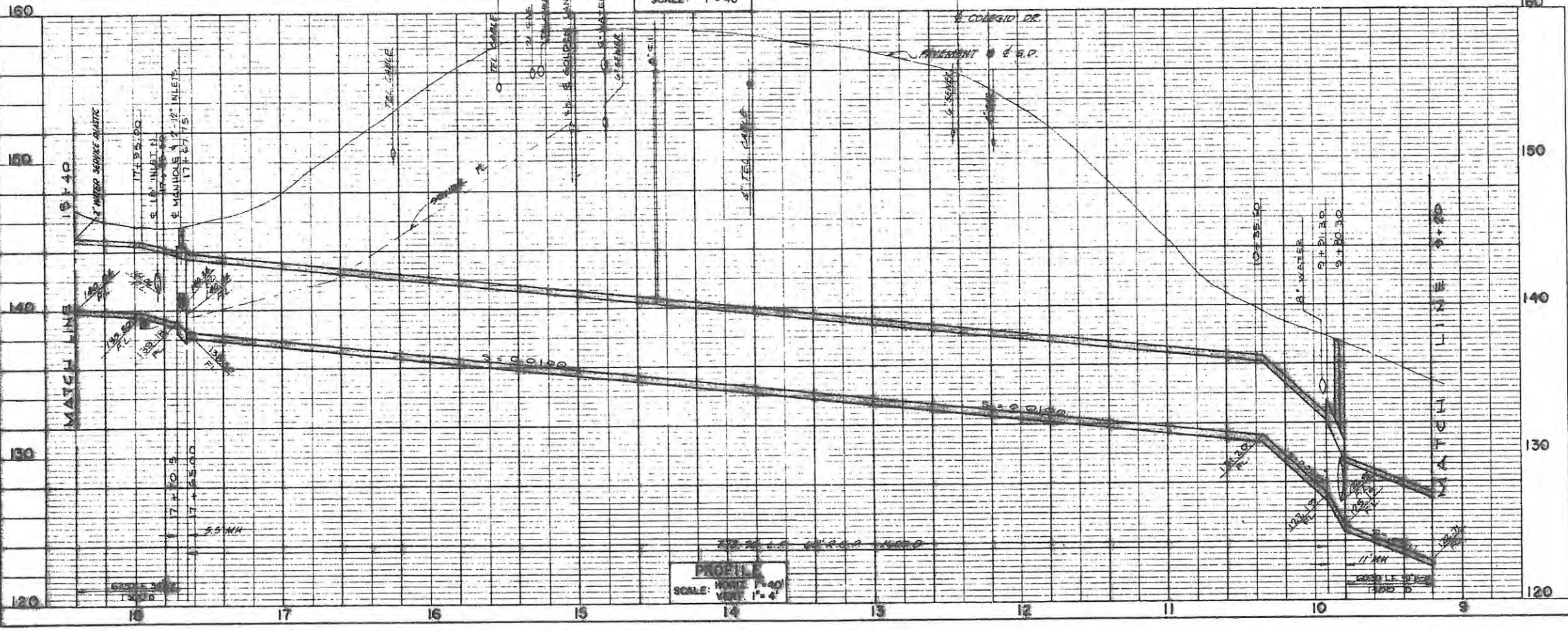
PRESSURE FLOW

V	S _f 17" O.D.	S _f 11" O.D.				
17+95 TO 18+40	230	54" φ	.0056	14.5	.0117	.0159

UTILITY NOTES

DESIGNATION	UTILITY	OWNER
A	3" GAS	SO CAL GAS CO.
B	2" GAS	SO CAL GAS CO.
C	4" TELEPHONE CABLE	PACIFIC TEL & TEL CO
D	4" GAS	SO CAL GAS CO.
E	8" WATER	CAPISTRANO BEACH CO. WATER DIST.
F	6" WATER	CAPISTRANO BEACH CO. WATER DIST.
G	6" SEWER	DANA POINT SAN. DIST.
H	8" SEWER	DANA POINT SAN. DIST.

- CONSTRUCTION NOTES**
- PLACE 51" R.C.P. 9+20 TO 9+80.30 PER PLAN, PROFILE AND SECTION.
 - CONSTRUCT MANHOLE PER O.C.F.C.D. STD. DWG. STD.-MH-1, A=11'-10", ANGLE A=30°, B=30", C=11'-0", EL. S=126.95', EL. R=127.05'.
 - PLACE 60" R.C.P. 9+91.30 TO 13+47.25 PER PLAN, PROFILE AND SECTION.
 - CONSTRUCT MANHOLE PER O.C.F.C.D. STD. DWG. STD.-MH-2-1.
 - PLACE 60" R.C.P. 13+52.75 TO 17+65.00 PER PLAN PROFILE AND SECTION.
 - REMOVE INTERFERING PORTIONS OF EXISTING CATCH BASIN. PLUG INLETS WITH DOUBLE COURSE OF 8" BRICK AND MORTAR AND FILL TO GRADE. CONSTRUCT INLET TYPE 1 PER O.C.R.D. STD. PLAN 301. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
 - CONSTRUCT 18" R.C.P. CONNECTOR. SEE PROFILE AND DETAILS SHEET 9.
 - CONSTRUCT SEWER LINES PER DETAILS SHEET 10.
 - REMOVE INTERFERING PORTION OF 18" R.C.P.
 - PLACE 54" R.C.P. 17+70.50 TO 18+46.00 PER PLAN, PROFILE AND SECTION.
 - CONSTRUCT DOUBLE 12" R.C.P. CONNECTOR. SEE PROFILE AND DETAILS SHEET 9.
 - CONSTRUCT STAND-PIPE WITH 8" C.T. PIPE (CLASS 25) PER DETAIL SHEET 10.



DATUM OCFCO = OCS 1970 ADJUSTMENT
 BENCH MARK: OCS S-783-70 ELEV. 122.975

0.8 MILES WEST ALONG PACIFIC COAST HIGHWAY FROM THE ATCHISON TOPEKA RAILWAY OVERPASS AT DHERNEY PARK, AT THE '1' INTERSECTION OF ALCAZAR DRIVE, 35 FEET NORTH OF THE CENTERLINE OF THE NORTH LANES OF THE HIGHWAY, 0.5 FOOT NORTH OF THE NORTH EDGE OF THE SIDEWALK, 0.4 FOOT EAST OF THE EAST EDGE OF THE EAST CURVE OF DRIVE, ABOUT 1 FOOT HIGHER THAN THE HIGHWAY, PLUSH WITH THE GROUND, AND SET IN THE TOP OF A CONCRETE POST.

3 inches on original drawing

DATE	DESCRIPTION

GOLDEN LANTERN STORM DRAIN

PLAN & PROFILE

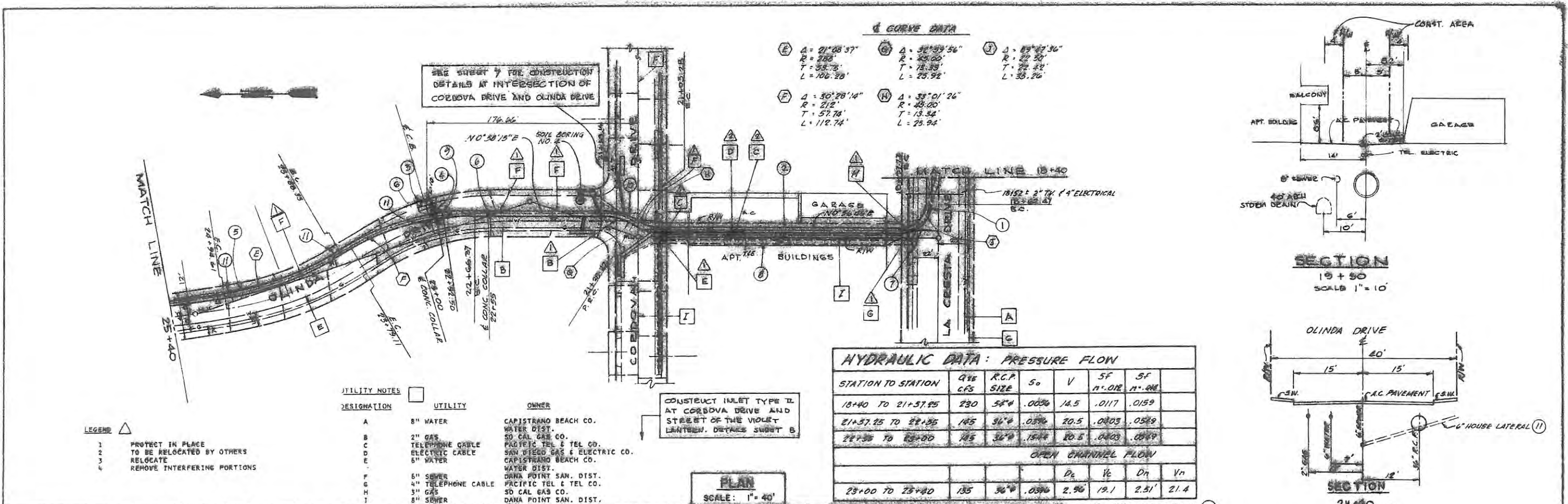
STA 9+20 TO STA. 18+40

SCALE: HORIZ. 1"=40'
 VERT. 1"=4'

EXHIBIT 5

PLAN
 SURVEYED
 PLOTTED
 GRADES CHECKED
 NOTE BOOK
 STRUCTURE ROTATING CHECKED

DATE
 BY
 PROFILE
 SURVEYED
 PLOTTED
 GRADES CHECKED
 NOTE BOOK
 STRUCTURE ROTATING CHECKED



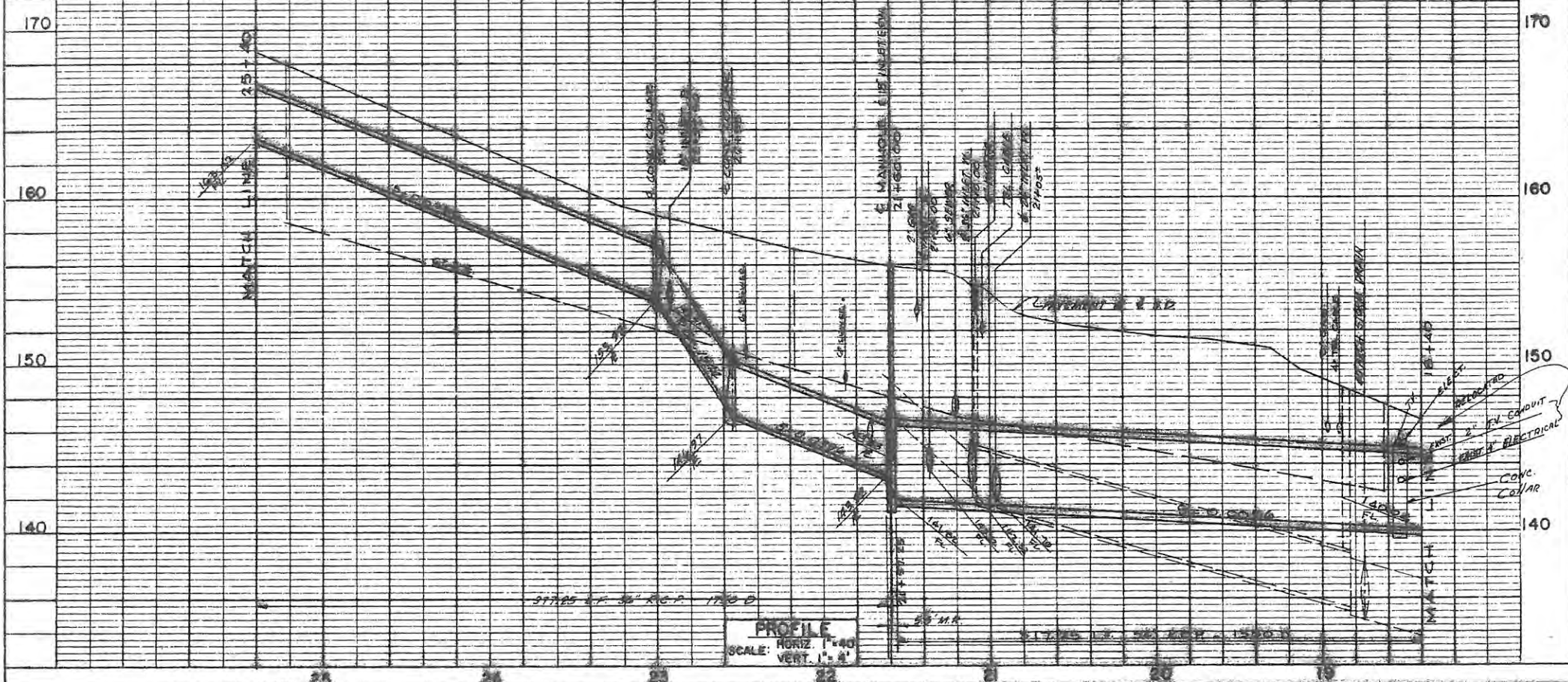
UTILITY NOTES

DESIGNATION	UTILITY	OWNER
A	8" WATER	CAPISTRANO BEACH CO. WATER DIST.
B	2" GAS	SO CAL GAS CO.
C	TELEPHONE CABLE	PACIFIC TEL & TEL CO.
D	ELECTRIC CABLE	SAN DIEGO GAS & ELECTRIC CO.
E	6" WATER	CAPISTRANO BEACH CO. WATER DIST.
F	6" SEWER	DRNA POINT SAN. DIST.
G	4" TELEPHONE CABLE	PACIFIC TEL & TEL CO.
H	3" GAS	SO CAL GAS CO.
I	8" SEWER	DANA POINT SAN. DIST.

- LEGEND**
- 1 PROTECT IN PLACE TO BE RELOCATED BY OTHERS
 - 2 RELOCATE
 - 3 REMOVE INTERFERING PORTIONS

CONSTRUCT INLET TYPE II AT CORDOVA DRIVE AND STREET OF THE VIOLET LANTERN. DETAIL SHEET B

PLAN
 SCALE: 1" = 40'



- CONSTRUCTION NOTES**
- PLACE 54" R.C.P. 17+70.5 TO 21+57.25 PER PLAN, PROFILE AND SECTION.
 - RESTORE TO ORIGINAL CONDITION, ALL EXISTING IMPROVEMENTS (LOCATED BETWEEN CORDOVA DRIVE AND LA CRESTA DRIVE). A) DRIVEWAY APPROACH AT CORDOVA, B) DRIVEWAY APPROACH AT LA CRESTA, C) TWO SPEED BUMPS, D) EXISTING A.C. PAVEMENT.
 - CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLAN 302. L=10.0', H=3.5'. CONNECTOR PIPE CONNECTION PER L.A.C.F.C.D. STD. DWG. 2-D224. LOCAL DEPRESSION PER DETAIL SHEET 10. (C.L.D. MODIFIED 3/18/85)
 - CONSTRUCT 18" R.C.P. CONNECTOR. SEE PROFILE AND DETAILS SHEET 9.
 - PLACE 36" R.C.P. 21+62.75 TO 25+40.00 PER PLAN, PROFILE AND SECTION.
 - CONSTRUCT CONCRETE COLLAR PER L.A.C.F.C.D. STD. DWG. NO. 2-Q393.
 - PLUG INLET AND OUTLET OF MANHOLE WITH A DOUBLE COURSE OF 8" BRICK AND MORTAR. REMOVE TOP 2' OF STRUCTURE AND FILL REMAINING STRUCTURE WITH SAND. BACKFILL TOP 2' WITH NATIVE MATERIAL TO MATCH SURROUNDING GROUND.
 - FILL 40" ARCH CONDUIT WITH 3/8" X NO. 4 AGGREGATE BETWEEN NORTH FACE OF MANHOLE AT LA CRESTA DRIVE AND SOUTHERLY RIGHT-OF-WAY LINE OF CORDOVA DRIVE. PROVIDE A BRICK AND MORTAR PLUG AT UPSTREAM END.
 - CONSTRUCT JUNCTION STRUCTURE PER L.A.C.F.C.D. STD. DWG. 2-D112. A=39°, B=18", C=2.7', D=36".
 - REMOVE INTERFERING PORTION OF 24" R.C.P. CONNECTOR.
 - RECONSTRUCT 6" HOUSE LATERALS PER O.C.S.D. STANDARD DRAWING 3-.
- DATUM OCPD = OCS 1970 ADJUSTMENT
 BENCH MARK: OCS 5-783-70 ELEV. 122.975

0.8 MILES WEST ALONG PACIFIC COAST HIGHWAY FROM THE ATCHISON TOPEKA RAILWAY OVERPASS AT BONEHEE PARK, AT THE INTERSECTION OF ALCAZAR DRIVE, 35 FEET NORTH OF THE CENTERLINE OF THE NORTH LANES OF THE HIGHWAY, 0.5 FOOT NORTH OF THE NORTH EDGE OF THE SIDEWALK, 0.4 FOOT EAST OF THE EAST EDGE OF THE EAST CURB OF DRIVE, ABOUT 1 FOOT HIGHER THAN THE HIGHWAY, FLUSH WITH THE GROUND, AND SET IN THE TOP OF THE CONCRETE POST.

3 inches on original drawing

REVISIONS		GOLDEN LANTERN STORM DRAIN	
NO.	DATE	DESCRIPTION	

PLAN & PROFILE
 STA. 18+40 TO STA. 25+40

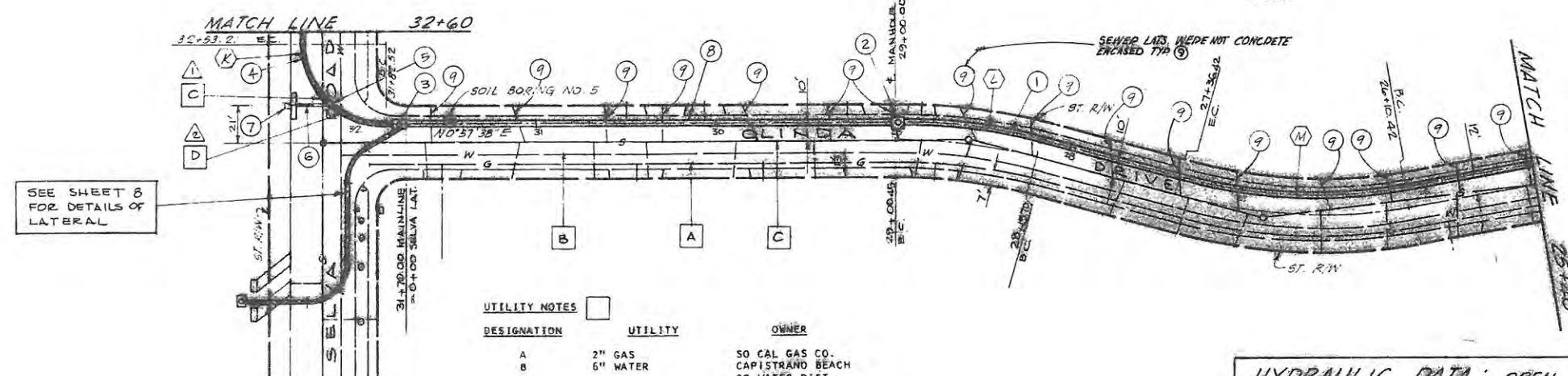
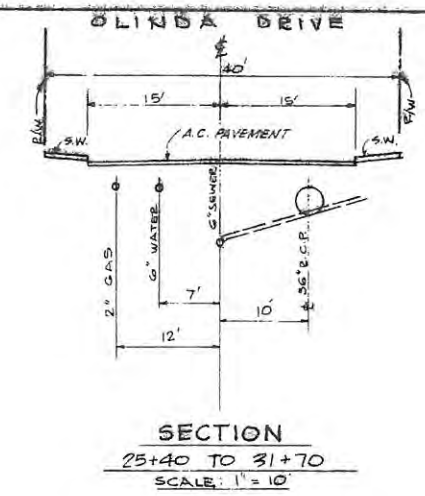
EXHIBIT 5

PLAN
 V.P. DATE: 8/1/75
 ROUTE: 101
 NOTE BOOK: 101-101
 NO. 101-101

PROFILE
 V.P. DATE: 8/1/75
 ROUTE: 101
 NOTE BOOK: 101-101
 NO. 101-101

CURVE DATA

(K)	$\Delta = 90^{\circ}00'49"$	(M)	$\Delta = 24^{\circ}58'55"$
	$R = 35'$		$R = 269'$
	$T = 25.01'$		$T = 62.02'$
	$L = 70.69'$		$L = 126.00'$
(L)	$\Delta = 15^{\circ}39'55"$		
	$R = 310'$		
	$T = 42.64'$		
	$L = 84.75'$		



UTILITY NOTES

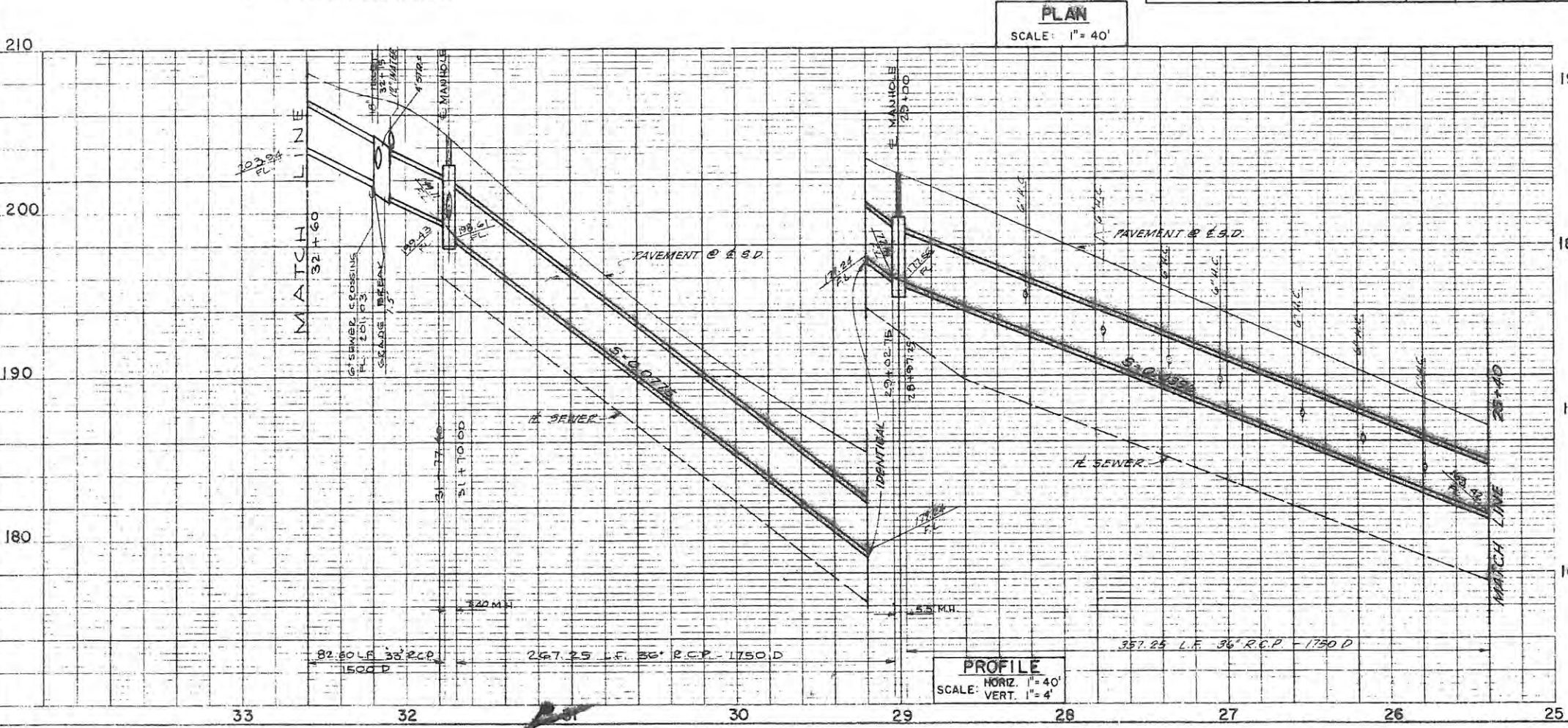
DESIGNATION	UTILITY	OWNER
A	2" GAS	SO CAL GAS CO.
B	6" WATER	CAPISTRANO BEACH CO WATER DIST.
C	6" SEWER	DANA POINT SAN. DIST.
D	4" WATER	CAPISTRANO BEACH CO WATER DIST.

HYDRAULIC DATA: OPEN CHANNEL FLOW

STATION TO STATION	Q ₂₅ CFS	R.C.P. SIZE	S ₀	D _c	V _c	D _n	V _n
25+40 TO 29+00	135	36"φ	.0396	2.96'	19.1	2.51'	21.4
29+00 TO 31+70	135	36"φ	.0775	2.96'	19.1	1.89'	28.8
31+77.4 TO 32+14	100	33"φ	.0775	2.71'	16.9	1.66'	26.6
32+14 TO 32+60	100	33"φ	.0362	2.71'	16.9	2.24'	19.3

- CONSTRUCTION NOTES**
- 1 PLACE 36" R.C.P. 25+40.00 TO 28+97.25 PER PLAN, PROFILE AND SECTION.
 - 2 CONSTRUCT MANHOLE PER O.C.F.C.D. STD. DWG. STD.-MH2-1.
 - 3 CONSTRUCT MANHOLE PER O.C.F.C.D. STD. DWG. STD.MH2-1 A=8.23', ANGLE A=30°, B=24", C=7.3', E1.S.=199.11', EL. R=199.23'.
 - 4 PLACE 33" R.C.P. 32+77.40 TO 32+60 PER PLAN, PROFILE AND SECTION.
 - 5 CONSTRUCT JUNCTION STRUCTURE MH-1 (LESS MH.)
 - 6 CONSTRUCT 18" R.C.P. CONNECTOR, SEE PROFILE AND DETAILS SHEET 9.
 - 7 CONSTRUCT INLET TYPE I PER O.C.R.D. STD. PLAN 301, H=3.5'. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
 - 8 PLACE 36" R.C.P. 29+02.75 TO 31+70.00 PER PLAN, PROFILE AND SECTION.
 - 9 RECONSTRUCT 6" HOUSE LATERALS PER O.C.S.D. STD. DRAWING S-.

- LEGEND**
- 1 PROTECT IN PLACE
 - 2 TO BE RELOCATED BY OTHERS



DATUM OCFCD = OCS 1970 ADJUSTMENT
 BENCH MARK: OCS S-783-70 ELEV. 122.975
 0.8 MILES WEST ALONG PACIFIC COAST HIGHWAY FROM THE ATCHISON TOPEKA RAILWAY OVERPASS AT BONEHEEY PARK, AT THE 'T' INTERSECTION OF ALCAZAR DRIVE, 35 FEET NORTH OF THE CENTERLINE OF THE NORTH LANES OF THE HIGHWAY, 0.5 FOOT NORTH OF THE NORTH EDGE OF THE SIDEWALK, 0.4 FOOT EAST OF THE EAST EDGE OF THE EAST CURB OF DRIVE, ABOUT 1 FOOT HIGHER THAN THE HIGHWAY, FLUSH WITH THE GROUND, AND SET IN THE TOP OF A CONCRETE POST.

3 inches on original drawing

PRELIMINARY REVISION CODE		DISREGARD PRINTS BEARING EARLIER CODES	
REVISIONS		ORANGE COUNTY FLOOD CONTROL DISTRICT	
MARK	DATE	DESCRIPTION	GOLDEN LANTERN STORM DRAIN
		PLAN & PROFILE	
		STA. 25+40 TO STA. 32+60	
DESIGNED BY	RECOMMENDED	DRAWN BY	
CHECKED BY	DATE	SCALE AS SHOWN	
SUBMITTED BY	DATE	DWG. NO. LOOP01-713-24	

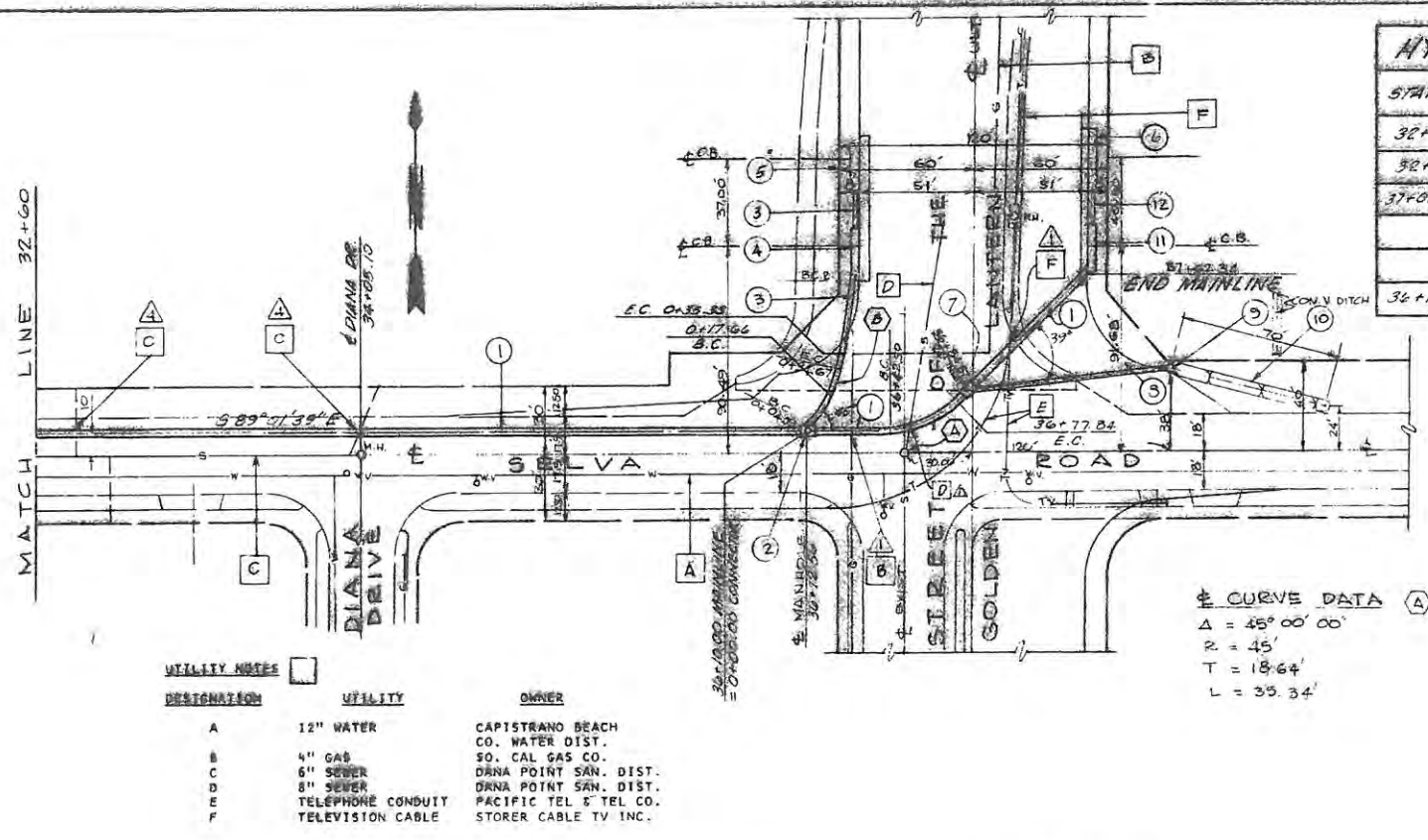
PROFILE
 HORIZ. 1"=40'
 VERT. 1"=4'

EXHIBIT 5

DATE: _____ BY: _____
 CHECKED: _____
 NOTE BOOK: _____
 NO. _____

DATE: _____ BY: _____
 CHECKED: _____
 NOTE BOOK: _____
 NO. _____

DATE: _____ BY: _____
 CHECKED: _____
 NOTE BOOK: _____
 NO. _____



UTILITY NOTES

DESIGNATION	UTILITY	OWNER
A	12" WATER	CAPISTRANO BEACH CO. WATER DIST.
B	4" GAS	SO. CAL GAS CO.
C	6" SEWER	DRNA POINT SAN. DIST.
D	8" SEWER	DRNA POINT SAN. DIST.
E	TELEPHONE CONDUIT	PACIFIC TEL & TEL CO.
F	TELEVISION CABLE	STORER CABLE TV INC.

- LEGEND**
- 1 PROTECT IN PLACE
 - 2 TO BE RELOCATED BY OTHERS
 - 3 RELOCATE
 - 4 REMOVE INTERFERING PORTIONS

± CURVE DATA (A)

Δ = 45° 00' 00"
 R = 45'
 T = 18.64'
 L = 35.34'

± CURVE DATA (B)

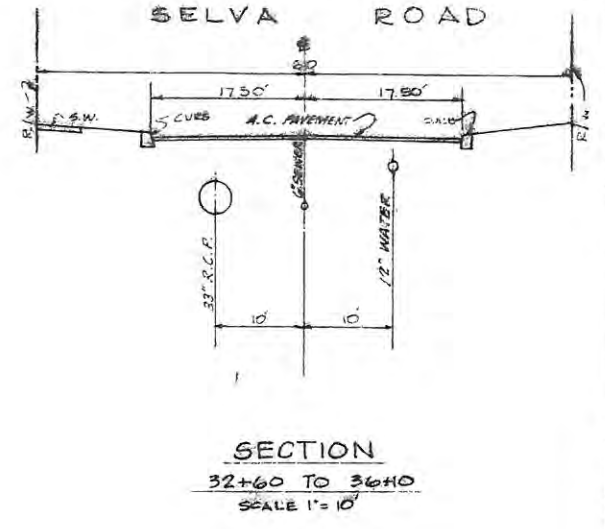
Δ = 38° 58' 21"
 R = 45'
 T = 15.91'
 L = 30.58'

HYDRAULIC DATA: OPEN CHANNEL FLOW

STATION TO STATION	Q ₂₅ CFS	R.C.P. SIZE	S ₀	D ₀	V ₀	D _N	V _N
32+60 TO 32+80	100	33" Ø	.0362	2.11'	16.9	2.24'	19.3
32+80 TO 36+09	100	33" Ø	.0580	2.11'	16.9	1.85'	23.8
37+01.6 TO 37+62.61	40	33" Ø	.0580	2.10'	8.2	1.06'	19.0

PRESSURE FLOW

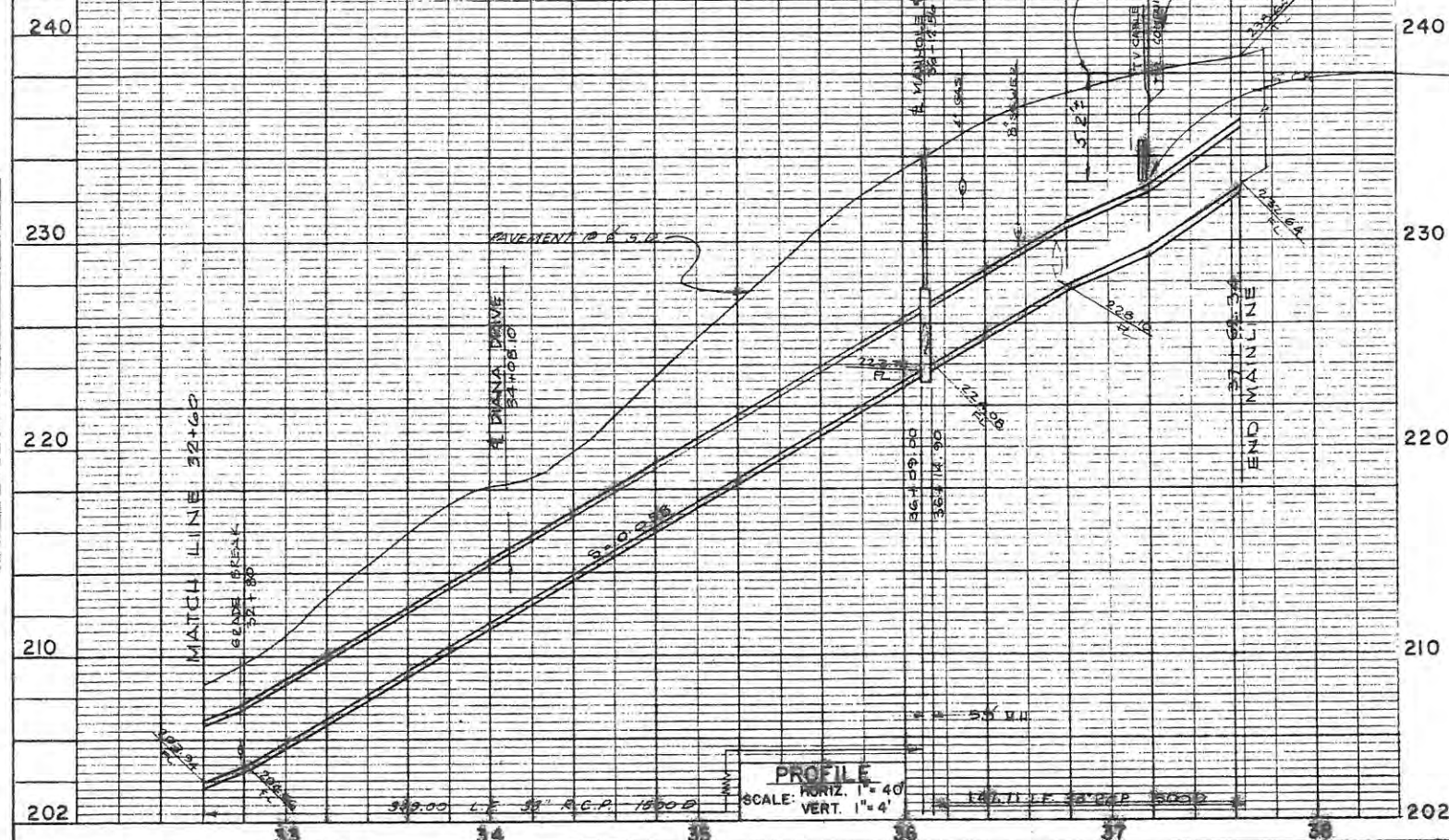
STATION TO STATION	Q ₂₅ CFS	R.C.P. SIZE	S ₀	D ₀	V ₀	D _N	V _N
34+14.20 TO 34+98.40	70	33" Ø	.0580	2.10'	11.8	1.019'	12.018'



- CONSTRUCTION NOTES**
- PLACE 33" R.C.P. 32+60 TO 37+62.61, PER PLAN, PROFILE AND SECTION.
 - CONSTRUCT MANHOLE PER O.C.F.C.D. STD. DWG. STD. MH-1 A=6.7', ANGLE A=45° B=21", C=5.0', E1.5=224.21, EL. R=224.51'.
 - CONSTRUCT 21" R.C.P. CONNECTOR. SEE PROFILE AND DETAILS SHEET 9.
 - CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLAN 302. L=21', H=5.5'. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
 - CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLAN 302. L=21', H=3.5'. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
 - CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLAN 302. L=28', H=3.5'. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
 - CONSTRUCT JUNCTION STRUCTURE PER L.A.C.F.C.D. STD. DWG. 2-D112. A=39°, B=24", C=3.1', D=33".
 - CONSTRUCT 24" R.C.P. CONNECTOR. SEE PROFILE AND DETAILS SHEET 10.
 - CONSTRUCT DROP INLET PER O.C.F.C.D. STD. DWG. STD.-D11-1. MODIFY TO PROVIDE 18" OPENING FOR 180 DEGREES. SEE DETAIL SHEET 10. EL. A=236.92 D₁=36", D₂=24", L₁=4.20', L₂=5.0'.
 - CONSTRUCT SWALE PER DETAILS SHEET 10.
 - CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLAN 302. L=21', H=6.0'. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
 - CONSTRUCT 21" R.C.P. CONNECTOR. SEE PROFILE AND DETAILS SHEET 10.

PLAN
 SCALE: 1" = 40'

PROFILE
 SCALE: HORIZ. 1" = 40'
 VERT. 1" = 4'



DATUM OCFCD = OCS 1970 ADJUSTMENT
 BENCH MARK: OCS S-783-70 ELEV. 122.975

0.8 MILES WEST ALONG PACIFIC COAST HIGHWAY FROM THE ATCHISON TOPEKA RAILWAY OVERPASS AT DOHENEY PARK, AT THE 'T' INTERSECTION OF ALCAZAR DRIVE, 35 FEET NORTH OF THE CENTERLINE OF THE NORTH LANES OF THE HIGHWAY, 0.5 FOOT NORTH OF THE NORTH EDGE OF THE SIDEWALK, 0.4 FOOT EAST OF THE EAST EDGE OF THE EAST CURB OF DRIVE, ABOUT 1 FOOT HIGHER THAN THE HIGHWAY, FLUSH WITH THE GROUND, AND SET IN THE TOP OF A CONCRETE POST.

1 1/2 0 2
 3 inches on original drawing

PRELIMINARY REVISION CODE		Disregard Prints Bearing Earlier Codes	
MARK	DATE	DESCRIPTION	

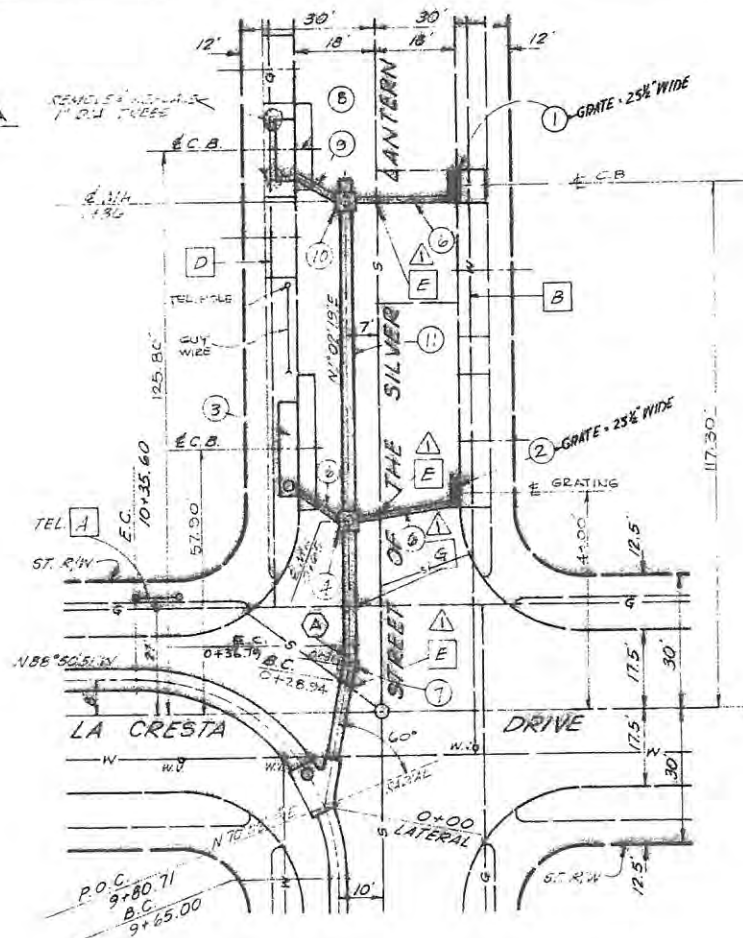
ORANGE COUNTY FLOOD CONTROL DISTRICT
GOLDEN LANTERN STORM DRAIN
PLAN & PROFILE
 STA. 32+60 TO STA. 37+62.34

DESIGNED: J.J. [Signature]
 DRAWN: [Signature] CHECKED: [Signature]
 SUBMITTED: [Signature]

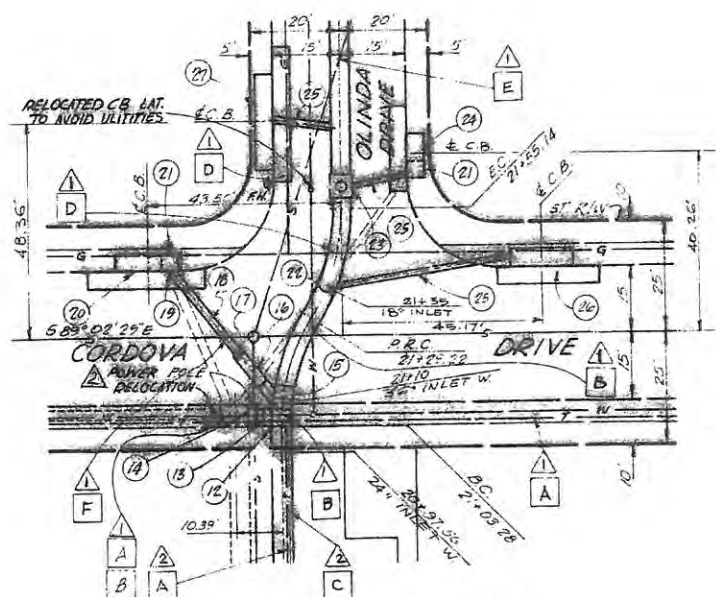
RECOMMENDED: [Signature]
 DESIGN DIVISION ENGINEER

SCALE: AS SHOWN DATE: AUG. 75 DWG. NO.: LOOP01-713-24

Δ CURVE DATA
 $\Delta = 10^{\circ} 00' 00''$
 $R = 45.00'$
 $T = 3.94'$
 $L = 7.85'$



**INTERSECTION PLAN
 SILVER LANTERN - LA CRESTA DRIVE**
 SCALE: 1" = 20'



**INTERSECTION PLAN
 OLINDA DRIVE - CORDOVA DRIVE**
 SCALE: 1" = 20'

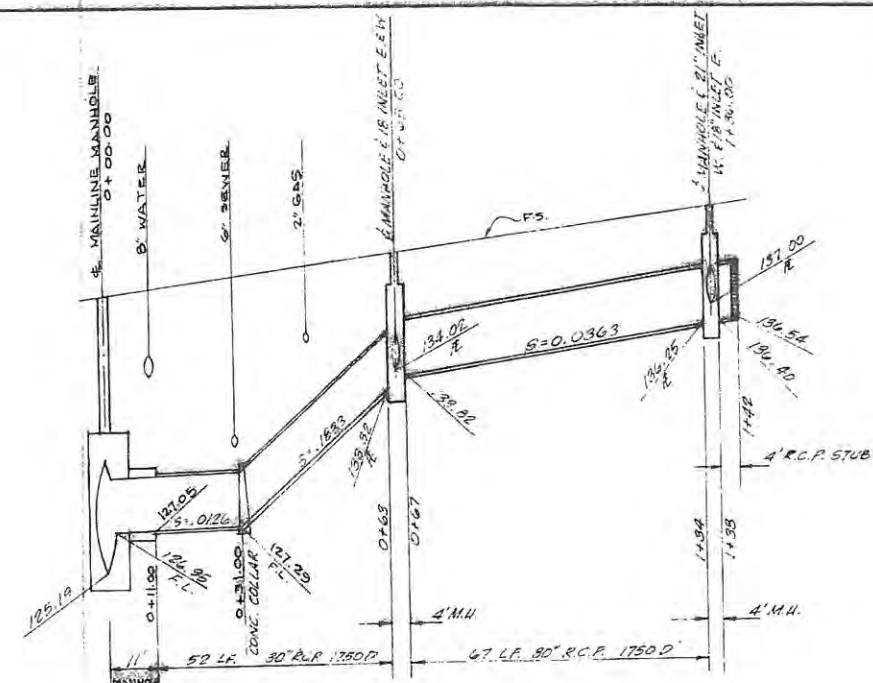
CONSTRUCTION NOTES

- 1 CONSTRUCT INLET TYPE IV PER O.C.R.D. STD PLAN 304, L=6.3', H=3.5' (2 GRATINGS).
- 2 CONSTRUCT INLET TYPE IV PER O.C.R.D. STD. PLAN 304 WITH 2 GRATINGS MODIFIED TO ELIMINATE SIDE OPENING. REDUCE WIDTH TO CONFORM TO MODIFICATION.
- 3 CONSTRUCT INLET TYPE II PER O.C.R.D. STD PLAN 302, L=21', H=3.5'. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
- 4 CONSTRUCT MANHOLE PER O.C.F.C.D. STD. DWG. NO. STD-MH-1.
- 5 CONSTRUCT CONCRETE COLLAR PER L.A.C.F.C.D. STD DWG. NO. 2-D393.
- 6 CONSTRUCT 18" R.C.P. CONNECTOR PER PROFILE THIS SHEET.
- 7 CONSTRUCT CONCRETE COLLAR PER L.A.C.F.C.D. STD. DWG. 2-D393.
- 8 CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLAN 302, L=14', H=4.0'. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
- 9 CONSTRUCT 21" R.C.P. PER PROFILE THIS SHEET.
- 10 CONSTRUCT MANHOLE PER O.C.F.C.D. STD DWG. NO. STD-MH-1. PROVIDE A 4 FOOT 30" R.C.P. STUB AT UPSTREAM END OF MANHOLE. SEAL END OF R.C.P. WITH A DOUBLE COURSE OF 8" BRICK AND MORTAR.
- 11 PLACE 30" R.C.P. PER PLAN AND PROFILE THIS SHEET.
- 12 CONSTRUCT JUNCTION STRUCTURE PER L.A.C.F.C.D. STD DWG. NO. 2-D112, A=4.5', B=24", C=2.7', D=54", E1.5=141.70'
- 13 CONSTRUCT 24" R.C.P. CONNECTOR PER PROFILE SHEET 9.
- 14 CONNECT 24" R.C.P. CONNECTOR TO EXISTING CATCH BASIN PER L.A.C.F.C.D. STD DWG. NO. 2-D224. SEE DETAILS, SHEET 9.
- 15 CONSTRUCT JUNCTION STRUCTURE PER L.A.C.F.C.D. STD DWG. NO. 2-D112, A=41.5', B=36", C=4.4', D=54"
- 16 CONSTRUCT 36" R.C.P. SEE PROFILES AND DETAILS SHEET 9.
- 17 CONSTRUCT CONCRETE COLLAR PER L.A.C.F.C.D. STD DWG. NO. 2-D393.
- 18 CONSTRUCT 30" R.C.P. SEE PROFILES AND DETAILS SHEET 9.
- 19 CONNECT 27" R.C.P. TO CATCH BASIN PER L.A.C.F.C.D. STD. DWG. NO. 2-D224.
- 20 CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLAN 302, L=14', H=4.5'; MODIFY PER L.A.C.F.C.D. STD. DWG. 2-D461. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
- 21 REMOVE INTERFERING PORTIONS OF EXISTING CATCH BASIN. PLUG INLETS WITH DOUBLE COURSE OF 8" BRICK & MORTAR AND FILL TO GRADE.
- 22 CONSTRUCT JUNCTION STRUCTURE PER L.A.C.F.C.D. STD DWG. NO. 2-D193.
- 23 CONSTRUCT MANHOLE PER O.C.F.C.D. STD DWG. NO. STD-MH-1.
- 24 CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLANS 302, L=10', H=7.0'. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
- 25 CONSTRUCT 18" R.C.P. CONNECTOR. SEE PROFILE SHEET 9.
- 26 CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLANS 302, L=7', H=3.5'; MODIFY PER L.A.C.F.C.D. STD. DWG. 2-D461. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.
- 27 CONSTRUCT INLET TYPE II PER O.C.R.D. STD. PLANS 302, L=21', H=8.0'. CONSTRUCT LOCAL DEPRESSION PER DETAIL SHEET 10.

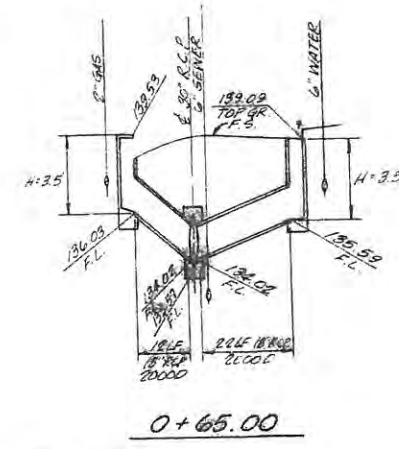
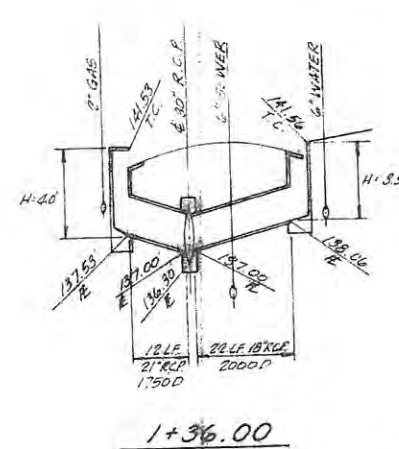
- LEGEND**
- 1 PROTECT IN PLACE
 - 2 TO BE RELOCATED BY OTHERS
 - 3 RELOCATE
 - 4 REMOVE INTERFERING PORTIONS

UTILITY NOTES

DESIGNATION	UTILITY	OWNER
A	TELEPHONE CABLE	PACIFIC TEL & TEL CO.
B	6" WATER	CAPISTRANO BEACH CO. WATER DISTRICT
C	ELECTRIC CABLE	SO CAL EDISON CO.
D	2" GAS	SO CAL GAS CO.
E	6" SEWER	DANA POINT SANITARY DIST.
F	8" SEWER	DANA POINT SANITARY DIST.
G	3" GAS	SO CAL GAS CO.



SILVER LANTERN LATERAL
 SCALE: HORIZ. 1" = 20'
 VERT. 1" = 4'



SCALE: HORIZ. 1" = 20'
 VERT. 1" = 4'

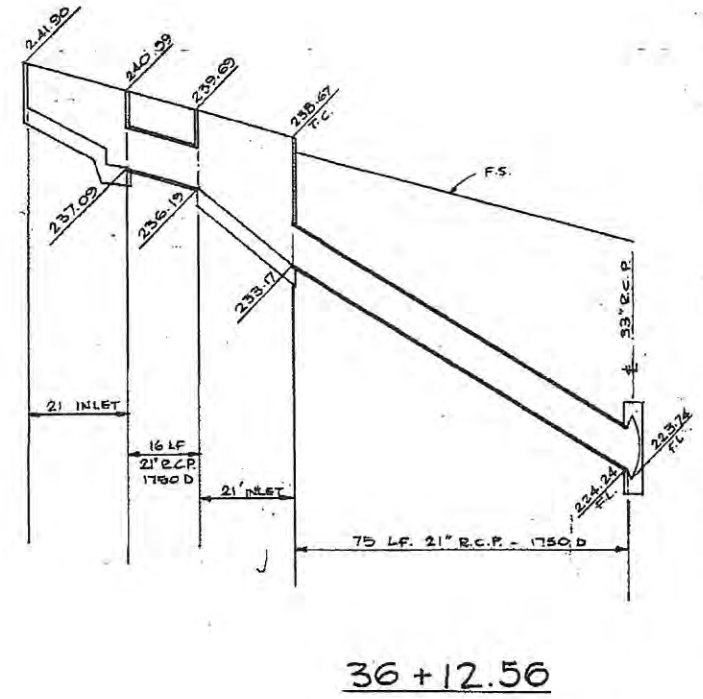
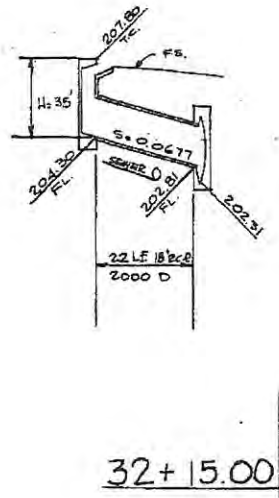
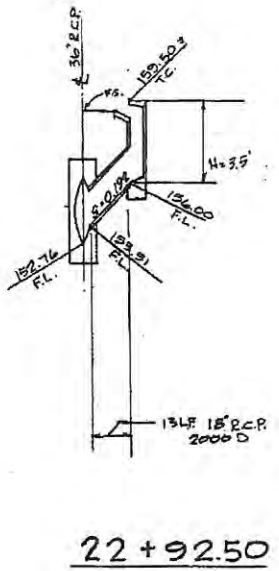
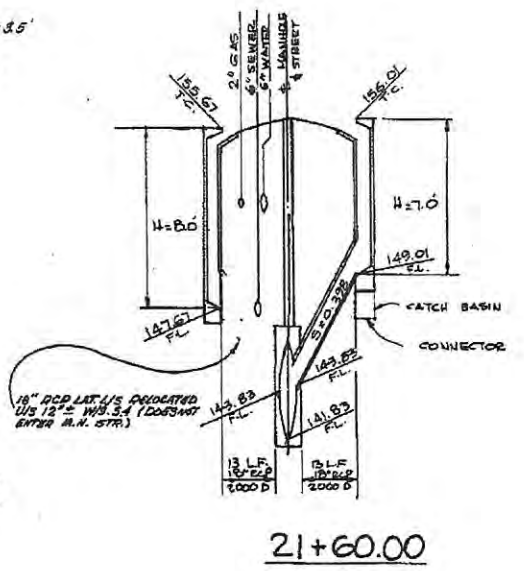
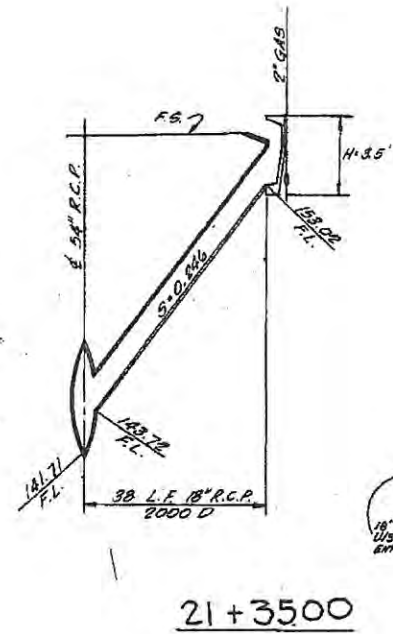
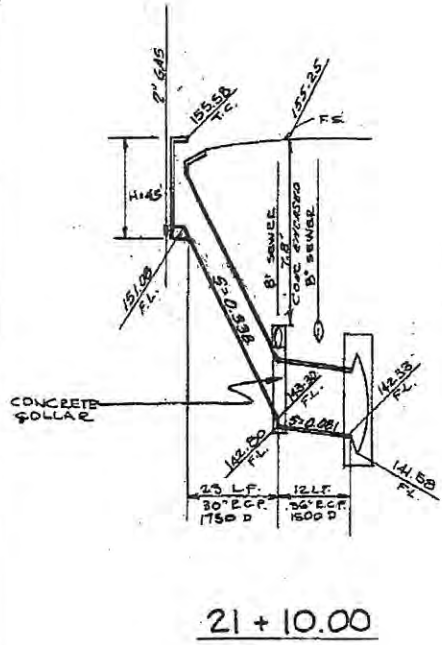
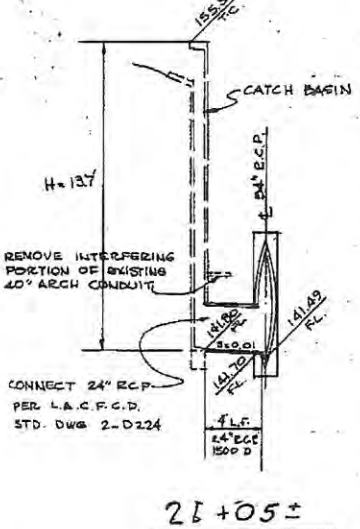
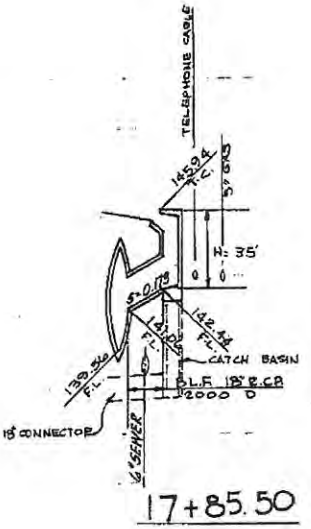
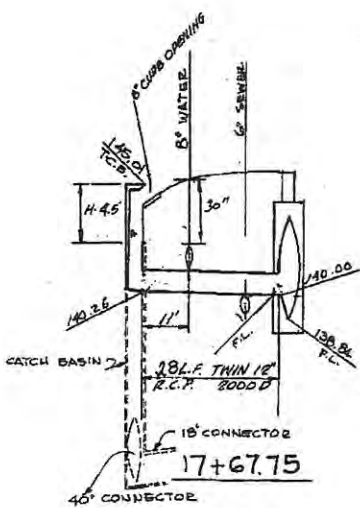
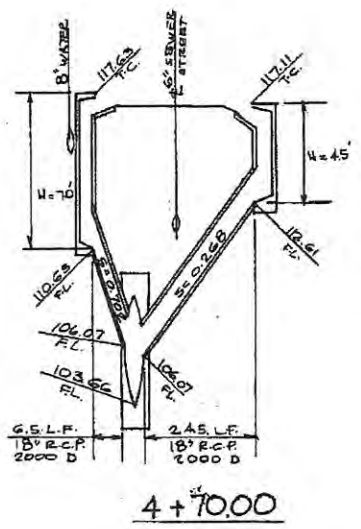
3 inches on original drawing

DATE	REVISIONS	DESCRIPTION

OWNER: GOLDEN LANTERN STORM DRAIN
 INTERSECTION DETAILS
 LA CRESTA DRIVE AT SILVER LANTERN
 CORDOVA DRIVE AT OLINDA DRIVE

SUBMITTED: 1.01
 SCALE: AS SHOWN
 DATE: AUG. 76
 DWG. NO.: LOOP01-713-2A

EXHIBIT 5



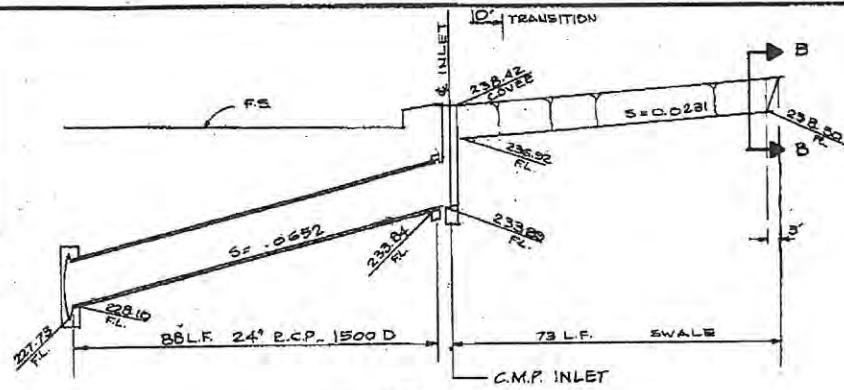
MAINLINE CONNECTORS PROFILES

SCALE: 1" = 20' HORIZ.
1" = 4' VERT.

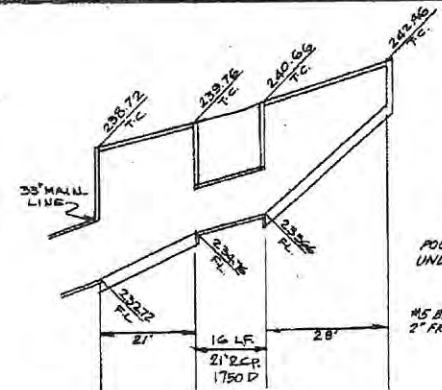
1/2" 0 2
3 inches on original drawing

PRELIMINARY REVISION CODE		ORANGE COUNTY FLOOD CONTROL DISTRICT	
Disregard Prints Bearing Earlier Codes		REVISIONS	
MARK	DATE	DESCRIPTION	
DESIGNED: J.T.	RECOMMENDED: J.M.M.	DESIGN DIVISION ENGINEER	
DRAWN: M.M.	CHECKED: M.A.C.	SCALE: AS SHOWN	DATE: AUG. 75
SUBMITTED: J.P. Valley	DESIGNER ENGINEER	DWG. NO. LOOP01-713-2A	

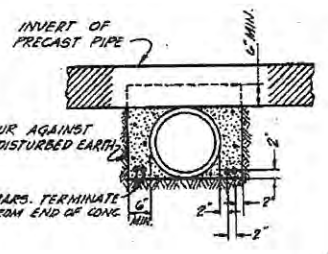
EXHIBIT 5



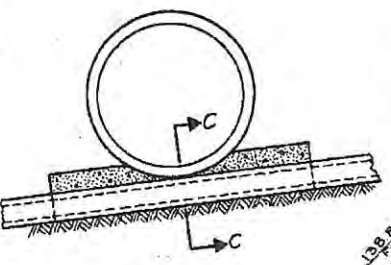
**37+00.00
CONNECTOR PROFILE**
SCALE: 1" = 20' HORIZ.
1" = 4' VERT.



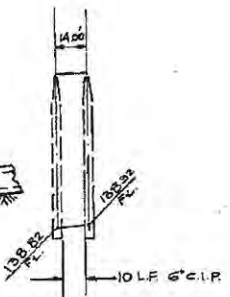
**37+62.61
CONNECTOR PROFILE**
SCALE: 1" = 20' HORIZ.
1" = 4' VERT.



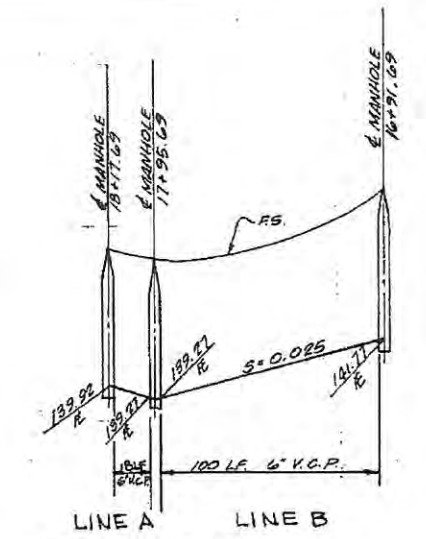
**SECTION C-C
SEWER ENCASEMENT DETAIL**
NO SCALE



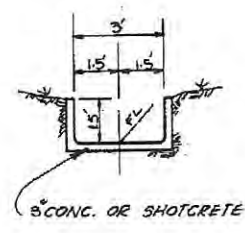
PLAN



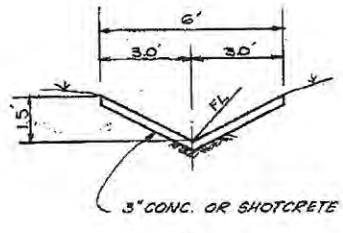
LINE C



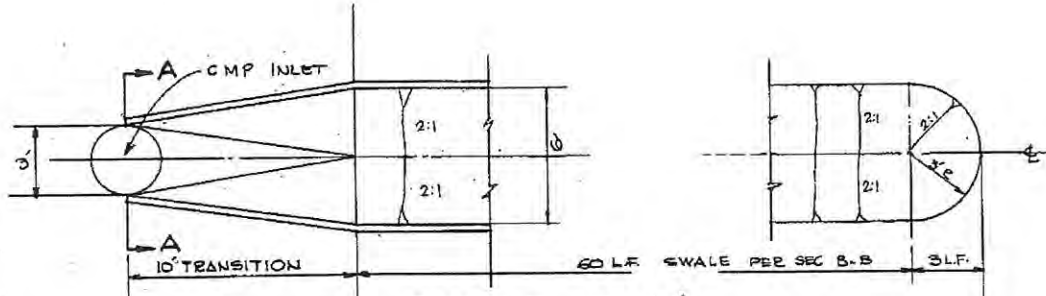
PROFILE
SCALE: 1" = 4' VERT.
1" = 40' HORIZ.



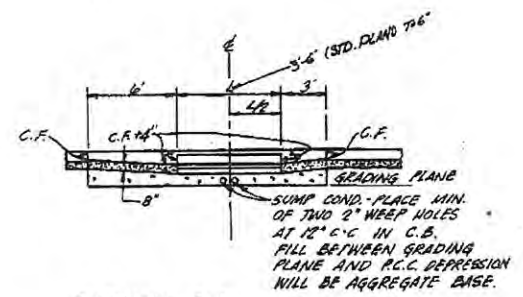
SECTION A-A



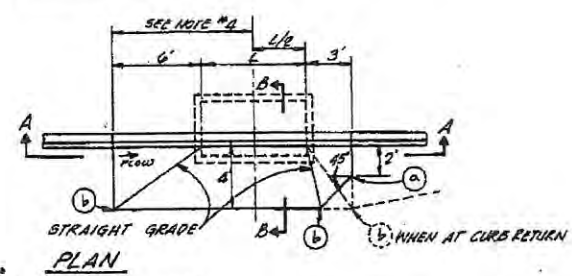
SECTION B-B



SWALE PLAN
SCALE: 1/4" = 1'-0"

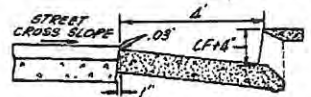


SECTION A-A



PLAN

- NOTES:**
1. LOCAL DEPRESSION SHALL BE CLASS "B" PORTLAND CEMENT CONCRETE, 8" THICK.
 2. LOCAL DEPRESSION SHALL CONFORM TO SAME SHAPE WHETHER GRATE INLET OR CURB OPENING, OR BOTH, ARE USED.
 3. LENGTH OF OPENING "L" SHALL BE SPECIFIED ON PLANS.
 4. BOTH ENDS OF DEPRESSION SHALL BE SYMMETRICAL ABOUT C OF OPENING IN SUMP CONDITION.
 5. SEE O.C.R.D. STD. PLAN 305 FOR CURB OPENING DETAIL.

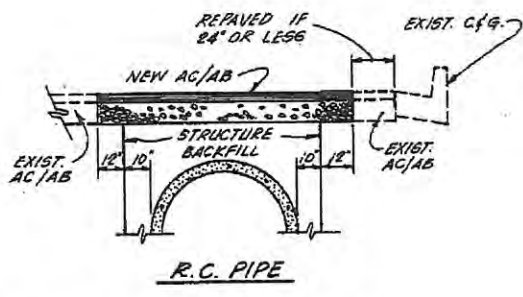


SECTION B-B

POINT	6' TO 10' OF TRANS. DISTANCE BEHIND TRANS.	8' TO 12' OF TRANS. DISTANCE BEHIND TRANS.
a	.38'	.50'
b	.34'	.41'

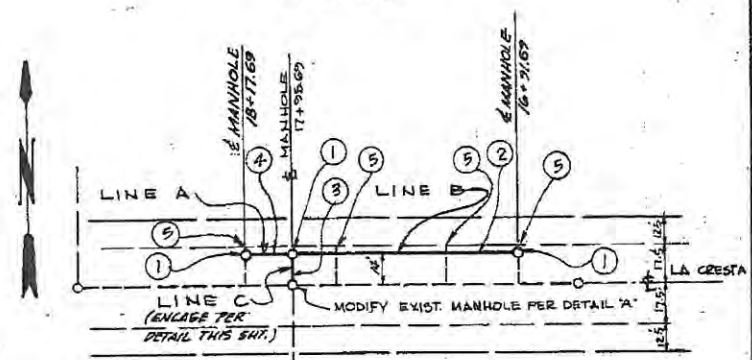
BASED ON 1.7% STREET CROSSFALL

LOCAL DEPRESSION DETAIL

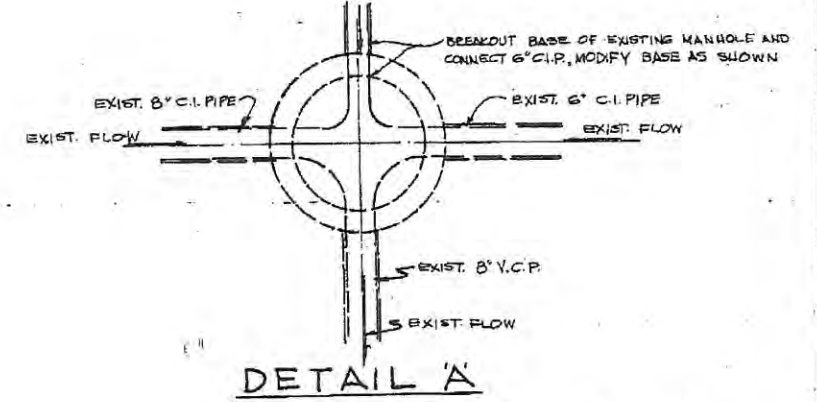


PAVEMENT PAYLINE DETAIL
NO SCALE

- SEWER RECONSTRUCTION NOTES**
1. CONSTRUCT SEWER MANHOLE PER O.C.S.D. STD. DWG. NO. S-33-1.
 2. CONSTRUCT 100 L.F. 6" V.C.P. PER DETAILS THIS SHEET.
 3. CONSTRUCT 10 L.F. 6" C.I. PIPE WITH CONCRETE ENCASEMENT PER DETAILS THIS SHEET.
 4. CONSTRUCT 18 L.F. 6" V.C.P. PER DETAILS THIS SHEET.
 5. CONNECT EXISTING HOUSE LATERALS TO MAINLINE.

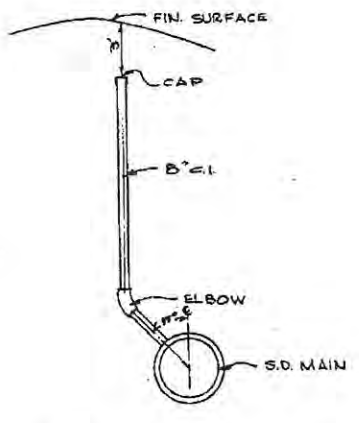


SEWER RECONSTRUCTION PLAN
SCALE: 1" = 40'



DETAIL A

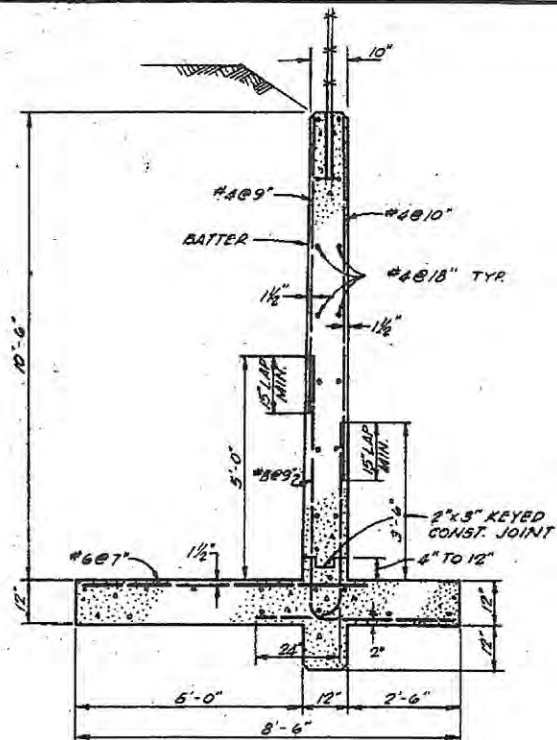
1/2 0 1 2
3 inches on original drawing



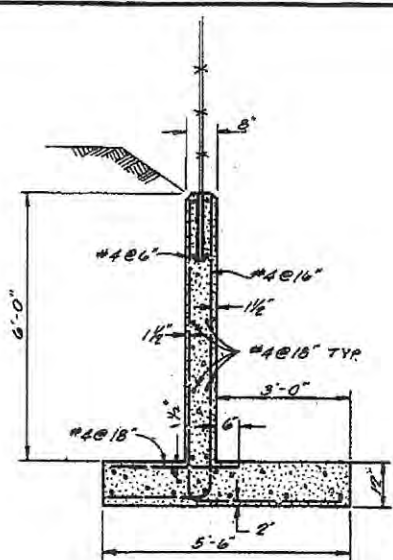
STAND PIPE DETAIL
NO SCALE

PRELIMINARY REVISION CODE		ORANGE COUNTY FLOOD CONTROL DISTRICT	
MARK	DATE	DESCRIPTION	
DESIGNED: J.T.T.		RECOMMENDED: [Signature]	
DRAWN: M.N.M.		CHECKED: M.A.C.	
SUBMITTED: [Signature]		DESIGN DIVISION ENGINEER	
SCALE: AS SHOWN		DATE: AUG. 75	DWG. NO. LOOP01-713-2.1

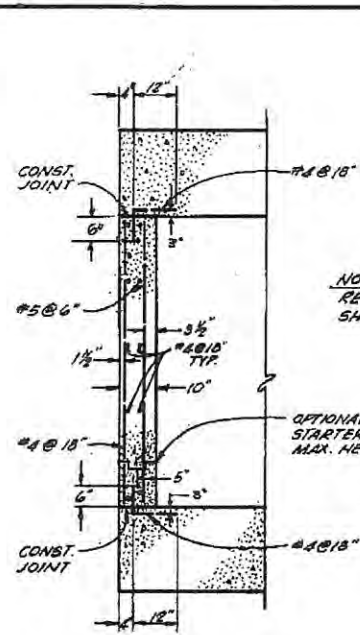
EXHIBIT 5



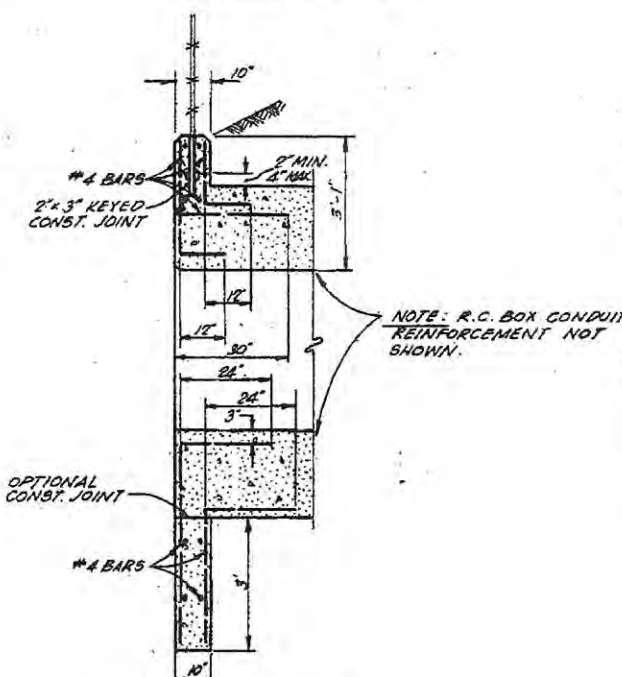
SECTION B-B
SCALE: 1/2" = 1'-0"



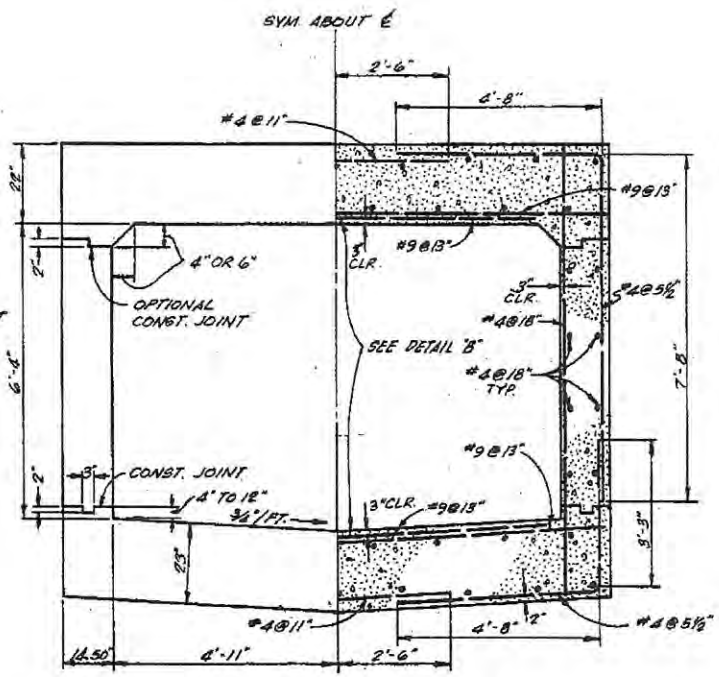
SECTION C-C
SCALE: 1/8" = 1'-0"



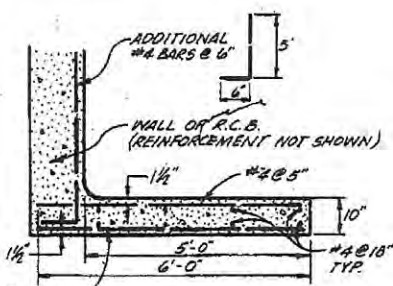
SECTION E-E
SCALE: 1/2" = 1'-0"



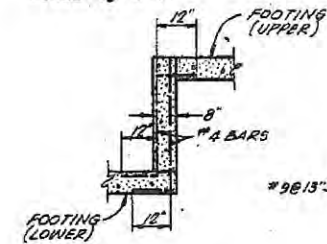
SECTION D-D
SCALE: 1/2" = 1'-0"



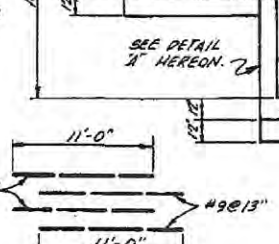
SECTION A-A
SCALE: 1/8" = 1'-0"



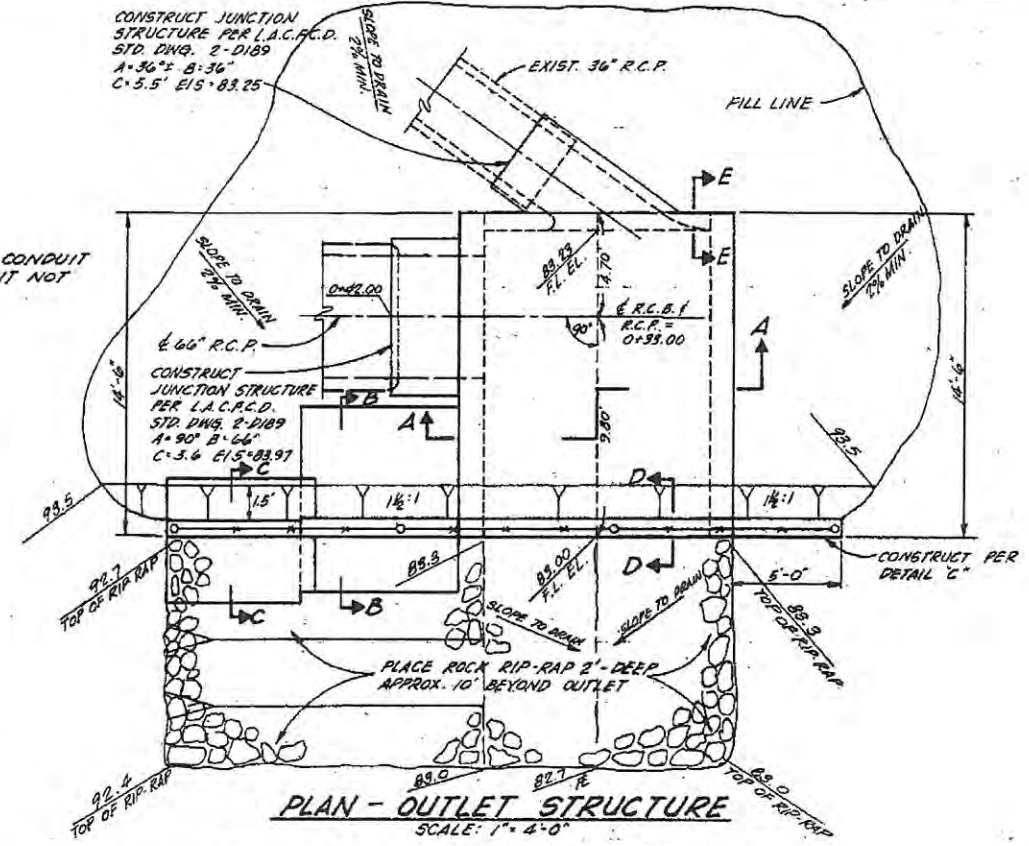
DETAIL C-C
SCALE: 1/2" = 1'-0"



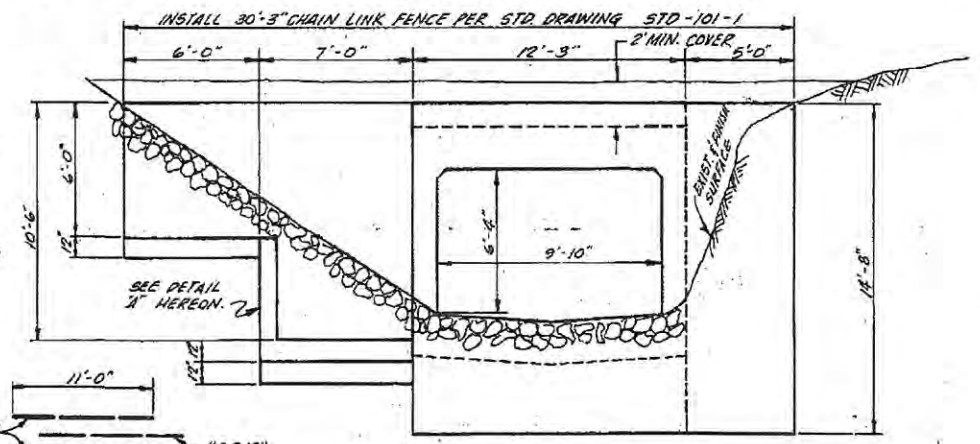
DETAIL A-A
NO SCALE



DETAIL B-B
NO SCALE



PLAN - OUTLET STRUCTURE
SCALE: 1" = 4'-0"



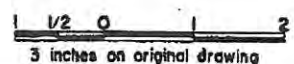
ELEVATION OUTLET STRUCTURE
SCALE: 1" = 4'-0"

DESIGN DATA
DESIGN LOADS
(EARTH @ 110 p.s.f., CONCRETE 150 p.s.f.)
RETAINING WALL **BOX SECTION**
62.5 p.s.f. s.f.p. LATERAL LIVE LOAD H320-44 TRUCK
LOAD WITH 2' SURCHARGE DEAD LOAD 22 FEET OF FILL
LATERAL LOAD 37 p.s.f. s.f.p. LATERAL LOAD

DESIGN METHOD
WORKING STRENGTH METHOD
ALLOWABLE STRESSES
CONCRETE $f_c = 3000$ psi
 $f_c = 1350$ psi
REINFORCEMENT $f_s = 20,000$ psi
SHEAR AND BOND STRESSES PER
ACI 318-71, n = 92

STRUCTURAL NOTES FOR OUTLET STRUCTURE

- ALL REINFORCING STEEL SHALL HAVE 1 1/2" CLEAR CONCRETE COVER UNLESS SHOWN OTHERWISE.
- THE VERTICAL WALL STEEL IN THE INTERIOR FACE OF WALLS MAY BE SPLICED AT THE CONSTRUCTION JOINT AT THE BASE OF THE WALL. THE SPLICE SHALL BE 20 BAR DIAMETERS IN LENGTH.
THE VERTICAL LENGTHS OF ALL STEEL IN EXTERIOR FACE HAS BEEN CALCULATED FOR A FOUR INCH STARTER WALL. IF THE HEIGHT OF STARTER WALL IS VARIED, THE STEEL LENGTH SHALL BE VARIED SO AS TO MAINTAIN A 30" DIAMETER LAP BETWEEN BARS BASED ON THE SMALLER DIAMETER.
- LONGITUDINAL STEEL SHALL BE LAPPED 20 BAR DIAMETERS AT SPLICES.



PRELIMINARY REVISION CODE		ORANGE COUNTY FLOOD CONTROL DISTRICT	
Revised Prints Bearing Earlier Codes		GOLDEN LANTERN STORM DRAIN	
REVISIONS		OUTLET STRUCTURE	
MARK	DATE	DESCRIPTION	DESIGN DIVISION ENGINEER
DESIGNED	J.T.L.	RECOMMENDED	J.A.M.
DRAWN	R.L.G./	CHECKED	M.A.C.
SUBMITTED	10/2/75	SCALE	AS SHOWN
		DATE	AUG. 75
		DWG. NO.	LOOP01-713-24

BORING LOG GEOLABS, INC.
GEOLOGY AND SOIL ENGINEERING

Project: Golden Lantern Storm Drain
Boring No. 1 Location: See Plate 1
WQ 918-00 Drill Date 5/12/75
Surface Elev. Logged by V.S. Driving Weight 1500#-12" drop

DEPTH (FEET)	GRAPHIC LOG	UNIT (soil, fill, alluvium, siltstone, etc.)	MATERIAL DESCRIPTION (% sand, silt, clay, color, consolidation, etc.)	ATTITUDE MEASUREMENTS: B-Bedding J-Joint C-Contact F-Fault RS-Rupture Surface	GROUP SYMBOL U.S.C.S.	PERCENT RESIST BLOW/FOOT	C-CORRECTION B-BAG	DRY DENSITY (pcf)	MOISTURE CONTENT (%)
0		FILL: SILTY SAND: Medium brown, mixed with silt of SILTY CLAY and traces of GRAVEL, occasional pieces of asphaltic concrete, moist, loosely to moderately compacted.			SM				
5		NATURAL GROUND: SILTY SAND: Light brown to gray, medium to fine grained, slightly clayey, moist medium dense.			SM	1	C	112.0	7.2
10		SILTY CLAY: Dark brown, moist, medium stiff.			CL	2	C	105.0	10.0
15		SILTY SAND: Dark brown, fine grained, moist, medium dense.			SM	3	C	108.0	10.9
20		SAND: Light brown, trace of gravel, slightly moist, dense, very hard BOULDERS at 22'-24'.			SP				
25		becoming yellowish colored, fine to medium grained with trace of small pebbles, very dense.			SM	26*	C	110.0	4.5
30		SAND: Yellowish-white, well graded, slightly moist, very dense.			SW SP	40*	C	126.0	4.1
35		SILTY SAND: Medium brown with cobbles, very dense, very slow drilling.			SM				
33.5		End of boring at 33.5 feet.							
		No caving							
		No water							
		*750#-hammer 12"-drop							

BORING LOG GEOLABS, INC.
GEOLOGY AND SOIL ENGINEERING

Project: Golden Lantern Storm Drain
Boring No. 3 Location: See Plate 5
WQ 918-00 Drill Date 5/12/75
Surface Elev. Logged by V.S. Driving Weight 1500#-12" drop

DEPTH (FEET)	GRAPHIC LOG	UNIT (soil, fill, alluvium, siltstone, etc.)	MATERIAL DESCRIPTION (% sand, silt, clay, color, consolidation, etc.)	ATTITUDE MEASUREMENTS: B-Bedding J-Joint C-Contact F-Fault RS-Rupture Surface	GROUP SYMBOL U.S.C.S.	PERCENT RESIST BLOW/FOOT	C-CORRECTION B-BAG	DRY DENSITY (pcf)	MOISTURE CONTENT (%)
0		FILL: SILTY CLAY: Brown, wet, soft.			CL				
5		SANDY CLAY: Dark brown, wet, soft to medium stiff.			CL				
10		NATURAL GROUND: BEDROCK: CLAYEY SILTSTONE: Dark brown, very weathered, moist, firm with occasional stringers of gypsum and orange bands, moist, firm.			ML	2	C	83.0	37.8
13		End of Boring at 13 feet.							
		No caving							
		No water							

BORING LOG GEOLABS, INC.
GEOLOGY AND SOIL ENGINEERING

Project: Golden Lantern Storm Drain
Boring No. 2 Location: See Plate 2
WQ 918-00 Drill Date 5/12/75
Surface Elev. Logged by V.S. Driving Weight 1500#-12" drop

DEPTH (FEET)	GRAPHIC LOG	UNIT (soil, fill, alluvium, siltstone, etc.)	MATERIAL DESCRIPTION (% sand, silt, clay, color, consolidation, etc.)	ATTITUDE MEASUREMENTS: B-Bedding J-Joint C-Contact F-Fault RS-Rupture Surface	GROUP SYMBOL U.S.C.S.	PERCENT RESIST BLOW/FOOT	C-CORRECTION B-BAG	DRY DENSITY (pcf)	MOISTURE CONTENT (%)
0		FILL: SILTY SAND: medium brown, moist, loose.			SM				
5		NATURAL GROUND: BEDROCK: CLAYEY SILTSTONE: Mottled brown and gray, very moist, firm.			ML	4	C	90.0	28.8
10		Slightly sandy at 10 feet.				5	C	88.0	33.0
15		becoming dark green to black colored at 20 feet.				10	C	89.0	33.2
20		End of Boring at 22 feet.				14	C	91.0	30.7
		No caving							
		No water							

BORING LOG GEOLABS, INC.
GEOLOGY AND SOIL ENGINEERING

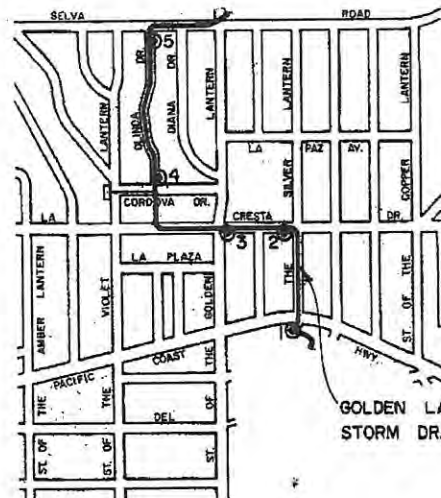
Project: Golden Lantern Storm Drain
Boring No. 3 Location: See Plate 3
WQ 918-00 Drill Date 5/12/75
Surface Elev. Logged by V.S. Driving Weight 1500#-12" drop

DEPTH (FEET)	GRAPHIC LOG	UNIT (soil, fill, alluvium, siltstone, etc.)	MATERIAL DESCRIPTION (% sand, silt, clay, color, consolidation, etc.)	ATTITUDE MEASUREMENTS: B-Bedding J-Joint C-Contact F-Fault RS-Rupture Surface	GROUP SYMBOL U.S.C.S.	PERCENT RESIST BLOW/FOOT	C-CORRECTION B-BAG	DRY DENSITY (pcf)	MOISTURE CONTENT (%)
0		NATURAL GROUND: SILTY SAND: Light brown, moist, loose.			SM				
5		SANDY CLAY: Medium brown, moist, stiff.			CL				
10		CLAYEY SAND: Medium brown, moist, dense.			SC	6	C	124.0	10.7
15		SILTY SAND: Brown, fine grained, moist, dense.			SM	10	C-B	12.1	9.2
20		becoming light gray, very fine grained, moist, very dense.							
25		With few gravel and cobbles at 14 feet.							
30		End of Boring at 28 feet.							
		No caving							
		No water							

BORING LOG GEOLABS, INC.
GEOLOGY AND SOIL ENGINEERING

Project: Golden Lantern Storm Drain
Boring No. 4 Location: See Plate 4
WQ 918-00 Drill Date 5/12/75
Surface Elev. Logged by V.S. Driving Weight 1500#-12" drop

DEPTH (FEET)	GRAPHIC LOG	UNIT (soil, fill, alluvium, siltstone, etc.)	MATERIAL DESCRIPTION (% sand, silt, clay, color, consolidation, etc.)	ATTITUDE MEASUREMENTS: B-Bedding J-Joint C-Contact F-Fault RS-Rupture Surface	GROUP SYMBOL U.S.C.S.	PERCENT RESIST BLOW/FOOT	C-CORRECTION B-BAG	DRY DENSITY (pcf)	MOISTURE CONTENT (%)
0		FILL: SILTY CLAY: very moist, soft.			CL				
5		SANDY CLAY: Light brown, wet, soft.			CL				
10		SILTY SAND: Light brown, fine grained, slightly clayey, wet, loose to very loose.			SM	1	C	99.0	21.8
15		SILTY CLAY: Black, trace of organic, very moist, soft to medium stiff.			CL				
20		NATURAL GROUND: SILTY SAND: Mottled, brown and gray, very moist, medium dense.			SM	1 </td <td>C</td> <td>100.6</td> <td>25.1</td>	C	100.6	25.1
25		Layer of SAND, saturated, water seeping at rapid rate.			SP	9	C	124.0	12.9
30		Back to SILTSTONE, dark gray, very firm.			ML	6	C		
35		End of Boring at 17 feet.							
		Caving at 15 feet.							
		Water at 14.5 feet.							



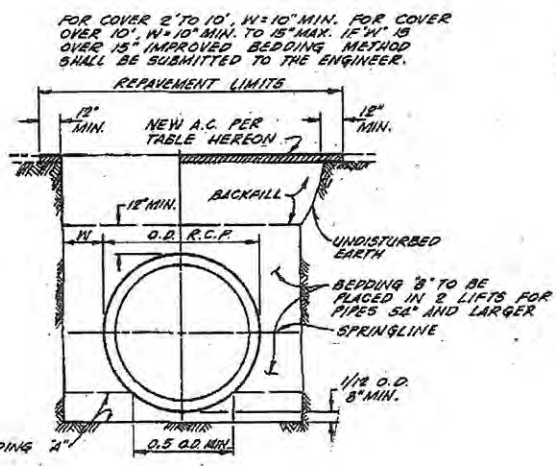
BORING LOCATION MAP
SCALE: 1" = 600'

EXCAVATION & PAVING NOTES

- AT TIMES OF RESURFACING OPERATIONS, ALL PORTLAND CEMENT AND BITUMINOUS TIRE WEARING SURFACES SHALL BE CUT WITH A PAVEMENT SAW.
- IF SIDEWALLS CAVE IN, EXCAVATE TO SURFACE AND 12" INTO UNDISTURBED MATERIAL OR TO NEXT PAVEMENT JOINT IF WITHIN 3 FT.

BEDDING NOTES

- BEDDING "A" SHALL BE COMPOSED OF SAND, NO. 3 OR NO. 4 CRUSHED ROCK OR GRAVEL, OR OTHER GRANULAR MATERIAL APPROVED BY THE ENGINEER.
- BEDDING "B" SHALL BE COMPOSED OF SAND OR OTHER GRANULAR MATERIAL APPROVED BY THE ENGINEER AND SHALL BE COMPACTED AND APPROVED PRIOR TO PLACING BALANCE OF BACKFILL.
- SAND-CEMENT SLURRY MAY BE USED FOR BEDDING.



BEDDING DETAIL
NO SCALE

REPAVEMENT SCHEDULE

LIMIT	REPLACEMENT SECTION
ST. OF THE SILVER LANTERN P.C.H. TO LA CRESTA DR.	0.25' AC/NS
LA CRESTA DRIVE ST. OF THE SILVER LANTERN TO 450' WEST OF ST. OF THE GOLDEN LANTERN	0.25' AC/NS
OLINDA DRIVE CORDOVA DR. TO SELVA RD.	0.30' AC/NS
SELVA ROAD OLINDA DR. TO ST. OF THE GOLDEN LANTERN	0.30' AC/NS

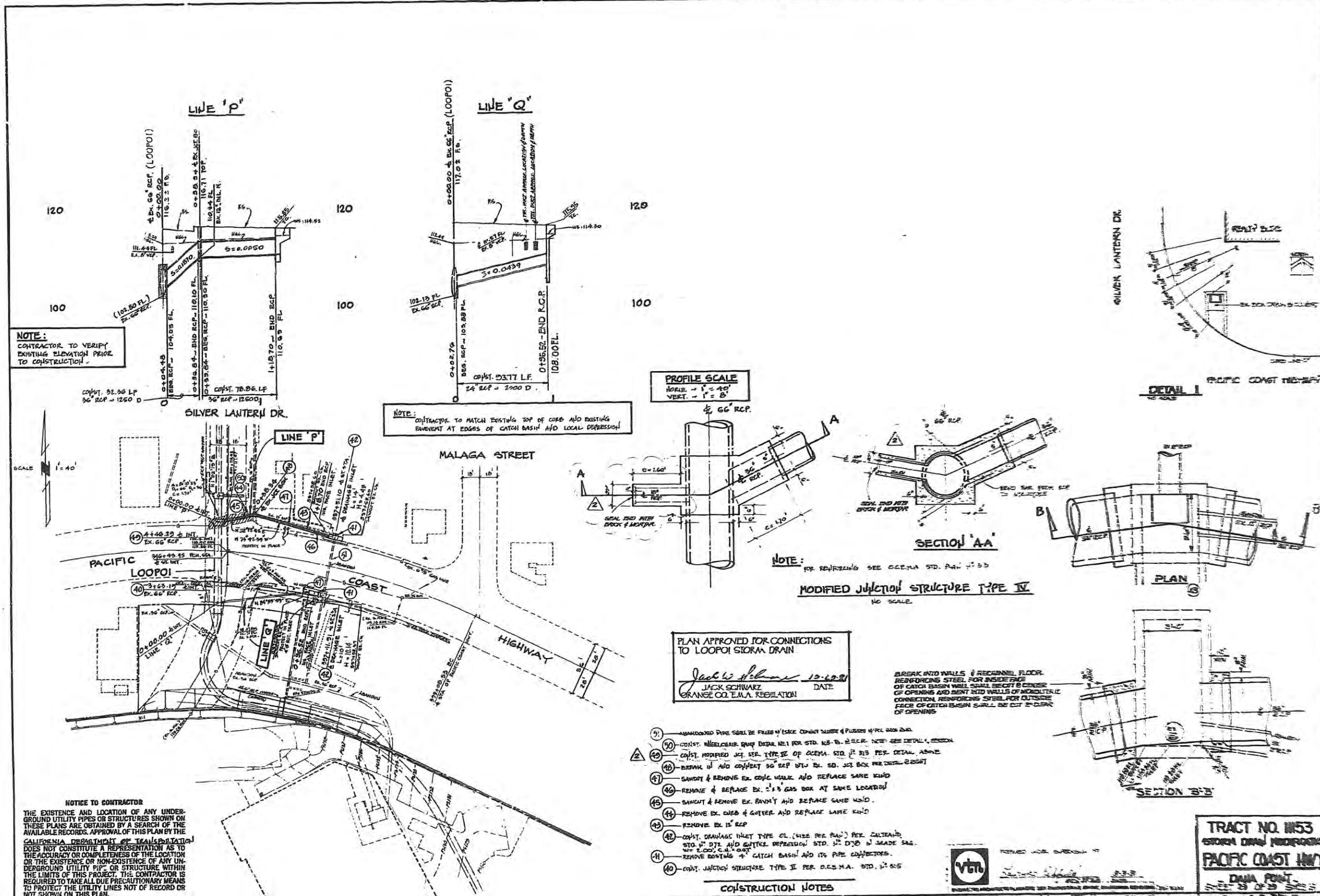
NOTE: THESE BORING LOGS WERE ACCOMPANIED BY A SOILS INVESTIGATION REPORT PREPARED BY GEOLABS, INC. THE REPORT IS AVAILABLE FOR STUDY IN THE OFFICE OF THE DISTRICT.

REVISIONS	DATE	DESCRIPTION

DESIGNED: J.T.T.
DRAWN: J.M.G. (CHECKED: J.M.G.)
SUBMITTED: J.M.G. (DESIGN ENGINEER)

RECORDED: J.M.G.
SCALE: AS SHOWN
DATE: AUG 75
DWG. NO.: L00P01-713-2A

EXHIBIT 5



NOTE:
CONTRACTOR TO VERIFY
EXISTING ELEVATION PRIOR
TO CONSTRUCTION.

NOTE:
CONTRACTOR TO MATCH EXISTING TOP OF CURB AND EXISTING
PAVEMENT AT EDGES OF CATCH BASIN AND LOCAL DEPRESSION!

PROFILE SCALE
HORIZ. - 1" = 40'
VERT. - 1" = 5'

NOTE:
FOR REINFORCING SEE OCEMA STD. PAR. 4.3.5
MODIFIED JUNCTION STRUCTURE TYPE IV
NO SCALE

**PLAN APPROVED FOR CONNECTIONS
TO LOOPOI STORM DRAIN**
Jack Schwarz 12-20-92
DATE
JACK SCHWARTZ
GRANGE CO. E.M.A. REGULATION

BREAK INTO WALLS & RECONSTRUCT FLOOR.
REINFORCING STEEL FOR INSIDE FINE
OF CATCH BASIN SHALL BE CUT & BENT TO
CONNECTION REINFORCING STEEL FOR OUTSIDE
FACE OF CATCH BASIN SHALL BE CUT IN CASE
OF OPENING

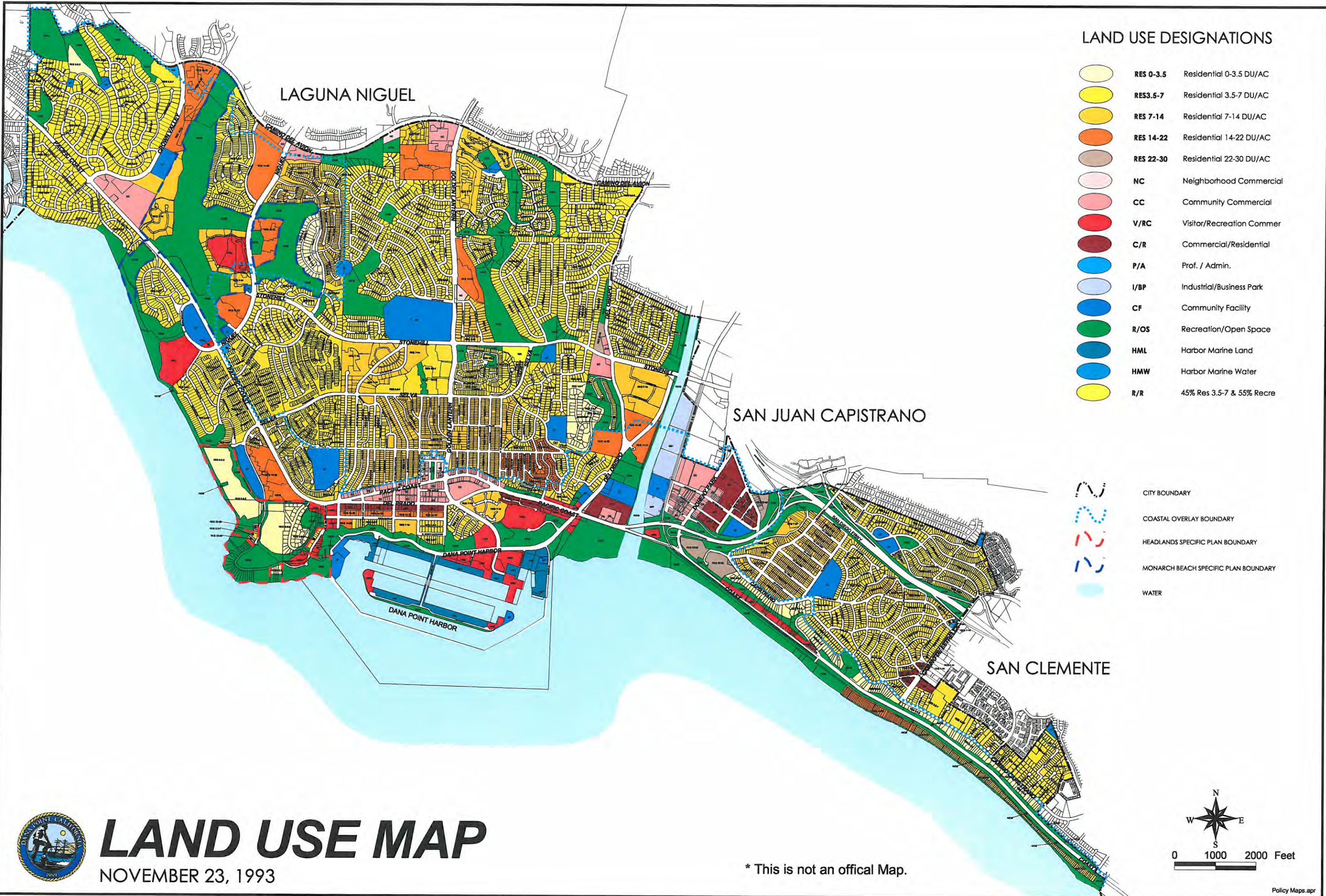
- 1) ABANDONED PIPE SHALL BE FRIED W/ (S) (SEE CONDUIT NUMBER & PLACES W/ R/C MARK AND
- 2) CONST. REINFORCING STEEL DETAIL PER STD. 4.3.5.2 R.C.P. (SEE DETAIL 1, SECTION
- 3) CONST. MODIFIED JCT. STR. TYPE IV OF OCEMA STD. 4.3.5 PER DETAIL ABOVE
- 4) BREAK IN AND CONNECT 30" RCP W/ 18" R.C.P. JCT. BOX PER DETAIL 2 (SEE)
- 5) SAWCUT & REMOVE EX. CONC. WALK AND REPLACE SAME KIND
- 6) REMOVE & REPLACE EX. 2" GAS BOX AT SAME LOCATION
- 7) SAWCUT & REMOVE EX. RAIN'T AND REPLACE SAME KIND
- 8) REMOVE EX. CURB & GUTTER AND REPLACE SAME KIND
- 9) REMOVE EX. 15" RCP
- 10) CONST. DRAINAGE INLET TYPE C1 (4" DIA PER PAR.) PER CONTR. STD. 4.3.5.1 AND GUTTER DEPRESSION STD. 4.3.5.2 IN GRADE S&E. W/ 1.00" C.A. & 0.01"
- 11) REMOVE EXISTING 4" CATCH BASIN AND ITS PIPE CONNECTIONS.
- 12) CONST. JUNCTION STRUCTURE TYPE IV PER O.C.S.M.A. STD. 4.3.5

CONSTRUCTION NOTES

NOTICE TO CONTRACTOR
THE EXISTENCE AND LOCATION OF ANY UNDERGROUND UTILITY PIPES OR STRUCTURES SHOWN ON THESE PLANS ARE OBTAINED BY A SEARCH OF THE AVAILABLE RECORDS. APPROVAL OF THIS PLAN BY THE CALIFORNIA DEPARTMENT OF TRANSPORTATION DOES NOT CONSTITUTE A REPRESENTATION AS TO THE ACCURACY OR COMPLETENESS OF THE LOCATION OR THE EXISTENCE OR NON-EXISTENCE OF ANY UNDERGROUND UTILITY PIPE OR STRUCTURE WITHIN THE LIMITS OF THIS PROJECT. THE CONTRACTOR IS REQUIRED TO TAKE ALL DUE PRECAUTIONARY MEANS TO PROTECT THE UTILITY LINES NOT OF RECORD OR NOT SHOWN ON THIS PLAN.

TRACT NO. 1153
STORM DRAIN IMPROVEMENT
PACIFIC COAST HWY
DATA POINT
TR. IMP. (1153)

EXHIBIT 5



LAND USE DESIGNATIONS

	RES 0-3.5	Residential 0-3.5 DU/AC
	RES3.5-7	Residential 3.5-7 DU/AC
	RES 7-14	Residential 7-14 DU/AC
	RES 14-22	Residential 14-22 DU/AC
	RES 22-30	Residential 22-30 DU/AC
	NC	Neighborhood Commercial
	CC	Community Commercial
	V/RC	Visitor/Recreation Commer
	C/R	Commercial/Residential
	P/A	Prof. / Admin.
	I/BP	Industrial/Business Park
	CF	Community Facility
	R/OS	Recreation/Open Space
	HML	Harbor Marine Land
	HMW	Harbor Marine Water
	R/R	45% Res 3.5-7 & 55% Recre

	CITY BOUNDARY
	COASTAL OVERLAY BOUNDARY
	HEADLANDS SPECIFIC PLAN BOUNDARY
	MONARCH BEACH SPECIFIC PLAN BOUNDARY
	WATER



LAND USE MAP
NOVEMBER 23, 1993

* This is not an official Map.

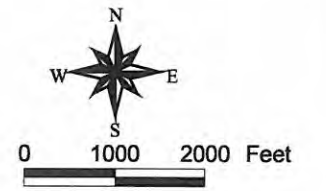


EXHIBIT 6

LAGUNA NIGUEL

LEGEND

RESIDENTIAL

- RSF 2 RESIDENTIAL SINGLE FAMILY 2 DU/AC
- RSF 3 RESIDENTIAL SINGLE FAMILY 3 DU/AC
- RSF 4 RESIDENTIAL SINGLE FAMILY 4 DU/AC
- RSF 7 RESIDENTIAL SINGLE FAMILY 7 DU/AC
- RSF 12 RESIDENTIAL SINGLE FAMILY 12 DU/AC
- RSF 22 RESIDENTIAL SINGLE FAMILY 22 DU/AC
- RBR 12 RESIDENTIAL BEACH ROAD 12 DU/AC
- RBR 18 RESIDENTIAL BEACH ROAD DUPLEX 18 DU/AC
- RD 14 RESIDENTIAL DUPLEX 14 DU/AC
- RMF 17 RESIDENTIAL MULTIPLE FAMILY 7 DU/AC
- RMF 14 RESIDENTIAL MULTIPLE FAMILY 14 DU/AC
- RMF 22 RESIDENTIAL MULTIPLE FAMILY 22 DU/AC
- RMF 30 RESIDENTIAL MULTIPLE FAMILY 30 DU/AC

MIXED USE

- C/R COMMERCIAL / RESIDENTIAL
- P/R PROFESSIONAL / RESIDENTIAL
- TC-MU TOWN CENTER MIXED-USE

COMMUNITY / OPEN SPACE

- REC RECREATION
- OS OPEN SPACE
- CONS CONSERVATION
- CD COMMUNITY FACILITIES
- DPHPC DP HARBOR PLANNED COMMUNITY
- TC TRANSPORTATION CORRIDOR

COMMERCIAL / PROFESSIONAL

- NC NEIGHBORHOOD COMMERCIAL
- C.C.P. COMMUNITY COMMERCIAL / PEDESTRIAN
- C.C.V. COMMUNITY COMMERCIAL / VEHICLE
- V/RC VISITOR / RECREATION COMMERCIAL
- P/A PROFESSIONAL / ADMINISTRATION
- I/B INDUSTRIAL / BUSINESS

OVERLAY DISTRICTS

- DPSP DP SPECIFIC PLAN OVERLAY
Per CC 20-10P
Approved by the Orange County Planning Commission on April 6, 1985 and adopted by Ordinance No. 3528 by the Orange County Board of Supervisors on May 15, 1985.
- SPO ZONE SPECIFIC PLAN OVERLAY ZONES
MSP - Mariner Beach Specific Plan
PCOP - Headlands Conservation Plan
- FP-2 FLOODPLAIN OVERLAY (FP-2)
- FP-3 FLOODPLAIN OVERLAY (FP-3)

BOUNDARIES

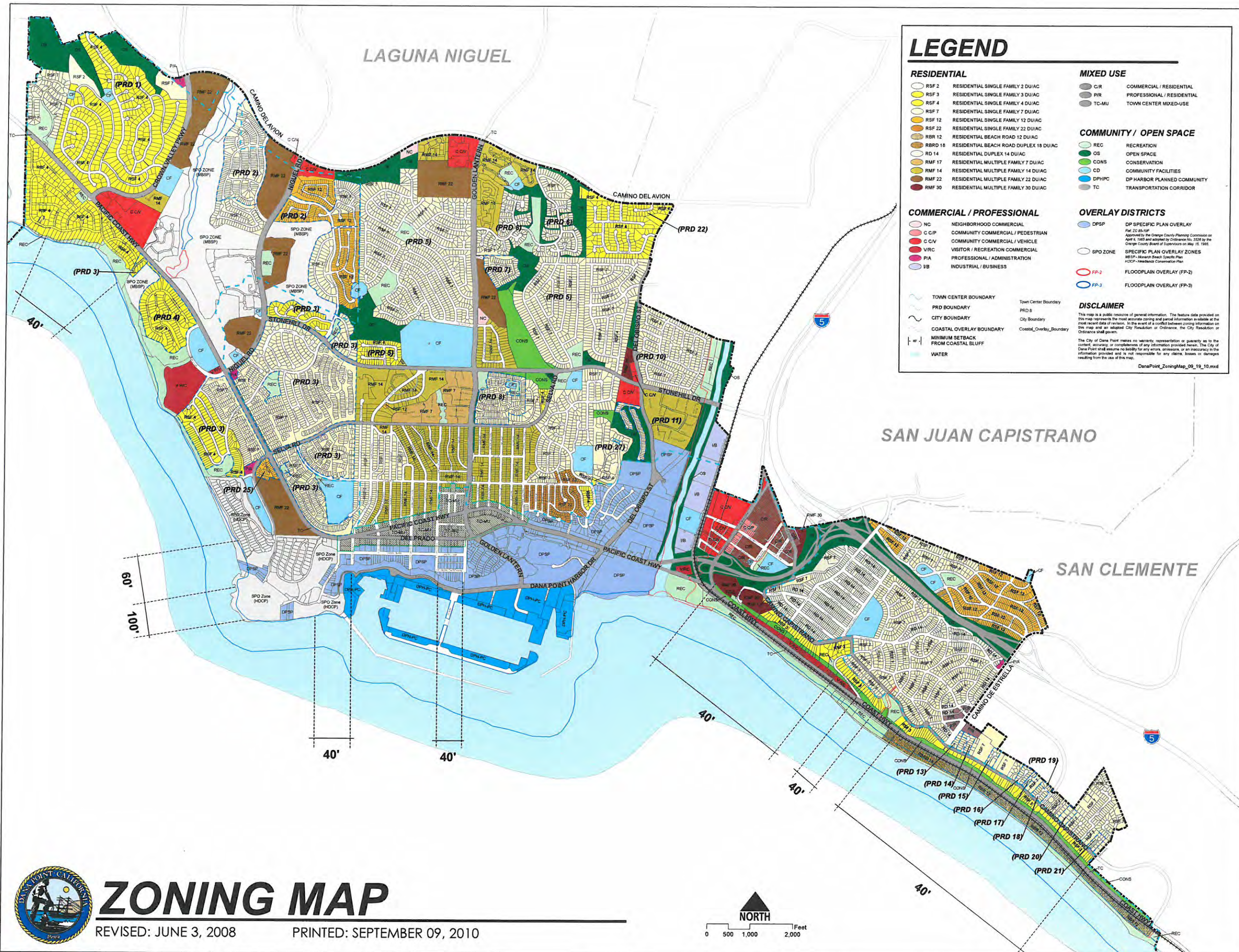
- TOWN CENTER BOUNDARY
- PRD BOUNDARY
- CITY BOUNDARY
- COASTAL OVERLAY BOUNDARY
- MINIMUM SETBACK FROM COASTAL BLUFF
- WATER

DISCLAIMER

This map is a public resource of general information. The feature data provided on this map represents the most accurate zoning and parcel information available at the most recent date of revision. In the event of a conflict between zoning information on this map and an adopted City Resolution or Ordinance, the City Resolution or Ordinance shall govern.

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DanaPoint_ZoningMap_09_19_10.mxd



ZONING MAP

REVISED: JUNE 3, 2008

PRINTED: SEPTEMBER 09, 2010

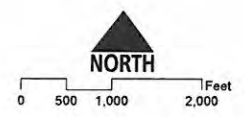


EXHIBIT 7

APPENDIX B. 10-YEAR HIGH CONFIDENCE HYDROLOGY CALCULATIONS

- B.1 EXISTING CONDITION W/O HARBOR (MODEL 1)
- B.2 EXISTING CONDITION W/ HARBOR (MODEL 2)
- B.3 PROPOSED CONDITION W/ HARBOR (MODEL 3)

B.1

Existing 10-Year
60" Hydrology
w/o Harbor
(consistent w/
City MPD)

DPHOSR2

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
(c) Copyright 1983-2012 Advanced Engineering Software (aes)
Ver. 19.0 Release Date: 06/01/2012 License ID 1355

Analysis prepared by:

Fusco Engineering, Inc.
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Irvine, CA 92606

FILE NAME: DPHOSR2.DAT
TIME/DATE OF STUDY: 15:40 04/26/2013

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 10.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 12.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- CROWN TO		STREET-CROSSFALL:		CURB HEIGHT (FT)	GUTTER GEOMETRIES:			MANNING FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)	IN- SIDE	OUT- SIDE / PARK- WAY		WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018	0.018/0.020	0.67	2.00	0.0313	0.167	0.0150
2	18.0	5.0	0.020	0.020/0.020	0.50	1.50	0.0313	0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.67 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 280.00
ELEVATION DATA: UPSTREAM (FEET) = 295.00 DOWNSTREAM (FEET) = 290.00

Tc = K * [(LENGTH** 3.00) / (ELEVATION CHANGE)] ** 0.20
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 8.288
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.039
SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.30	0.20	0.500	75	8.29

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA RUNOFF (CFS) = 3.44
TOTAL AREA (ACRES) = 1.30 PEAK FLOW RATE (CFS) = 3.44

FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

UPSTREAM ELEVATION (FEET) = 290.00 DOWNSTREAM ELEVATION (FEET) = 285.00

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STREET LENGTH(FEET) = 135.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.64
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.35
HALFSTREET FLOOD WIDTH(FEET) = 11.43
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.66
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.65
STREET FLOW TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 8.77
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.942

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 2.50 0.20 0.500 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 2.50 SUBAREA RUNOFF(CFS) = 6.39
EFFECTIVE AREA(ACRES) = 3.80 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50
TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 9.72

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.35
FLOW VELOCITY(FEET/SEC.) = 5.11 DEPTH*VELOCITY(FT*FT/SEC.) = 2.01
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 103.00 = 415.00 FEET.

FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 285.00 DOWNSTREAM ELEVATION(FEET) = 253.00
STREET LENGTH(FEET) = 345.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 14.11
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.40
HALFSTREET FLOOD WIDTH(FEET) = 13.48
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.77
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.13
STREET FLOW TRAVEL TIME(MIN.) = 0.74 Tc(MIN.) = 9.51
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.808

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 3.60 0.20 0.500 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 3.60 SUBAREA RUNOFF(CFS) = 8.78
EFFECTIVE AREA(ACRES) = 7.40 AREA-AVERAGED Fm(INCH/HR) = 0.10

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AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50
TOTAL AREA(ACRES) = 7.4 PEAK FLOW RATE(CFS) = 18.04

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 14.96
FLOW VELOCITY(FEET/SEC.) = 8.23 DEPTH*VELOCITY(FT*FT/SEC.) = 3.54
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 104.00 = 760.00 FEET.

FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 253.00 DOWNSTREAM ELEVATION(FEET) = 225.00
STREET LENGTH(FEET) = 630.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 20.18
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.49
HALFSTREET FLOOD WIDTH(FEET) = 18.24
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.38
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.11
STREET FLOW TRAVEL TIME(MIN.) = 1.65 Tc(MIN.) = 11.16
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.563

SUBAREA LOSS RATE DATA(AMC II):

Table with 6 columns: DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN. Rows include Residential (5-7 Dwellings/Acre, Public Park, Commercial) and summary statistics for Subarea Average Pervious Loss Rate, Area Fraction, and Peak Flow Rate.

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.40
FLOW VELOCITY(FEET/SEC.) = 6.43 DEPTH*VELOCITY(FT*FT/SEC.) = 3.16
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 105.00 = 1390.00 FEET.

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 204.30 DOWNSTREAM(FEET) = 202.30
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.43
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 20.69
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 11.18
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 106.00 = 1415.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.18
RAINFALL INTENSITY(INCH/HR) = 2.56
AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.46
EFFECTIVE STREAM AREA(ACRES) = 9.30
TOTAL STREAM AREA(ACRES) = 9.30
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.69
```

```
*****
FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 21
-----
```

```
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 270.00
ELEVATION DATA: UPSTREAM(FEET) = 330.00 DOWNSTREAM(FEET) = 320.00
```

```
Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.880
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.699
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 1.00 0.20 0.200 75 5.88
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 3.29
TOTAL AREA(ACRES) = 1.00 PEAK FLOW RATE(CFS) = 3.29
```

```
*****
FLOW PROCESS FROM NODE 108.00 TO NODE 109.00 IS CODE = 31
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 310.00 DOWNSTREAM(FEET) = 265.00
FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.15
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.29
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 6.14
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 109.00 = 505.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 109.00 TO NODE 109.00 IS CODE = 81
-----
```

```
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
MAINLINE Tc(MIN.) = 6.14
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.609
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 3.90 0.20 0.200 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA(ACRES) = 3.90 SUBAREA RUNOFF(CFS) = 12.53
EFFECTIVE AREA(ACRES) = 4.90 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 4.9 PEAK FLOW RATE(CFS) = 15.74
```

```
*****
FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 31
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
Page 4
```


DPHOSR2

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 265.00 DOWNSTREAM(FEET) = 258.00
FLOW LENGTH(FEET) = 560.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.94
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.74
PIPE TRAVEL TIME(MIN.) = 1.18 Tc(MIN.) = 7.31
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 110.00 = 1065.00 FEET.

FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.31
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.265
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.30 0.20 0.500 75
PUBLIC PARK D 2.10 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.716
SUBAREA AREA(ACRES) = 3.40 SUBAREA RUNOFF(CFS) = 9.55
EFFECTIVE AREA(ACRES) = 8.30 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 8.3 PEAK FLOW RATE(CFS) = 23.77

FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 258.00 DOWNSTREAM(FEET) = 238.00
FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.66
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.77
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 7.45
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 111.00 = 1240.00 FEET.

FLOW PROCESS FROM NODE 111.00 TO NODE 111.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.229
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 5.50 0.20 0.500 75
PUBLIC PARK D 0.80 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.544
SUBAREA AREA(ACRES) = 6.30 SUBAREA RUNOFF(CFS) = 17.69
EFFECTIVE AREA(ACRES) = 14.60 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 14.6 PEAK FLOW RATE(CFS) = 41.20

FLOW PROCESS FROM NODE 111.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 238.00 DOWNSTREAM(FEET) = 202.30

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FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.0 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 26.38
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 41.20
 PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 7.60
 LONGEST FLOWPATH FROM NODE 107.00 TO NODE 106.00 = 1475.00 FEET.

 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

 TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 7.60
 RAINFALL INTENSITY(INCH/HR) = 3.19
 AREA-AVERAGED Fm(INCH/HR) = 0.09
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.47
 EFFECTIVE STREAM AREA(ACRES) = 14.60
 TOTAL STREAM AREA(ACRES) = 14.60
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 41.20

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	20.69	11.18	2.560	0.20(0.09)	0.46	9.3	101.00
2	41.20	7.60	3.193	0.20(0.09)	0.47	14.6	107.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	58.87	7.60	3.193	0.20(0.09)	0.47	20.9	107.00
2	53.47	11.18	2.560	0.20(0.09)	0.46	23.9	101.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 58.87 Tc(MIN.) = 7.60
 EFFECTIVE AREA(ACRES) = 20.92 AREA-AVERAGED Fm(INCH/HR) = 0.09
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
 TOTAL AREA(ACRES) = 23.9
 LONGEST FLOWPATH FROM NODE 107.00 TO NODE 106.00 = 1475.00 FEET.

 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

 FLOW PROCESS FROM NODE 112.00 TO NODE 113.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

 INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
 ELEVATION DATA: UPSTREAM(FEET) = 330.00 DOWNSTREAM(FEET) = 328.70

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.309
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.543
 SUBAREA Tc AND LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
 RESIDENTIAL
 "5-7 DWELLINGS/ACRE" D 1.10 0.20 0.500 75 11.31
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
 SUBAREA RUNOFF(CFS) = 2.42

DPHOSR2
TOTAL AREA(ACRES) = 1.10 PEAK FLOW RATE(CFS) = 2.42

FLOW PROCESS FROM NODE 113.00 TO NODE 114.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	328.70	DOWNSTREAM ELEVATION(FEET) =	327.40
STREET LENGTH(FEET) =	225.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	18.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =	5.00
INSIDE STREET CROSSFALL(DECIMAL) =	0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =	0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =	2
STREET PARKWAY CROSSFALL(DECIMAL) =	0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =	0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =	0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	4.00
--	------

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) =	0.33		
HALFSTREET FLOOD WIDTH(FEET) =	10.17		
AVERAGE FLOW VELOCITY(FEET/SEC.) =	1.74		
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =	0.57		
STREET FLOW TRAVEL TIME(MIN.) =	2.16	Tc(MIN.) =	13.47

* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.301

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.60	0.20	0.500	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 1.60 SUBAREA RUNOFF(CFS) = 3.17
EFFECTIVE AREA(ACRES) = 2.70 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50
TOTAL AREA(ACRES) = 2.7 PEAK FLOW RATE(CFS) = 5.35

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) =	0.36	HALFSTREET FLOOD WIDTH(FEET) =	11.52
FLOW VELOCITY(FEET/SEC.) =	1.85	DEPTH*VELOCITY(FT*FT/SEC.) =	0.66
LONGEST FLOWPATH FROM NODE	112.00 TO NODE	114.00 =	525.00 FEET.

FLOW PROCESS FROM NODE 114.00 TO NODE 115.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	312.40	DOWNSTREAM(FEET) =	310.80
FLOW LENGTH(FEET) =	180.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS	11.4 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	5.34		
ESTIMATED PIPE DIAMETER(INCH) =	15.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	5.35		
PIPE TRAVEL TIME(MIN.) =	0.56	Tc(MIN.) =	14.03
LONGEST FLOWPATH FROM NODE	112.00 TO NODE	115.00 =	705.00 FEET.

FLOW PROCESS FROM NODE 115.00 TO NODE 115.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) =	14.03
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	2.248

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.30	0.20	0.500	75

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SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 2.51
EFFECTIVE AREA(ACRES) = 4.00 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50
TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 7.73

FLOW PROCESS FROM NODE 115.00 TO NODE 116.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 310.80 DOWNSTREAM(FEET) = 247.20
FLOW LENGTH(FEET) = 825.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.35
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.73
PIPE TRAVEL TIME(MIN.) = 1.03 Tc(MIN.) = 15.06
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 116.00 = 1530.00 FEET.

FLOW PROCESS FROM NODE 116.00 TO NODE 116.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====
MAINLINE Tc(MIN.) = 15.06
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.158
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 4.60 0.20 0.500 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.461
SUBAREA AREA(ACRES) = 5.10 SUBAREA RUNOFF(CFS) = 9.48
EFFECTIVE AREA(ACRES) = 9.10 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 9.1 PEAK FLOW RATE(CFS) = 16.89

FLOW PROCESS FROM NODE 116.00 TO NODE 117.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 247.20 DOWNSTREAM(FEET) = 234.20
FLOW LENGTH(FEET) = 765.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.16
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 16.89
PIPE TRAVEL TIME(MIN.) = 1.39 Tc(MIN.) = 16.45
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 117.00 = 2295.00 FEET.

FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====
MAINLINE Tc(MIN.) = 16.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.052
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.00 0.20 0.500 75
COMMERCIAL D 0.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.386
SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 2.49

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EFFECTIVE AREA(ACRES) = 10.50 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 10.5 PEAK FLOW RATE(CFS) = 18.51

FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 16.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.052
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 3.10 0.20 0.500 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 3.10 SUBAREA RUNOFF(CFS) = 5.44
EFFECTIVE AREA(ACRES) = 13.60 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 13.6 PEAK FLOW RATE(CFS) = 23.95

FLOW PROCESS FROM NODE 117.00 TO NODE 125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 234.20 DOWNSTREAM(FEET) = 228.00
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.99
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.95
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 16.56
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 125.00 = 2395.00 FEET.

FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.56
RAINFALL INTENSITY(INCH/HR) = 2.04
AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.47
EFFECTIVE STREAM AREA(ACRES) = 13.60
TOTAL STREAM AREA(ACRES) = 13.60
PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.95

FLOW PROCESS FROM NODE 118.00 TO NODE 119.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 275.00
ELEVATION DATA: UPSTREAM(FEET) = 336.00 DOWNSTREAM(FEET) = 328.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.463
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.227
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.70 0.20 0.500 75 7.46
PUBLIC PARK D 0.20 0.20 0.850 75 9.27
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.537
SUBAREA RUNOFF(CFS) = 5.33
TOTAL AREA(ACRES) = 1.90 PEAK FLOW RATE(CFS) = 5.33

FLOW PROCESS FROM NODE 119.00 TO NODE 120.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 328.00 DOWNSTREAM ELEVATION(FEET) = 307.00
STREET LENGTH(FEET) = 675.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.07
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.33
HALFSTREET FLOOD WIDTH(FEET) = 10.08
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.00
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.31
STREET FLOW TRAVEL TIME(MIN.) = 2.81 Tc(MIN.) = 10.28
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.686

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 3.20 0.20 0.500 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 3.20 SUBAREA RUNOFF(CFS) = 7.45
EFFECTIVE AREA(ACRES) = 5.10 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51
TOTAL AREA(ACRES) = 5.1 PEAK FLOW RATE(CFS) = 11.86

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.34
FLOW VELOCITY(FEET/SEC.) = 4.22 DEPTH*VELOCITY(FT*FT/SEC.) = 1.49
LONGEST FLOWPATH FROM NODE 118.00 TO NODE 120.00 = 950.00 FEET.

FLOW PROCESS FROM NODE 120.00 TO NODE 121.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 307.00 DOWNSTREAM ELEVATION(FEET) = 301.00
STREET LENGTH(FEET) = 115.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.99
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 12.06
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.72
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.10

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STREET FLOW TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 10.61
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.638

SUBAREA LOSS RATE DATA(AMC II):

Table with columns: DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN. Rows include Residential (5-7 dwellings/acre), Public Park, and Commercial.

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.59
FLOW VELOCITY(FEET/SEC.) = 6.09 DEPTH*VELOCITY(FT*FT/SEC.) = 2.42
LONGEST FLOWPATH FROM NODE 118.00 TO NODE 121.00 = 1065.00 FEET.

FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 296.00 DOWNSTREAM(FEET) = 280.00
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.89
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.91
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 10.80
LONGEST FLOWPATH FROM NODE 118.00 TO NODE 122.00 = 1265.00 FEET.

FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 280.00 DOWNSTREAM ELEVATION(FEET) = 262.00
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 34.22

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.53
HALFSTREET FLOOD WIDTH(FEET) = 20.82
AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.42
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 4.50
STREET FLOW TRAVEL TIME(MIN.) = 0.53 Tc(MIN.) = 11.33
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.540

SUBAREA LOSS RATE DATA(AMC II):

Table with columns: DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN. Rows include Residential (5-7 dwellings/acre), Public Park, and Commercial.

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EFFECTIVE AREA(ACRES) = 19.90 AREA-AVERAGED Fm(INCH/HR) = 0.10
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.52
 TOTAL AREA(ACRES) = 19.9 PEAK FLOW RATE(CFS) = 43.61

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.57 HALFSTREET FLOOD WIDTH(FEET) = 22.85
 FLOW VELOCITY(FEET/SEC.) = 8.98 DEPTH*VELOCITY(FT*FT/SEC.) = 5.12
 LONGEST FLOWPATH FROM NODE 118.00 TO NODE 123.00 = 1535.00 FEET.

 FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 262.00 DOWNSTREAM ELEVATION(FEET) = 239.00
 STREET LENGTH(FEET) = 250.00 CURB HEIGHT(INCHES) = 8.0
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 44.16
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.55
 HALFSTREET FLOOD WIDTH(FEET) = 21.60
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 10.13
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 5.55
 STREET FLOW TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 11.74
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.489

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	D	0.20	0.20	0.850	75
COMMERCIAL	D	0.30	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
 SUBAREA AREA(ACRES) = 0.50 SUBAREA RUNOFF(CFS) = 1.08
 EFFECTIVE AREA(ACRES) = 20.40 AREA-AVERAGED Fm(INCH/HR) = 0.10
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.52
 TOTAL AREA(ACRES) = 20.4 PEAK FLOW RATE(CFS) = 43.78

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.55 HALFSTREET FLOOD WIDTH(FEET) = 21.52
 FLOW VELOCITY(FEET/SEC.) = 10.11 DEPTH*VELOCITY(FT*FT/SEC.) = 5.53
 LONGEST FLOWPATH FROM NODE 118.00 TO NODE 124.00 = 1785.00 FEET.

 FLOW PROCESS FROM NODE 124.00 TO NODE 125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 232.60 DOWNSTREAM(FEET) = 228.00
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.44
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 43.78
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 11.80
 LONGEST FLOWPATH FROM NODE 118.00 TO NODE 125.00 = 1855.00 FEET.

 FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

DPHOSR2

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 11.80
RAINFALL INTENSITY(INCH/HR) = 2.48
AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.52
EFFECTIVE STREAM AREA(ACRES) = 20.40
TOTAL STREAM AREA(ACRES) = 20.40
PEAK FLOW RATE(CFS) AT CONFLUENCE = 43.78
```

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	23.95	16.56	2.044	0.20(0.09)	0.47	13.6	112.00
2	43.78	11.80	2.481	0.20(0.10)	0.52	20.4	118.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	64.69	11.80	2.481	0.20(0.10)	0.51	30.1	118.00
2	59.68	16.56	2.044	0.20(0.10)	0.50	34.0	112.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```
PEAK FLOW RATE(CFS) = 64.69 Tc(MIN.) = 11.80
EFFECTIVE AREA(ACRES) = 30.10 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51
TOTAL AREA(ACRES) = 34.0
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 125.00 = 2395.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 125.00 TO NODE 132.00 IS CODE = 31
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 228.00 DOWNSTREAM(FEET) = 224.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.10
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 64.69
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 11.84
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 132.00 = 2445.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1
```

```
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
```

```
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.84
RAINFALL INTENSITY(INCH/HR) = 2.48
AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.51
EFFECTIVE STREAM AREA(ACRES) = 30.10
TOTAL STREAM AREA(ACRES) = 34.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 64.69
```

```
*****
FLOW PROCESS FROM NODE 126.00 TO NODE 127.00 IS CODE = 21
```

```
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
```

```
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 322.00 DOWNSTREAM(FEET) = 320.50
```

DPHOSR2

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.589
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.977

SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 0.40 0.20 0.200 75 9.15
COMMERCIAL D 0.20 0.20 0.100 75 8.59
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.167
SUBAREA RUNOFF(CFS) = 1.59
TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.59

FLOW PROCESS FROM NODE 127.00 TO NODE 128.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 320.50 DOWNSTREAM ELEVATION(FEET) = 318.00
STREET LENGTH(FEET) = 600.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.65
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.77
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.60
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.63
STREET FLOW TRAVEL TIME(MIN.) = 6.23 Tc(MIN.) = 14.82
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.178

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.40 0.20 0.500 75
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 0.20 0.20 0.200 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.264
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.10
EFFECTIVE AREA(ACRES) = 1.70 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.23
TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 3.26

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.02
FLOW VELOCITY(FEET/SEC.) = 1.67 DEPTH*VELOCITY(FT*FT/SEC.) = 0.69
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 128.00 = 900.00 FEET.

FLOW PROCESS FROM NODE 128.00 TO NODE 129.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 318.00 DOWNSTREAM ELEVATION(FEET) = 302.00
STREET LENGTH(FEET) = 640.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.75
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.42
HALFSTREET FLOOD WIDTH(FEET) = 14.57
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.19
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.77
STREET FLOW TRAVEL TIME(MIN.) = 2.55 Tc(MIN.) = 17.37
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.989

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 5.50 0.20 0.500 75
COMMERCIAL D 0.90 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.444
SUBAREA AREA(ACRES) = 6.40 SUBAREA RUNOFF(CFS) = 10.94
EFFECTIVE AREA(ACRES) = 8.10 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 8.1 PEAK FLOW RATE(CFS) = 13.92

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 17.62
FLOW VELOCITY(FEET/SEC.) = 4.69 DEPTH*VELOCITY(FT*FT/SEC.) = 2.24
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 129.00 = 1540.00 FEET.

FLOW PROCESS FROM NODE 129.00 TO NODE 130.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 302.00 DOWNSTREAM ELEVATION(FEET) = 264.00
STREET LENGTH(FEET) = 450.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 19.54
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.45
HALFSTREET FLOOD WIDTH(FEET) = 15.82
AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.05
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.58
STREET FLOW TRAVEL TIME(MIN.) = 0.93 Tc(MIN.) = 18.30
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.930

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 6.10 0.20 0.500 75
COMMERCIAL D 0.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.459
SUBAREA AREA(ACRES) = 6.80 SUBAREA RUNOFF(CFS) = 11.25
EFFECTIVE AREA(ACRES) = 14.90 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.43
TOTAL AREA(ACRES) = 14.9 PEAK FLOW RATE(CFS) = 24.74

DPHOSR2

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 17.38
 FLOW VELOCITY(FEET/SEC.) = 8.55 DEPTH*VELOCITY(FT*FT/SEC.) = 4.05
 LONGEST FLOWPATH FROM NODE 126.00 TO NODE 130.00 = 1990.00 FEET.

 FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 264.00 DOWNSTREAM ELEVATION(FEET) = 242.00
 STREET LENGTH(FEET) = 310.00 CURB HEIGHT(INCHES) = 8.0
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 25.08

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.49
 HALFSTREET FLOOD WIDTH(FEET) = 18.09
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.05
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.91
 STREET FLOW TRAVEL TIME(MIN.) = 0.64 Tc(MIN.) = 18.95
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.892

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.40	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.67
 EFFECTIVE AREA(ACRES) = 15.30 AREA-AVERAGED Fm(INCH/HR) = 0.08
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.42
 TOTAL AREA(ACRES) = 15.3 PEAK FLOW RATE(CFS) = 24.91

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.09
 FLOW VELOCITY(FEET/SEC.) = 8.00 DEPTH*VELOCITY(FT*FT/SEC.) = 3.88
 LONGEST FLOWPATH FROM NODE 126.00 TO NODE 131.00 = 2300.00 FEET.

 FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 237.10 DOWNSTREAM(FEET) = 224.00
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.1 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 28.36
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 24.91
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 18.97
 LONGEST FLOWPATH FROM NODE 126.00 TO NODE 132.00 = 2350.00 FEET.

 FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 18.97

DPHOSR2

3	136.01	12.21	2.434	0.20(0.10)	0.48	63.5	118.00
4	124.96	16.97	2.016	0.20(0.09)	0.47	71.3	112.00
5	118.45	19.35	1.870	0.20(0.09)	0.47	73.2	126.00
TOTAL AREA(ACRES) =			73.2				

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 136.01 Tc(MIN.) = 12.212
EFFECTIVE AREA(ACRES) = 63.54 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 73.2
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 106.00 = 2890.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 135.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 202.30 DOWNSTREAM(FEET) = 141.50
FLOW LENGTH(FEET) = 1090.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.96
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 136.01
PIPE TRAVEL TIME(MIN.) = 0.76 Tc(MIN.) = 12.97
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 135.00 = 3980.00 FEET.

FLOW PROCESS FROM NODE 135.00 TO NODE 135.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 12.97
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.351
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	D	5.70	0.20	0.400	75
COMMERCIAL	D	0.60	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.371
SUBAREA AREA(ACRES) = 6.30 SUBAREA RUNOFF(CFS) = 12.91
EFFECTIVE AREA(ACRES) = 69.84 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 79.5 PEAK FLOW RATE(CFS) = 141.91

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	136.87	8.37	3.023	0.20(0.09)	0.46	51.9	107.00
2	141.96	11.94	2.465	0.20(0.09)	0.47	66.5	101.00
3	141.91	12.97	2.351	0.20(0.09)	0.47	69.8	118.00
4	130.72	17.73	1.965	0.20(0.09)	0.47	77.6	112.00
5	124.06	20.15	1.827	0.20(0.09)	0.46	79.5	126.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE(CFS) = 141.96 Tc(MIN.) = 11.94
AREA-AVERAGED Fm(INCH/HR) = 0.09 AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.47 EFFECTIVE AREA(ACRES) = 66.50

FLOW PROCESS FROM NODE 135.00 TO NODE 144.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 141.50 DOWNSTREAM(FEET) = 141.00
FLOW LENGTH(FEET) = 15.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 31.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.65
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 141.96
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 11.95

DPHOSR2
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 144.00 = 3995.00 FEET.

FLOW PROCESS FROM NODE 144.00 TO NODE 144.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	11.95
RAINFALL INTENSITY(INCH/HR) =	2.46
AREA-AVERAGED Fm(INCH/HR) =	0.09
AREA-AVERAGED Fp(INCH/HR) =	0.20
AREA-AVERAGED Ap =	0.47
EFFECTIVE STREAM AREA(ACRES) =	66.50
TOTAL STREAM AREA(ACRES) =	79.50
PEAK FLOW RATE(CFS) AT CONFLUENCE =	141.96

FLOW PROCESS FROM NODE 136.00 TO NODE 137.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) =	230.00
ELEVATION DATA: UPSTREAM(FEET) =	335.00
DOWNSTREAM(FEET) =	332.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20						
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =	6.794					
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	3.405					
SUBAREA Tc AND LOSS RATE DATA(AMC II):						
DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS	Tc
LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN	(MIN.)
RESIDENTIAL						
"11+ DWELLINGS/ACRE"	D	3.20	0.20	0.200	75	6.79
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =	0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =	0.200					
SUBAREA RUNOFF(CFS) =	9.69					
TOTAL AREA(ACRES) =	3.20	PEAK FLOW RATE(CFS) =	9.69			

FLOW PROCESS FROM NODE 137.00 TO NODE 138.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	332.00
DOWNSTREAM ELEVATION(FEET) =	308.00
STREET LENGTH(FEET) =	575.00
CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =	5.00
INSIDE STREET CROSSFALL(DECIMAL) =	0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =	0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =	1
STREET PARKWAY CROSSFALL(DECIMAL) =	0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =	0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =	0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	13.16
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:	
STREET FLOW DEPTH(FEET) =	0.42
HALFSTREET FLOOD WIDTH(FEET) =	14.76
AVERAGE FLOW VELOCITY(FEET/SEC.) =	5.73
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =	2.42
STREET FLOW TRAVEL TIME(MIN.) =	1.67
Tc(MIN.) =	8.47
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	3.002

SUBAREA LOSS RATE DATA(AMC II):					
DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS
LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
RESIDENTIAL					
"11+ DWELLINGS/ACRE"	D	2.60	0.20	0.200	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =	0.20				

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA(ACRES) = 2.60 SUBAREA RUNOFF(CFS) = 6.93
EFFECTIVE AREA(ACRES) = 5.80 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 5.8 PEAK FLOW RATE(CFS) = 15.46

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 15.70
FLOW VELOCITY(FEET/SEC.) = 5.99 DEPTH*VELOCITY(FT*FT/SEC.) = 2.64
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 138.00 = 805.00 FEET.

FLOW PROCESS FROM NODE 138.00 TO NODE 139.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 308.00 DOWNSTREAM ELEVATION(FEET) = 280.00
STREET LENGTH(FEET) = 440.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 22.35
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.48
HALFSTREET FLOOD WIDTH(FEET) = 17.70
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.47
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.58
STREET FLOW TRAVEL TIME(MIN.) = 0.98 Tc(MIN.) = 9.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.819

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 4.80 0.20 0.200 75
COMMERCIAL D 0.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.187
SUBAREA AREA(ACRES) = 5.50 SUBAREA RUNOFF(CFS) = 13.77
EFFECTIVE AREA(ACRES) = 11.30 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 11.3 PEAK FLOW RATE(CFS) = 28.28

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.51 HALFSTREET FLOOD WIDTH(FEET) = 19.41
FLOW VELOCITY(FEET/SEC.) = 7.94 DEPTH*VELOCITY(FT*FT/SEC.) = 4.05
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 139.00 = 1245.00 FEET.

FLOW PROCESS FROM NODE 139.00 TO NODE 140.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 280.00 DOWNSTREAM ELEVATION(FEET) = 255.00
STREET LENGTH(FEET) = 425.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

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Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 29.69
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.52
HALFSTREET FLOOD WIDTH(FEET) = 20.12
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.80
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 4.07
STREET FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 10.36
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.675

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.50 0.20 0.500 75
COMMERCIAL D 0.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.267
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 2.83
EFFECTIVE AREA(ACRES) = 12.50 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 12.5 PEAK FLOW RATE(CFS) = 29.64

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.52 HALFSTREET FLOOD WIDTH(FEET) = 20.12
FLOW VELOCITY(FEET/SEC.) = 7.78 DEPTH*VELOCITY(FT*FT/SEC.) = 4.06
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 140.00 = 1670.00 FEET.

FLOW PROCESS FROM NODE 140.00 TO NODE 141.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 257.00 DOWNSTREAM(FEET) = 250.00
FLOW LENGTH(FEET) = 95.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.50
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 29.64
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.44
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 141.00 = 1765.00 FEET.

FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 250.00 DOWNSTREAM ELEVATION(FEET) = 160.00
STREET LENGTH(FEET) = 1225.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 41.58
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.56
HALFSTREET FLOOD WIDTH(FEET) = 21.99
AVERAGE FLOW VELOCITY(FEET/SEC.) = 9.21
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 5.12
STREET FLOW TRAVEL TIME(MIN.) = 2.22 Tc(MIN.) = 12.66
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.384

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN

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RESIDENTIAL
 "8-10 DWELLINGS/ACRE" D 11.20 0.20 0.400 75
 COMMERCIAL D 0.30 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.392
 SUBAREA AREA(ACRES) = 11.50 SUBAREA RUNOFF(CFS) = 23.86
 EFFECTIVE AREA(ACRES) = 24.00 AREA-AVERAGED Fm(INCH/HR) = 0.06
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.29
 TOTAL AREA(ACRES) = 24.0 PEAK FLOW RATE(CFS) = 50.23

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.59 HALFSTREET FLOOD WIDTH(FEET) = 23.71
 FLOW VELOCITY(FEET/SEC.) = 9.63 DEPTH*VELOCITY(FT*FT/SEC.) = 5.65
 LONGEST FLOWPATH FROM NODE 136.00 TO NODE 142.00 = 2990.00 FEET.

 FLOW PROCESS FROM NODE 142.00 TO NODE 143.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 150.00 DOWNSTREAM(FEET) = 145.00
 FLOW LENGTH(FEET) = 285.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.9 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 11.97
 ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 50.23
 PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 13.05
 LONGEST FLOWPATH FROM NODE 136.00 TO NODE 143.00 = 3275.00 FEET.

 FLOW PROCESS FROM NODE 143.00 TO NODE 143.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
 =====
 MAINLINE Tc(MIN.) = 13.05
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.342
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 RESIDENTIAL
 "8-10 DWELLINGS/ACRE" D 5.60 0.20 0.400 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
 SUBAREA AREA(ACRES) = 5.60 SUBAREA RUNOFF(CFS) = 11.40
 EFFECTIVE AREA(ACRES) = 29.60 AREA-AVERAGED Fm(INCH/HR) = 0.06
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.31
 TOTAL AREA(ACRES) = 29.6 PEAK FLOW RATE(CFS) = 60.73

 FLOW PROCESS FROM NODE 143.00 TO NODE 144.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 145.00 DOWNSTREAM(FEET) = 141.00
 FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.7 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 23.17
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 60.73
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 13.09
 LONGEST FLOWPATH FROM NODE 136.00 TO NODE 144.00 = 3320.00 FEET.

 FLOW PROCESS FROM NODE 144.00 TO NODE 144.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
 =====
 TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 13.09

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RAINFALL INTENSITY(INCH/HR) = 2.34
AREA-AVERAGED Fm(INCH/HR) = 0.06
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.31
EFFECTIVE STREAM AREA(ACRES) = 29.60
TOTAL STREAM AREA(ACRES) = 29.60
PEAK FLOW RATE(CFS) AT CONFLUENCE = 60.73

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 6 rows of data for different stream nodes.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 6 rows of data for different stream nodes.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 202.44 Tc(MIN.) = 12.98
EFFECTIVE AREA(ACRES) = 99.21 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 109.1
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 144.00 = 3995.00 FEET.

FLOW PROCESS FROM NODE 144.00 TO NODE 145.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
ELEVATION DATA: UPSTREAM(FEET) = 141.00 DOWNSTREAM(FEET) = 139.00
FLOW LENGTH(FEET) = 325.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 63.0 INCH PIPE IS 47.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.57
ESTIMATED PIPE DIAMETER(INCH) = 63.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 202.44
PIPE TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 13.45
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 145.00 = 4320.00 FEET.

FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.45
RAINFALL INTENSITY(INCH/HR) = 2.30
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.42
EFFECTIVE STREAM AREA(ACRES) = 99.21
TOTAL STREAM AREA(ACRES) = 109.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 202.44

FLOW PROCESS FROM NODE 146.00 TO NODE 147.00 IS CODE = 21

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>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 270.00
ELEVATION DATA: UPSTREAM(FEET) = 218.00 DOWNSTREAM(FEET) = 216.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.364
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.833
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.20 0.20 0.400 75 9.36
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA RUNOFF(CFS) = 2.97
TOTAL AREA(ACRES) = 1.20 PEAK FLOW RATE(CFS) = 2.97

FLOW PROCESS FROM NODE 147.00 TO NODE 148.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 216.00 DOWNSTREAM ELEVATION(FEET) = 210.00
STREET LENGTH(FEET) = 405.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.50
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.38
HALFSTREET FLOOD WIDTH(FEET) = 12.78
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.14
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.20
STREET FLOW TRAVEL TIME(MIN.) = 2.15 Tc(MIN.) = 11.51
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.517

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 2.30 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 2.30 SUBAREA RUNOFF(CFS) = 5.05
EFFECTIVE AREA(ACRES) = 3.50 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 7.68

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.60
FLOW VELOCITY(FEET/SEC.) = 3.41 DEPTH*VELOCITY(FT*FT/SEC.) = 1.43
LONGEST FLOWPATH FROM NODE 146.00 TO NODE 148.00 = 675.00 FEET.

FLOW PROCESS FROM NODE 148.00 TO NODE 149.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 210.00 DOWNSTREAM ELEVATION(FEET) = 175.00
STREET LENGTH(FEET) = 475.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.64
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.61
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.58
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.36
STREET FLOW TRAVEL TIME(MIN.) = 1.20 Tc(MIN.) = 12.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.378

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.90 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 3.93
EFFECTIVE AREA(ACRES) = 5.40 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 5.4 PEAK FLOW RATE(CFS) = 11.17

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.33
FLOW VELOCITY(FEET/SEC.) = 6.82 DEPTH*VELOCITY(FT*FT/SEC.) = 2.54
LONGEST FLOWPATH FROM NODE 146.00 TO NODE 149.00 = 1150.00 FEET.

FLOW PROCESS FROM NODE 149.00 TO NODE 149.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 12.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.378
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.50 0.20 0.400 75
COMMERCIAL D 1.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.255
SUBAREA AREA(ACRES) = 2.90 SUBAREA RUNOFF(CFS) = 6.07
EFFECTIVE AREA(ACRES) = 8.30 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA(ACRES) = 8.3 PEAK FLOW RATE(CFS) = 17.24

FLOW PROCESS FROM NODE 149.00 TO NODE 145.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 175.00 DOWNSTREAM ELEVATION(FEET) = 146.00
STREET LENGTH(FEET) = 580.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 25.63

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STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.51
 HALFSTREET FLOOD WIDTH(FEET) = 19.65
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.04
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.61
 STREET FLOW TRAVEL TIME(MIN.) = 1.37 Tc(MIN.) = 14.09
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.242
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 RESIDENTIAL
 "8-10 DWELLINGS/ACRE" D 7.90 0.20 0.400 75
 COMMERCIAL D 0.70 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.376
 SUBAREA AREA(ACRES) = 8.60 SUBAREA RUNOFF(CFS) = 16.77
 EFFECTIVE AREA(ACRES) = 16.90 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
 TOTAL AREA(ACRES) = 16.9 PEAK FLOW RATE(CFS) = 33.00

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.55 HALFSTREET FLOOD WIDTH(FEET) = 21.68
 FLOW VELOCITY(FEET/SEC.) = 7.52 DEPTH*VELOCITY(FT*FT/SEC.) = 4.13
 LONGEST FLOWPATH FROM NODE 146.00 TO NODE 145.00 = 1730.00 FEET.

 FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
 =====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 14.09
 RAINFALL INTENSITY(INCH/HR) = 2.24
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.36
 EFFECTIVE STREAM AREA(ACRES) = 16.90
 TOTAL STREAM AREA(ACRES) = 16.90
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 33.00

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	187.38	8.86	2.925	0.20(0.08)	0.42	70.9	107.00
1	200.47	12.42	2.410	0.20(0.08)	0.42	93.5	101.00
1	202.44	13.45	2.302	0.20(0.08)	0.42	99.2	118.00
1	202.40	13.56	2.292	0.20(0.08)	0.42	99.6	136.00
1	181.46	18.23	1.934	0.20(0.08)	0.42	107.2	112.00
1	171.11	20.65	1.801	0.20(0.08)	0.42	109.1	126.00
2	33.00	14.09	2.242	0.20(0.07)	0.36	16.9	146.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	214.67	8.86	2.925	0.20(0.08)	0.42	81.5	107.00
2	231.81	12.42	2.410	0.20(0.08)	0.41	108.4	101.00
3	234.82	13.45	2.302	0.20(0.08)	0.41	115.3	118.00
4	234.88	13.56	2.292	0.20(0.08)	0.41	115.9	136.00
5	233.01	14.09	2.242	0.20(0.08)	0.41	117.4	146.00
6	209.78	18.23	1.934	0.20(0.08)	0.41	124.1	112.00
7	197.40	20.65	1.801	0.20(0.08)	0.41	126.0	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 234.88 Tc(MIN.) = 13.56
 EFFECTIVE AREA(ACRES) = 115.87 AREA-AVERAGED Fm(INCH/HR) = 0.08
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
 TOTAL AREA(ACRES) = 126.0
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 145.00 = 4320.00 FEET.

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*****
FLOW PROCESS FROM NODE 145.00 TO NODE 150.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 139.00 DOWNSTREAM(FEET) = 125.00
FLOW LENGTH(FEET) = 780.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 54.0 INCH PIPE IS 41.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.87
ESTIMATED PIPE DIAMETER(INCH) = 54.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 234.88
PIPE TRAVEL TIME(MIN.) = 0.73 Tc(MIN.) = 14.28
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 150.00 = 5100.00 FEET.
*****
FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.28
RAINFALL INTENSITY(INCH/HR) = 2.22
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.41
EFFECTIVE STREAM AREA(ACRES) = 115.87
TOTAL STREAM AREA(ACRES) = 126.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 234.88
*****
FLOW PROCESS FROM NODE 151.00 TO NODE 152.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 235.00 DOWNSTREAM(FEET) = 230.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.751
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.418
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
PUBLIC PARK D 0.30 0.20 0.850 75 10.73
COMMERCIAL D 0.30 0.20 0.100 75 6.75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.475
SUBAREA RUNOFF(CFS) = 1.79
TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.79
*****
FLOW PROCESS FROM NODE 152.00 TO NODE 153.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 230.00 DOWNSTREAM ELEVATION(FEET) = 195.00
STREET LENGTH(FEET) = 390.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

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**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.02
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 6.22
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.61
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.53
STREET FLOW TRAVEL TIME(MIN.) = 1.16 Tc(MIN.) = 7.91
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.121

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK D 0.40 0.20 0.850 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.433
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 2.46
EFFECTIVE AREA(ACRES) = 1.50 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.45
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 4.09

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 7.47
FLOW VELOCITY(FEET/SEC.) = 5.91 DEPTH*VELOCITY(FT*FT/SEC.) = 1.75
LONGEST FLOWPATH FROM NODE 151.00 TO NODE 153.00 = 690.00 FEET.

FLOW PROCESS FROM NODE 153.00 TO NODE 154.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 195.00 DOWNSTREAM ELEVATION(FEET) = 180.00
STREET LENGTH(FEET) = 275.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.88
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.88
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.81
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.11
STREET FLOW TRAVEL TIME(MIN.) = 0.79 Tc(MIN.) = 8.70
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.956

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 3.70 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 3.70 SUBAREA RUNOFF(CFS) = 9.58
EFFECTIVE AREA(ACRES) = 5.20 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 5.2 PEAK FLOW RATE(CFS) = 13.45

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.13
FLOW VELOCITY(FEET/SEC.) = 6.36 DEPTH*VELOCITY(FT*FT/SEC.) = 2.60
LONGEST FLOWPATH FROM NODE 151.00 TO NODE 154.00 = 965.00 FEET.

FLOW PROCESS FROM NODE 154.00 TO NODE 155.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

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>>>>(STREET TABLE SECTION # 2 USED)<<<<

UPSTREAM ELEVATION(FEET) = 180.00 DOWNSTREAM ELEVATION(FEET) = 175.00
STREET LENGTH(FEET) = 125.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 21.04
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.48
HALFSTREET FLOOD WIDTH(FEET) = 17.88
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.35
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.07
STREET FLOW TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 9.03
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.894

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 6.00 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 6.00 SUBAREA RUNOFF(CFS) = 15.19
EFFECTIVE AREA(ACRES) = 11.20 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 11.2 PEAK FLOW RATE(CFS) = 28.35

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.00
FLOW VELOCITY(FEET/SEC.) = 6.35 DEPTH*VELOCITY(FT*FT/SEC.) = 3.09
LONGEST FLOWPATH FROM NODE 151.00 TO NODE 155.00 = 1090.00 FEET.

FLOW PROCESS FROM NODE 155.00 TO NODE 156.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

UPSTREAM ELEVATION(FEET) = 175.00 DOWNSTREAM ELEVATION(FEET) = 139.00
STREET LENGTH(FEET) = 570.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 41.26
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.45
HALFSTREET FLOOD WIDTH(FEET) = 16.24
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.48
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.38
STREET FLOW TRAVEL TIME(MIN.) = 1.27 Tc(MIN.) = 10.30
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.684

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 3.90 0.20 0.400 75
RESIDENTIAL

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"11+ DWELLINGS/ACRE" D 6.20 0.20 0.200 75
 COMMERCIAL D 0.80 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.264
 SUBAREA AREA(ACRES) = 10.90 SUBAREA RUNOFF(CFS) = 25.81
 EFFECTIVE AREA(ACRES) = 22.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.34
 TOTAL AREA(ACRES) = 22.1 PEAK FLOW RATE(CFS) = 52.04

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 17.80
 FLOW VELOCITY(FEET/SEC.) = 7.91 DEPTH*VELOCITY(FT*FT/SEC.) = 3.82
 LONGEST FLOWPATH FROM NODE 151.00 TO NODE 156.00 = 1660.00 FEET.

 FLOW PROCESS FROM NODE 156.00 TO NODE 150.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 133.50 DOWNSTREAM(FEET) = 125.00
 FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 31.62
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 52.04
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 10.32
 LONGEST FLOWPATH FROM NODE 151.00 TO NODE 150.00 = 1700.00 FEET.

 FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
 =====
 TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 10.32
 RAINFALL INTENSITY(INCH/HR) = 2.68
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.34
 EFFECTIVE STREAM AREA(ACRES) = 22.10
 TOTAL STREAM AREA(ACRES) = 22.10
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 52.04

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	214.67	9.60	2.794	0.20(0.08)	0.42	81.5	107.00
1	231.81	13.15	2.333	0.20(0.08)	0.41	108.4	101.00
1	234.82	14.18	2.234	0.20(0.08)	0.41	115.3	118.00
1	234.88	14.28	2.225	0.20(0.08)	0.41	115.9	136.00
1	233.01	14.82	2.178	0.20(0.08)	0.41	117.4	146.00
1	209.78	18.98	1.890	0.20(0.08)	0.41	124.1	112.00
1	197.40	21.40	1.765	0.20(0.08)	0.41	126.0	126.00
2	52.04	10.32	2.680	0.20(0.07)	0.34	22.1	151.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	265.17	9.60	2.794	0.20(0.08)	0.40	102.0	107.00
2	270.18	10.32	2.680	0.20(0.08)	0.40	109.0	151.00
3	276.92	13.15	2.333	0.20(0.08)	0.40	130.5	101.00
4	277.97	14.18	2.234	0.20(0.08)	0.40	137.4	118.00
5	277.84	14.28	2.225	0.20(0.08)	0.40	138.0	136.00
6	275.04	14.82	2.178	0.20(0.08)	0.40	139.5	146.00
7	246.08	18.98	1.890	0.20(0.08)	0.40	146.2	112.00
8	231.20	21.40	1.765	0.20(0.08)	0.40	148.1	126.00

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COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 277.97 Tc(MIN.) = 14.18
EFFECTIVE AREA(ACRES) = 137.44 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 148.1
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 150.00 = 5100.00 FEET.

FLOW PROCESS FROM NODE 150.00 TO NODE 159.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 125.00 DOWNSTREAM(FEET) = 102.00
FLOW LENGTH(FEET) = 610.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 51.0 INCH PIPE IS 37.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.79
ESTIMATED PIPE DIAMETER(INCH) = 51.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 277.97
PIPE TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 14.59
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 159.00 = 5710.00 FEET.

FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 14.59
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.198
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 5.10 0.20 0.400 75
COMMERCIAL D 3.30 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.282
SUBAREA AREA(ACRES) = 8.40 SUBAREA RUNOFF(CFS) = 16.19
EFFECTIVE AREA(ACRES) = 145.84 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 156.5 PEAK FLOW RATE(CFS) = 278.14

FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.59
RAINFALL INTENSITY(INCH/HR) = 2.20
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.39
EFFECTIVE STREAM AREA(ACRES) = 145.84
TOTAL STREAM AREA(ACRES) = 156.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 278.14

FLOW PROCESS FROM NODE 160.00 TO NODE 161.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 260.00
ELEVATION DATA: UPSTREAM(FEET) = 145.00 DOWNSTREAM(FEET) = 143.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.441
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.232
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)

DPHOSR2

COMMERCIAL D 0.50 0.20 0.100 75 7.44
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 1.45
TOTAL AREA(ACRES) = 0.50 PEAK FLOW RATE(CFS) = 1.45

FLOW PROCESS FROM NODE 161.00 TO NODE 162.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 143.00 DOWNSTREAM ELEVATION(FEET) = 138.00
STREET LENGTH(FEET) = 345.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.58
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.05
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.79
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.00
STREET FLOW TRAVEL TIME(MIN.) = 2.06 Tc(MIN.) = 9.50
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.810

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 1.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 4.27
EFFECTIVE AREA(ACRES) = 2.20 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 5.52

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.40
FLOW VELOCITY(FEET/SEC.) = 3.07 DEPTH*VELOCITY(FT*FT/SEC.) = 1.24
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 162.00 = 605.00 FEET.

FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 9.50
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.810
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 2.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.50 SUBAREA RUNOFF(CFS) = 6.28
EFFECTIVE AREA(ACRES) = 4.70 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 4.7 PEAK FLOW RATE(CFS) = 11.80

FLOW PROCESS FROM NODE 162.00 TO NODE 163.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

DPHOSR2

ELEVATION DATA: UPSTREAM(FEET) = 132.00 DOWNSTREAM(FEET) = 127.00
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.77
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.80
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 9.60
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 163.00 = 685.00 FEET.

FLOW PROCESS FROM NODE 163.00 TO NODE 163.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 9.60
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.793
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 1.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 4.24
EFFECTIVE AREA(ACRES) = 6.40 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 6.4 PEAK FLOW RATE(CFS) = 15.97

FLOW PROCESS FROM NODE 163.00 TO NODE 164.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 127.00 DOWNSTREAM(FEET) = 117.50
FLOW LENGTH(FEET) = 350.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.59
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.97
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 10.15
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 164.00 = 1035.00 FEET.

FLOW PROCESS FROM NODE 164.00 TO NODE 164.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 10.15
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.706
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.40 0.20 0.400 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.321
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 4.52
EFFECTIVE AREA(ACRES) = 8.30 AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.15
TOTAL AREA(ACRES) = 8.3 PEAK FLOW RATE(CFS) = 19.99

FLOW PROCESS FROM NODE 164.00 TO NODE 165.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 117.50 DOWNSTREAM(FEET) = 114.50
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.78
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

DPHOSR2

PIPE-FLOW(CFS) = 19.99
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 10.18
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 165.00 = 1070.00 FEET.

FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 10.18
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.701
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 2.20 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 5.31
EFFECTIVE AREA(ACRES) = 10.50 AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.14
TOTAL AREA(ACRES) = 10.5 PEAK FLOW RATE(CFS) = 25.26

FLOW PROCESS FROM NODE 165.00 TO NODE 159.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 114.50 DOWNSTREAM(FEET) = 102.00
FLOW LENGTH(FEET) = 220.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.14
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 25.26
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 10.41
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 159.00 = 1290.00 FEET.

FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.41
RAINFALL INTENSITY(INCH/HR) = 2.67
AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.14
EFFECTIVE STREAM AREA(ACRES) = 10.50
TOTAL STREAM AREA(ACRES) = 10.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 25.26

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists data for 2 streams and their confluence points.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE.

DPHOSR2							
1	290.01	10.01	2.727	0.20(0.07)	0.37	120.5	107.00
2	293.22	10.41	2.667	0.20(0.07)	0.37	124.9	160.00
3	295.00	10.73	2.621	0.20(0.07)	0.37	127.9	151.00
4	298.59	13.56	2.292	0.20(0.08)	0.38	149.4	101.00
5	298.90	14.59	2.198	0.20(0.08)	0.38	156.3	118.00
6	298.65	14.69	2.189	0.20(0.08)	0.38	156.9	136.00
7	295.30	15.23	2.144	0.20(0.08)	0.38	158.4	146.00
8	266.20	19.41	1.866	0.20(0.08)	0.38	165.1	112.00
9	250.98	21.83	1.745	0.20(0.08)	0.38	167.0	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 298.90 Tc(MIN.) = 14.59
EFFECTIVE AREA(ACRES) = 156.34 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.38
TOTAL AREA(ACRES) = 167.0
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 159.00 = 5710.00 FEET.

FLOW PROCESS FROM NODE 159.00 TO NODE 168.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 102.00 DOWNSTREAM(FEET) = 94.30
FLOW LENGTH(FEET) = 1005.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 69.0 INCH PIPE IS 53.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.76
ESTIMATED PIPE DIAMETER(INCH) = 69.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 298.90
PIPE TRAVEL TIME(MIN.) = 1.22 Tc(MIN.) = 15.81
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 168.00 = 6715.00 FEET.

FLOW PROCESS FROM NODE 168.00 TO NODE 168.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 15.81
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.099
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	7.50	0.20	0.100	75
PUBLIC PARK	D	0.20	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.119
SUBAREA AREA(ACRES) = 7.70 SUBAREA RUNOFF(CFS) = 14.38
EFFECTIVE AREA(ACRES) = 164.04 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.37
TOTAL AREA(ACRES) = 174.7 PEAK FLOW RATE(CFS) = 299.14

FLOW PROCESS FROM NODE 168.00 TO NODE 169.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 94.30 DOWNSTREAM(FEET) = 93.50
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 75.0 INCH PIPE IS 56.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.09
ESTIMATED PIPE DIAMETER(INCH) = 75.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 299.14
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 16.01
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 169.00 = 6865.00 FEET.

FLOW PROCESS FROM NODE 169.00 TO NODE 169.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

DPHOSR2

TIME OF CONCENTRATION(MIN.) = 16.01
 RAINFALL INTENSITY(INCH/HR) = 2.08
 AREA-AVERAGED F_m(INCH/HR) = 0.07
 AREA-AVERAGED F_p(INCH/HR) = 0.20
 AREA-AVERAGED A_p = 0.37
 EFFECTIVE STREAM AREA(ACRES) = 164.04
 TOTAL STREAM AREA(ACRES) = 174.70
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 299.14

 FLOW PROCESS FROM NODE 170.00 TO NODE 171.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
 ELEVATION DATA: UPSTREAM(FEET) = 145.00 DOWNSTREAM(FEET) = 140.00

T_c = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM T_c(MIN.) = 6.751
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.418
 SUBAREA T_c AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F _p (INCH/HR)	A _p (DECIMAL)	SCS CN	T _c (MIN.)
COMMERCIAL	D	0.90	0.20	0.100	75	6.75

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.100
 SUBAREA RUNOFF(CFS) = 2.75
 TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 2.75

 FLOW PROCESS FROM NODE 171.00 TO NODE 172.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 130.00 DOWNSTREAM(FEET) = 128.00
 FLOW LENGTH(FEET) = 265.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 9.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.24
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 2.75
 PIPE TRAVEL TIME(MIN.) = 1.04 T_c(MIN.) = 7.79
 LONGEST FLOWPATH FROM NODE 170.00 TO NODE 172.00 = 565.00 FEET.

 FLOW PROCESS FROM NODE 172.00 TO NODE 172.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE T_c(MIN.) = 7.79
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.148
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F _p (INCH/HR)	A _p (DECIMAL)	SCS CN
COMMERCIAL	D	3.10	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.100
 SUBAREA AREA(ACRES) = 3.10 SUBAREA RUNOFF(CFS) = 8.73
 EFFECTIVE AREA(ACRES) = 4.00 AREA-AVERAGED F_m(INCH/HR) = 0.02
 AREA-AVERAGED F_p(INCH/HR) = 0.20 AREA-AVERAGED A_p = 0.10
 TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 11.26

 FLOW PROCESS FROM NODE 172.00 TO NODE 169.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 128.00 DOWNSTREAM(FEET) = 93.50
 FLOW LENGTH(FEET) = 215.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.4 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.28

DPHOSR2

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.26
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 7.98
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 169.00 = 780.00 FEET.

FLOW PROCESS FROM NODE 169.00 TO NODE 169.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.98
RAINFALL INTENSITY(INCH/HR) = 3.11
AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 4.00
TOTAL STREAM AREA(ACRES) = 4.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.26

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 15 rows of data for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 10 rows of data for streams 1 through 10.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 306.67 Tc(MIN.) = 16.01
EFFECTIVE AREA(ACRES) = 168.04 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 178.7
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 169.00 = 6865.00 FEET.

FLOW PROCESS FROM NODE 169.00 TO NODE 173.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 93.50 DOWNSTREAM(FEET) = 91.80
FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 66.0 INCH PIPE IS 53.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.86
ESTIMATED PIPE DIAMETER(INCH) = 66.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 306.67
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 16.22

```

DPHOSR2
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 173.00 = 7045.00 FEET.
*****
FLOW PROCESS FROM NODE 173.00 TO NODE 173.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.22
RAINFALL INTENSITY(INCH/HR) = 2.07
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 168.04
TOTAL STREAM AREA(ACRES) = 178.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 306.67
*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 500.00
ELEVATION DATA: UPSTREAM(FEET) = 140.00 DOWNSTREAM(FEET) = 115.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.648
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.448
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL D 0.70 0.20 0.100 75 6.65
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.60 0.20 0.500 75 8.51
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.285
SUBAREA RUNOFF(CFS) = 3.97
TOTAL AREA(ACRES) = 1.30 PEAK FLOW RATE(CFS) = 3.97
*****
FLOW PROCESS FROM NODE 301.00 TO NODE 173.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 100.00 DOWNSTREAM(FEET) = 91.80
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.10
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.97
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 6.70
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 173.00 = 550.00 FEET.
*****
FLOW PROCESS FROM NODE 173.00 TO NODE 173.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.70
RAINFALL INTENSITY(INCH/HR) = 3.43
AREA-AVERAGED Fm(INCH/HR) = 0.06
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.28
EFFECTIVE STREAM AREA(ACRES) = 1.30
TOTAL STREAM AREA(ACRES) = 1.30
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.97

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** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	261.23	8.19	3.060	0.20(0.07)	0.34	93.4	170.00
1	299.16	11.64	2.501	0.20(0.07)	0.35	132.2	107.00
1	302.19	12.04	2.453	0.20(0.07)	0.35	136.6	160.00
1	303.83	12.36	2.417	0.20(0.07)	0.35	139.6	151.00
1	306.41	15.19	2.148	0.20(0.07)	0.36	161.1	101.00
1	306.67	16.22	2.069	0.20(0.07)	0.36	168.0	118.00
1	306.44	16.32	2.061	0.20(0.07)	0.36	168.6	136.00
1	303.14	16.86	2.023	0.20(0.07)	0.36	170.1	146.00
1	274.98	21.08	1.780	0.20(0.07)	0.36	176.8	112.00
1	260.07	23.52	1.672	0.20(0.07)	0.36	178.7	126.00
2	3.97	6.70	3.432	0.20(0.06)	0.28	1.3	300.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	244.42	6.70	3.432	0.20(0.07)	0.34	77.8	300.00
2	264.76	8.19	3.060	0.20(0.07)	0.34	94.7	170.00
3	302.03	11.64	2.501	0.20(0.07)	0.35	133.5	107.00
4	305.01	12.04	2.453	0.20(0.07)	0.35	137.9	160.00
5	306.61	12.36	2.417	0.20(0.07)	0.35	140.9	151.00
6	308.87	15.19	2.148	0.20(0.07)	0.36	162.4	101.00
7	309.04	16.22	2.069	0.20(0.07)	0.36	169.3	118.00
8	308.80	16.32	2.061	0.20(0.07)	0.36	169.9	136.00
9	305.45	16.86	2.023	0.20(0.07)	0.36	171.4	146.00
10	277.00	21.08	1.780	0.20(0.07)	0.36	178.1	112.00
11	261.96	23.52	1.672	0.20(0.07)	0.36	180.0	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 309.04 Tc(MIN.) = 16.22
EFFECTIVE AREA(ACRES) = 169.34 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 180.0
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 173.00 = 7045.00 FEET.

FLOW PROCESS FROM NODE 173.00 TO NODE 175.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 91.80 DOWNSTREAM(FEET) = 74.40
FLOW LENGTH(FEET) = 470.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 54.0 INCH PIPE IS 38.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 25.38
ESTIMATED PIPE DIAMETER(INCH) = 54.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 309.04
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 16.52
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 175.00 = 7515.00 FEET.

FLOW PROCESS FROM NODE 175.00 TO NODE 175.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.52
RAINFALL INTENSITY(INCH/HR) = 2.05
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 169.34
TOTAL STREAM AREA(ACRES) = 180.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 309.04

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FLOW PROCESS FROM NODE 176.00 TO NODE 177.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 125.00 DOWNSTREAM(FEET) = 120.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.994
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.102
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
CONDOMINIUMS D 0.90 0.20 0.350 75 7.99
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA RUNOFF(CFS) = 2.46
TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 2.46

FLOW PROCESS FROM NODE 177.00 TO NODE 178.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 110.00 DOWNSTREAM(FEET) = 105.00
FLOW LENGTH(FEET) = 290.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.79
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.46
PIPE TRAVEL TIME(MIN.) = 0.84 Tc(MIN.) = 8.83
LONGEST FLOWPATH FROM NODE 176.00 TO NODE 178.00 = 590.00 FEET.

FLOW PROCESS FROM NODE 178.00 TO NODE 178.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.83
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.931
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
CONDOMINIUMS D 1.50 0.20 0.350 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA AREA(ACRES) = 1.50 SUBAREA RUNOFF(CFS) = 3.86
EFFECTIVE AREA(ACRES) = 2.40 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 6.18

FLOW PROCESS FROM NODE 178.00 TO NODE 179.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 105.00 DOWNSTREAM(FEET) = 80.00
FLOW LENGTH(FEET) = 390.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.86
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.18
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 9.38
LONGEST FLOWPATH FROM NODE 176.00 TO NODE 179.00 = 980.00 FEET.

FLOW PROCESS FROM NODE 179.00 TO NODE 179.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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MAINLINE Tc(MIN.) = 9.38
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.831
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 CONDOMINIUMS D 3.00 0.20 0.350 75
 RESIDENTIAL
 "11+ DWELLINGS/ACRE" D 0.20 0.20 0.200 75
 PUBLIC PARK D 0.40 0.20 0.850 75
 COMMERCIAL D 0.90 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.338
 SUBAREA AREA(ACRES) = 4.50 SUBAREA RUNOFF(CFS) = 11.19
 EFFECTIVE AREA(ACRES) = 6.90 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.34
 TOTAL AREA(ACRES) = 6.9 PEAK FLOW RATE(CFS) = 17.16

FLOW PROCESS FROM NODE 179.00 TO NODE 175.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 80.00 DOWNSTREAM(FEET) = 74.40
 FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 15.89
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 17.16
 PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 9.46
 LONGEST FLOWPATH FROM NODE 176.00 TO NODE 175.00 = 1060.00 FEET.

FLOW PROCESS FROM NODE 175.00 TO NODE 175.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 9.46
 RAINFALL INTENSITY(INCH/HR) = 2.82
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.34
 EFFECTIVE STREAM AREA(ACRES) = 6.90
 TOTAL STREAM AREA(ACRES) = 6.90
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.16

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	244.42	7.03	3.339	0.20(0.07)	0.34	77.8	300.00
1	264.76	8.51	2.994	0.20(0.07)	0.34	94.7	170.00
1	302.03	11.96	2.463	0.20(0.07)	0.35	133.5	107.00
1	305.01	12.36	2.417	0.20(0.07)	0.35	137.9	160.00
1	306.61	12.67	2.383	0.20(0.07)	0.35	140.9	151.00
1	308.87	15.50	2.123	0.20(0.07)	0.36	162.4	101.00
1	309.04	16.52	2.046	0.20(0.07)	0.36	169.3	118.00
1	308.80	16.63	2.039	0.20(0.07)	0.36	169.9	136.00
1	305.45	17.17	2.002	0.20(0.07)	0.36	171.4	146.00
1	277.00	21.40	1.765	0.20(0.07)	0.36	178.1	112.00
1	261.96	23.85	1.658	0.20(0.07)	0.36	180.0	126.00
2	17.16	9.46	2.817	0.20(0.07)	0.34	6.9	176.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	259.59	7.03	3.339	0.20(0.07)	0.34	82.9	300.00
2	281.18	8.51	2.994	0.20(0.07)	0.34	100.9	170.00

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3	292.22	9.46	2.817	0.20(0.07)	0.34	112.3	176.00
4	316.98	11.96	2.463	0.20(0.07)	0.35	140.4	107.00
5	319.67	12.36	2.417	0.20(0.07)	0.35	144.8	160.00
6	321.05	12.67	2.383	0.20(0.07)	0.35	147.8	151.00
7	321.70	15.50	2.123	0.20(0.07)	0.36	169.3	101.00
8	321.39	16.52	2.046	0.20(0.07)	0.36	176.2	118.00
9	321.10	16.63	2.039	0.20(0.07)	0.36	176.8	136.00
10	317.52	17.17	2.002	0.20(0.07)	0.36	178.3	146.00
11	287.59	21.40	1.765	0.20(0.07)	0.36	185.0	112.00
12	271.89	23.85	1.658	0.20(0.07)	0.36	186.9	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 321.70 Tc(MIN.) = 15.50
EFFECTIVE AREA(ACRES) = 169.33 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 186.9
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 175.00 = 7515.00 FEET.

FLOW PROCESS FROM NODE 175.00 TO NODE 180.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 74.40 DOWNSTREAM(FEET) = 51.60
FLOW LENGTH(FEET) = 270.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 45.0 INCH PIPE IS 35.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.38
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 321.70
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 15.63
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 180.00 = 7785.00 FEET.

FLOW PROCESS FROM NODE 180.00 TO NODE 180.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 15.63
RAINFALL INTENSITY(INCH/HR) = 2.11
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 169.33
TOTAL STREAM AREA(ACRES) = 186.90
PEAK FLOW RATE(CFS) AT CONFLUENCE = 321.70

FLOW PROCESS FROM NODE 181.00 TO NODE 182.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 125.00 DOWNSTREAM(FEET) = 120.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.994
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.102
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
CONDOMINIUMS	D	1.10	0.20	0.350	75	7.99

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA RUNOFF(CFS) = 3.00
TOTAL AREA(ACRES) = 1.10 PEAK FLOW RATE(CFS) = 3.00

FLOW PROCESS FROM NODE 182.00 TO NODE 183.00 IS CODE = 31

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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 110.00 DOWNSTREAM(FEET) = 105.00
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.34
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.00
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 8.11
LONGEST FLOWPATH FROM NODE 181.00 TO NODE 183.00 = 370.00 FEET.

FLOW PROCESS FROM NODE 183.00 TO NODE 183.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.11
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.078
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
CONDOMINIUMS D 2.00 0.20 0.350 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA AREA(ACRES) = 2.00 SUBAREA RUNOFF(CFS) = 5.41
EFFECTIVE AREA(ACRES) = 3.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 8.39

FLOW PROCESS FROM NODE 183.00 TO NODE 184.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 105.00 DOWNSTREAM(FEET) = 60.00
FLOW LENGTH(FEET) = 415.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.57
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.39
PIPE TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 8.55
LONGEST FLOWPATH FROM NODE 181.00 TO NODE 184.00 = 785.00 FEET.

FLOW PROCESS FROM NODE 184.00 TO NODE 184.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.55
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.985
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
CONDOMINIUMS D 3.10 0.20 0.350 75
COMMERCIAL D 0.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.321
SUBAREA AREA(ACRES) = 3.50 SUBAREA RUNOFF(CFS) = 9.20
EFFECTIVE AREA(ACRES) = 6.60 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.33
TOTAL AREA(ACRES) = 6.6 PEAK FLOW RATE(CFS) = 17.33

FLOW PROCESS FROM NODE 184.00 TO NODE 180.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 60.00 DOWNSTREAM(FEET) = 51.60
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013

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DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.3 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 19.29
ESTIMATED PIPE DIAMETER (INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 17.33
PIPE TRAVEL TIME (MIN.) = 0.06 Tc (MIN.) = 8.61
LONGEST FLOWPATH FROM NODE 181.00 TO NODE 180.00 = 855.00 FEET.

FLOW PROCESS FROM NODE 180.00 TO NODE 180.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION (MIN.) = 8.61
RAINFALL INTENSITY (INCH/HR) = 2.97
AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.33
EFFECTIVE STREAM AREA (ACRES) = 6.60
TOTAL STREAM AREA (ACRES) = 6.60
PEAK FLOW RATE (CFS) AT CONFLUENCE = 17.33

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp (Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists 18 rows of data for different stream numbers and their respective flow characteristics.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp (Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists 13 rows of data for different stream numbers and their respective peak flow rates.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 334.78 Tc (MIN.) = 12.80
EFFECTIVE AREA (ACRES) = 154.45 AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA (ACRES) = 193.5
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 180.00 = 7785.00 FEET.

FLOW PROCESS FROM NODE 180.00 TO NODE 185.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

DPHOSR2

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=====
ELEVATION DATA: UPSTREAM(FEET) = 51.60 DOWNSTREAM(FEET) = 46.80
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 45.0 INCH PIPE IS 36.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.98
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 334.78
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 12.83
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 185.00 = 7840.00 FEET.

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FLOW PROCESS FROM NODE 185.00 TO NODE 185.00 IS CODE = 1
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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
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TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.83
RAINFALL INTENSITY(INCH/HR) = 2.37
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.35
EFFECTIVE STREAM AREA(ACRES) = 154.45
TOTAL STREAM AREA(ACRES) = 193.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 334.78

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*****
FLOW PROCESS FROM NODE 186.00 TO NODE 187.00 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
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INITIAL SUBAREA FLOW-LENGTH(FEET) = 260.00
ELEVATION DATA: UPSTREAM(FEET) = 120.00 DOWNSTREAM(FEET) = 115.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.195
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.590
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap      SCS      Tc
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL            D      0.60    0.20    0.100    75    6.20
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 1.93
TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.93

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*****
FLOW PROCESS FROM NODE 187.00 TO NODE 188.00 IS CODE = 62
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>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<
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UPSTREAM ELEVATION(FEET) = 115.00 DOWNSTREAM ELEVATION(FEET) = 105.00
STREET LENGTH(FEET) = 365.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

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**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.42
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.28
HALFSTREET FLOOD WIDTH(FEET) = 7.56
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.20
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.89
STREET FLOW TRAVEL TIME(MIN.) = 1.90 Tc(MIN.) = 8.10

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DPHOSR2

* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.080
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 COMMERCIAL D 1.80 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 1.80 SUBAREA RUNOFF(CFS) = 4.96
 EFFECTIVE AREA(ACRES) = 2.40 AREA-AVERAGED Fm(INCH/HR) = 0.02
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 6.61

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.09
 FLOW VELOCITY(FEET/SEC.) = 3.50 DEPTH*VELOCITY(FT*FT/SEC.) = 1.08
 LONGEST FLOWPATH FROM NODE 186.00 TO NODE 188.00 = 625.00 FEET.

FLOW PROCESS FROM NODE 188.00 TO NODE 189.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 105.00 DOWNSTREAM ELEVATION(FEET) = 70.00
 STREET LENGTH(FEET) = 360.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.35
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.30
 HALFSTREET FLOOD WIDTH(FEET) = 8.64
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.56
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.96
 STREET FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 9.01
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.896

SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 PUBLIC PARK D 0.70 0.20 0.850 75
 COMMERCIAL D 3.00 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.242
 SUBAREA AREA(ACRES) = 3.70 SUBAREA RUNOFF(CFS) = 9.48
 EFFECTIVE AREA(ACRES) = 6.10 AREA-AVERAGED Fm(INCH/HR) = 0.04
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.19
 TOTAL AREA(ACRES) = 6.1 PEAK FLOW RATE(CFS) = 15.70

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 9.99
 FLOW VELOCITY(FEET/SEC.) = 7.03 DEPTH*VELOCITY(FT*FT/SEC.) = 2.29
 LONGEST FLOWPATH FROM NODE 186.00 TO NODE 189.00 = 985.00 FEET.

FLOW PROCESS FROM NODE 189.00 TO NODE 185.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 60.00 DOWNSTREAM(FEET) = 46.80
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 8.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 22.58
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 15.70

DPHOSR2
 PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 9.06
 LONGEST FLOWPATH FROM NODE 186.00 TO NODE 185.00 = 1055.00 FEET.

 FLOW PROCESS FROM NODE 185.00 TO NODE 185.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 9.06
 RAINFALL INTENSITY(INCH/HR) = 2.89
 AREA-AVERAGED Fm(INCH/HR) = 0.04
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.19
 EFFECTIVE STREAM AREA(ACRES) = 6.10
 TOTAL STREAM AREA(ACRES) = 6.10
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.70

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	275.66	7.20	3.295	0.20(0.07)	0.34	88.4	300.00
1	298.10	8.64	2.968	0.20(0.07)	0.34	107.2	181.00
1	298.48	8.67	2.962	0.20(0.07)	0.34	107.5	170.00
1	308.49	9.62	2.790	0.20(0.07)	0.34	118.9	176.00
1	331.18	12.12	2.445	0.20(0.07)	0.35	147.0	107.00
1	333.60	12.52	2.399	0.20(0.07)	0.35	151.4	160.00
1	334.78	12.83	2.366	0.20(0.07)	0.35	154.4	151.00
1	333.90	15.65	2.111	0.20(0.07)	0.35	175.9	101.00
1	333.14	16.68	2.035	0.20(0.07)	0.36	182.8	118.00
1	332.81	16.79	2.028	0.20(0.07)	0.36	183.4	136.00
1	329.01	17.33	1.991	0.20(0.07)	0.36	184.9	146.00
1	297.68	21.56	1.757	0.20(0.07)	0.36	191.6	112.00
1	281.35	24.01	1.652	0.20(0.07)	0.36	193.5	126.00
2	15.70	9.06	2.887	0.20(0.04)	0.19	6.1	186.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	289.91	7.20	3.295	0.20(0.07)	0.33	93.3	300.00
2	313.48	8.64	2.968	0.20(0.07)	0.33	113.0	181.00
3	313.88	8.67	2.962	0.20(0.07)	0.33	113.3	170.00
4	318.35	9.06	2.887	0.20(0.07)	0.33	118.4	186.00
5	323.65	9.62	2.790	0.20(0.07)	0.34	125.0	176.00
6	344.44	12.12	2.445	0.20(0.07)	0.34	153.1	107.00
7	346.61	12.52	2.399	0.20(0.07)	0.34	157.5	160.00
8	347.61	12.83	2.366	0.20(0.07)	0.34	160.5	151.00
9	345.33	15.65	2.111	0.20(0.07)	0.35	182.0	101.00
10	344.15	16.68	2.035	0.20(0.07)	0.35	188.9	118.00
11	343.78	16.79	2.028	0.20(0.07)	0.35	189.5	136.00
12	339.78	17.33	1.991	0.20(0.07)	0.35	191.0	146.00
13	307.16	21.56	1.757	0.20(0.07)	0.35	197.7	112.00
14	290.25	24.01	1.652	0.20(0.07)	0.36	199.6	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 347.61 Tc(MIN.) = 12.83
 EFFECTIVE AREA(ACRES) = 160.55 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.34
 TOTAL AREA(ACRES) = 199.6
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 185.00 = 7840.00 FEET.

 FLOW PROCESS FROM NODE 185.00 TO NODE 191.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 46.80 DOWNSTREAM(FEET) = 5.50

DPHOSR2

FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 48.0 INCH PIPE IS 35.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.76
ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 347.61
PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 13.08
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 191.00 = 8355.00 FEET.

FLOW PROCESS FROM NODE 191.00 TO NODE 191.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.08
RAINFALL INTENSITY(INCH/HR) = 2.34
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.34
EFFECTIVE STREAM AREA(ACRES) = 160.55
TOTAL STREAM AREA(ACRES) = 199.60
PEAK FLOW RATE(CFS) AT CONFLUENCE = 347.61

FLOW PROCESS FROM NODE 192.00 TO NODE 193.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 280.00
ELEVATION DATA: UPSTREAM(FEET) = 142.00 DOWNSTREAM(FEET) = 140.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.955
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.736
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.70 0.20 0.500 75 9.95
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA RUNOFF(CFS) = 1.66
TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 1.66

FLOW PROCESS FROM NODE 193.00 TO NODE 194.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 140.00 DOWNSTREAM ELEVATION(FEET) = 138.00
STREET LENGTH(FEET) = 320.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.07
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.30
HALFSTREET FLOOD WIDTH(FEET) = 8.91
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.68
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.51
STREET FLOW TRAVEL TIME(MIN.) = 3.17 Tc(MIN.) = 13.12
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.335

DPHOSR2

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.40	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 2.82					
EFFECTIVE AREA(ACRES) = 2.10 AREA-AVERAGED Fm(INCH/HR) = 0.10					
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50					
TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 4.22					

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.26
FLOW VELOCITY(FEET/SEC.) = 1.80 DEPTH*VELOCITY(FT*FT/SEC.) = 0.60
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 194.00 = 600.00 FEET.

FLOW PROCESS FROM NODE 194.00 TO NODE 195.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 138.00 DOWNSTREAM ELEVATION(FEET) = 135.00
STREET LENGTH(FEET) = 415.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.86
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.38
HALFSTREET FLOOD WIDTH(FEET) = 12.87
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.22
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.85
STREET FLOW TRAVEL TIME(MIN.) = 3.12 Tc(MIN.) = 16.25
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.066

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	4.10	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 4.10 SUBAREA RUNOFF(CFS) = 7.26					
EFFECTIVE AREA(ACRES) = 6.20 AREA-AVERAGED Fm(INCH/HR) = 0.10					
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50					
TOTAL AREA(ACRES) = 6.2 PEAK FLOW RATE(CFS) = 10.97					

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.76
FLOW VELOCITY(FEET/SEC.) = 2.39 DEPTH*VELOCITY(FT*FT/SEC.) = 1.01
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 195.00 = 1015.00 FEET.

FLOW PROCESS FROM NODE 195.00 TO NODE 196.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 130.00 DOWNSTREAM(FEET) = 120.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.98
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 10.97

DPHOSR2
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 16.29
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 196.00 = 1065.00 FEET.

FLOW PROCESS FROM NODE 196.00 TO NODE 196.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) =	16.29				
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	2.064				
SUBAREA LOSS RATE DATA(AMC II):					
DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	3.50	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 3.50		SUBAREA RUNOFF(CFS) = 6.19			
EFFECTIVE AREA(ACRES) = 9.70		AREA-AVERAGED Fm(INCH/HR) = 0.10			
AREA-AVERAGED Fp(INCH/HR) = 0.20		AREA-AVERAGED Ap = 0.50			
TOTAL AREA(ACRES) = 9.7		PEAK FLOW RATE(CFS) = 17.14			

FLOW PROCESS FROM NODE 196.00 TO NODE 197.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	120.00	DOWNSTREAM(FEET) =	110.00
FLOW LENGTH(FEET) =	135.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.4 INCHES			
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.24			
ESTIMATED PIPE DIAMETER(INCH) = 18.00		NUMBER OF PIPES = 1	
PIPE-FLOW(CFS) = 17.14			
PIPE TRAVEL TIME(MIN.) =	0.14	Tc(MIN.) =	16.42
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 197.00 =	1200.00 FEET.		

FLOW PROCESS FROM NODE 197.00 TO NODE 197.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) =	16.42				
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	2.054				
SUBAREA LOSS RATE DATA(AMC II):					
DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	2.80	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 2.80		SUBAREA RUNOFF(CFS) = 4.92			
EFFECTIVE AREA(ACRES) = 12.50		AREA-AVERAGED Fm(INCH/HR) = 0.10			
AREA-AVERAGED Fp(INCH/HR) = 0.20		AREA-AVERAGED Ap = 0.50			
TOTAL AREA(ACRES) = 12.5		PEAK FLOW RATE(CFS) = 21.98			

FLOW PROCESS FROM NODE 197.00 TO NODE 198.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	110.00	DOWNSTREAM(FEET) =	100.00
FLOW LENGTH(FEET) =	50.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.2 INCHES			
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.82			
ESTIMATED PIPE DIAMETER(INCH) = 15.00		NUMBER OF PIPES = 1	
PIPE-FLOW(CFS) = 21.98			
PIPE TRAVEL TIME(MIN.) =	0.03	Tc(MIN.) =	16.46
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 198.00 =	1250.00 FEET.		

FLOW PROCESS FROM NODE 198.00 TO NODE 198.00 IS CODE = 81

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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
MAINLINE Tc(MIN.) = 16.46
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.051
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap        SCS
LAND USE              GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE"   D        1.70     0.20     0.500    75
PUBLIC PARK            D        1.20     0.20     0.850    75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.645
SUBAREA AREA(ACRES) = 2.90      SUBAREA RUNOFF(CFS) = 5.02
EFFECTIVE AREA(ACRES) = 15.40   AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.20  AREA-AVERAGED Ap = 0.53
TOTAL AREA(ACRES) = 15.4      PEAK FLOW RATE(CFS) = 26.97

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*****
FLOW PROCESS FROM NODE 198.00 TO NODE 199.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 100.00 DOWNSTREAM(FEET) = 73.00
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.15
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 26.97
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 16.72
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 199.00 = 1550.00 FEET.

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*****
FLOW PROCESS FROM NODE 199.00 TO NODE 199.00 IS CODE = 81
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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
MAINLINE Tc(MIN.) = 16.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.033
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap        SCS
LAND USE              GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE"   D        2.60     0.20     0.500    75
PUBLIC PARK            D        1.30     0.20     0.850    75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.617
SUBAREA AREA(ACRES) = 3.90      SUBAREA RUNOFF(CFS) = 6.70
EFFECTIVE AREA(ACRES) = 19.30   AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.20  AREA-AVERAGED Ap = 0.55
TOTAL AREA(ACRES) = 19.3      PEAK FLOW RATE(CFS) = 33.41

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*****
FLOW PROCESS FROM NODE 199.00 TO NODE 200.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 73.00 DOWNSTREAM(FEET) = 59.00
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.53
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 33.41
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 16.90
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 200.00 = 1750.00 FEET.

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*****
FLOW PROCESS FROM NODE 200.00 TO NODE 200.00 IS CODE = 81
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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
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MAINLINE Tc(MIN.) = 16.90
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.020
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"5-7 DWELLINGS/ACRE"	D	2.20	0.20	0.500	75
PUBLIC PARK	D	1.20	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.624
 SUBAREA AREA(ACRES) = 3.40 SUBAREA RUNOFF(CFS) = 5.80
 EFFECTIVE AREA(ACRES) = 22.70 AREA-AVERAGED Fm(INCH/HR) = 0.11
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.56
 TOTAL AREA(ACRES) = 22.7 PEAK FLOW RATE(CFS) = 39.00

 FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 59.00 DOWNSTREAM(FEET) = 16.00
 FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.7 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 29.32
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 39.00
 PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 17.01
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 201.00 = 1950.00 FEET.

 FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 16.00 DOWNSTREAM(FEET) = 13.00
 FLOW LENGTH(FEET) = 355.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 23.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.71
 ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 39.00
 PIPE TRAVEL TIME(MIN.) = 0.68 Tc(MIN.) = 17.69
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 202.00 = 2305.00 FEET.

 FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
 =====
 MAINLINE Tc(MIN.) = 17.69
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.968
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	D	0.60	0.20	0.850	75
COMMERCIAL	D	4.90	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.182
 SUBAREA AREA(ACRES) = 5.50 SUBAREA RUNOFF(CFS) = 9.56
 EFFECTIVE AREA(ACRES) = 28.20 AREA-AVERAGED Fm(INCH/HR) = 0.10
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
 TOTAL AREA(ACRES) = 28.2 PEAK FLOW RATE(CFS) = 47.49

 FLOW PROCESS FROM NODE 202.00 TO NODE 191.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 13.00 DOWNSTREAM(FEET) = 5.50
 FLOW LENGTH(FEET) = 95.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.1 INCHES

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PIPE-FLOW VELOCITY(FEET/SEC.) = 21.26
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 47.49
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 17.77
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 191.00 = 2400.00 FEET.

FLOW PROCESS FROM NODE 191.00 TO NODE 191.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 17.77
RAINFALL INTENSITY(INCH/HR) = 1.96
AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 28.20
TOTAL STREAM AREA(ACRES) = 28.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 47.49

FLOW PROCESS FROM NODE 203.00 TO NODE 204.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 225.00
ELEVATION DATA: UPSTREAM(FEET) = 100.00 DOWNSTREAM(FEET) = 95.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.025
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.894
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
PUBLIC PARK D 0.70 0.20 0.850 75 9.03
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA RUNOFF(CFS) = 1.72
TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 1.72

FLOW PROCESS FROM NODE 204.00 TO NODE 205.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 95.00 DOWNSTREAM(FEET) = 90.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 155.00 CHANNEL SLOPE = 0.0323
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 2.00
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.823
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK D 1.10 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.03
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.43
AVERAGE FLOW DEPTH(FEET) = 0.49 TRAVEL TIME(MIN.) = 0.40
Tc(MIN.) = 9.43
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.63
EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.17
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.85
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.30

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.55 FLOW VELOCITY(FEET/SEC.) = 7.00
LONGEST FLOWPATH FROM NODE 203.00 TO NODE 205.00 = 380.00 FEET.

DPHOSR2

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*****
FLOW PROCESS FROM NODE    205.00 TO NODE    206.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    90.00  DOWNSTREAM(FEET) =    28.00
CHANNEL LENGTH THRU SUBAREA(FEET) =   345.00  CHANNEL SLOPE =  0.1797
CHANNEL BASE(FEET) =    0.00  "Z" FACTOR =    2.000
MANNING'S FACTOR = 0.015  MAXIMUM DEPTH(FEET) =    2.00
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =  2.757
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp      Ap      SCS
  LAND USE             GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
PUBLIC PARK            D        1.50     0.20    0.850   75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.850
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    6.04
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =  14.60
AVERAGE FLOW DEPTH(FEET) =  0.45  TRAVEL TIME(MIN.) =  0.39
Tc(MIN.) =    9.82
SUBAREA AREA(ACRES) =    1.50     SUBAREA RUNOFF(CFS) =    3.49
EFFECTIVE AREA(ACRES) =    3.30   AREA-AVERAGED Fm(INCH/HR) =  0.17
AREA-AVERAGED Fp(INCH/HR) =  0.20  AREA-AVERAGED Ap =  0.85
TOTAL AREA(ACRES) =    3.3       PEAK FLOW RATE(CFS) =    7.68

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =  0.50  FLOW VELOCITY(FEET/SEC.) =  15.44
LONGEST FLOWPATH FROM NODE    203.00 TO NODE    206.00 =    725.00 FEET.
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*****
FLOW PROCESS FROM NODE    206.00 TO NODE    207.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    18.00  DOWNSTREAM(FEET) =    13.00
FLOW LENGTH(FEET) =    70.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS  8.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  12.91
ESTIMATED PIPE DIAMETER(INCH) =  12.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =    7.68
PIPE TRAVEL TIME(MIN.) =  0.09  Tc(MIN.) =    9.91
LONGEST FLOWPATH FROM NODE    203.00 TO NODE    207.00 =    795.00 FEET.
```

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*****
FLOW PROCESS FROM NODE    207.00 TO NODE    207.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
MAINLINE Tc(MIN.) =    9.91
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =  2.743
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp      Ap      SCS
  LAND USE             GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
COMMERCIAL            D        1.90     0.20    0.100   75
PUBLIC PARK            D        0.60     0.20    0.850   75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.280
SUBAREA AREA(ACRES) =    2.50     SUBAREA RUNOFF(CFS) =    6.05
EFFECTIVE AREA(ACRES) =    5.80   AREA-AVERAGED Fm(INCH/HR) =  0.12
AREA-AVERAGED Fp(INCH/HR) =  0.20  AREA-AVERAGED Ap =  0.60
TOTAL AREA(ACRES) =    5.8       PEAK FLOW RATE(CFS) =   13.69
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*****
FLOW PROCESS FROM NODE    207.00 TO NODE    191.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    13.00  DOWNSTREAM(FEET) =    5.50
FLOW LENGTH(FEET) =    85.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS  9.7 INCHES
```


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PIPE-FLOW VELOCITY(FEET/SEC.) = 16.29
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 13.69
 PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.00
 LONGEST FLOWPATH FROM NODE 203.00 TO NODE 191.00 = 880.00 FEET.

 FLOW PROCESS FROM NODE 191.00 TO NODE 191.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
 TIME OF CONCENTRATION(MIN.) = 10.00
 RAINFALL INTENSITY(INCH/HR) = 2.73
 AREA-AVERAGED Fm(INCH/HR) = 0.12
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.60
 EFFECTIVE STREAM AREA(ACRES) = 5.80
 TOTAL STREAM AREA(ACRES) = 5.80
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.69

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	289.91	7.46	3.229	0.20(0.07)	0.33	93.3	300.00
1	313.48	8.89	2.918	0.20(0.07)	0.33	113.0	181.00
1	313.88	8.92	2.913	0.20(0.07)	0.33	113.3	170.00
1	318.35	9.32	2.841	0.20(0.07)	0.33	118.4	186.00
1	323.65	9.88	2.748	0.20(0.07)	0.34	125.0	176.00
1	344.44	12.36	2.416	0.20(0.07)	0.34	153.1	107.00
1	346.61	12.76	2.373	0.20(0.07)	0.34	157.5	160.00
1	347.61	13.08	2.340	0.20(0.07)	0.34	160.5	151.00
1	345.33	15.90	2.092	0.20(0.07)	0.35	182.0	101.00
1	344.15	16.93	2.018	0.20(0.07)	0.35	188.9	118.00
1	343.78	17.03	2.011	0.20(0.07)	0.35	189.5	136.00
1	339.78	17.58	1.975	0.20(0.07)	0.35	191.0	146.00
1	307.16	21.81	1.745	0.20(0.07)	0.35	197.7	112.00
1	290.25	24.27	1.642	0.20(0.07)	0.36	199.6	126.00
2	47.49	17.77	1.963	0.20(0.10)	0.48	28.2	192.00
3	13.69	10.00	2.729	0.20(0.12)	0.60	5.8	203.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	335.51	7.46	3.229	0.20(0.07)	0.36	109.4	300.00
2	362.48	8.89	2.918	0.20(0.07)	0.36	132.3	181.00
3	362.95	8.92	2.913	0.20(0.07)	0.36	132.7	170.00
4	368.28	9.32	2.841	0.20(0.07)	0.36	138.6	186.00
5	374.78	9.88	2.748	0.20(0.07)	0.36	146.4	176.00
6	376.04	10.00	2.729	0.20(0.07)	0.36	148.1	203.00
7	397.56	12.36	2.416	0.20(0.07)	0.36	178.6	107.00
8	400.03	12.76	2.373	0.20(0.07)	0.36	183.5	160.00
9	401.26	13.08	2.340	0.20(0.07)	0.36	187.1	151.00
10	401.11	15.90	2.092	0.20(0.07)	0.37	213.1	101.00
11	400.69	16.93	2.018	0.20(0.07)	0.37	221.6	118.00
12	400.40	17.03	2.011	0.20(0.07)	0.37	222.3	136.00
13	396.80	17.58	1.975	0.20(0.07)	0.37	224.7	146.00
14	395.48	17.77	1.963	0.20(0.07)	0.37	225.3	192.00
15	357.63	21.81	1.745	0.20(0.08)	0.38	231.7	112.00
16	337.54	24.27	1.642	0.20(0.08)	0.38	233.6	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 401.26 Tc(MIN.) = 13.08
 EFFECTIVE AREA(ACRES) = 187.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
 TOTAL AREA(ACRES) = 233.6
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 191.00 = 8355.00 FEET.

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 FLOW PROCESS FROM NODE 191.00 TO NODE 207.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 5.50 DOWNSTREAM(FEET) = 3.30
 FLOW LENGTH(FEET) = 485.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 84.0 INCH PIPE IS 67.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 12.09
 ESTIMATED PIPE DIAMETER(INCH) = 84.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 401.26
 PIPE TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 13.75
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 207.00 = 8840.00 FEET.

 FLOW PROCESS FROM NODE 207.00 TO NODE 208.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 3.30 DOWNSTREAM(FEET) = 2.30
 FLOW LENGTH(FEET) = 95.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 72.0 INCH PIPE IS 57.4 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 16.61
 ESTIMATED PIPE DIAMETER(INCH) = 72.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 401.26
 PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 13.84
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 208.00 = 8935.00 FEET.

 FLOW PROCESS FROM NODE 208.00 TO NODE 213.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 2.30 DOWNSTREAM(FEET) = 0.10
 FLOW LENGTH(FEET) = 250.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 75.0 INCH PIPE IS 58.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 15.59
 ESTIMATED PIPE DIAMETER(INCH) = 75.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 401.26
 PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 14.11
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 213.00 = 9185.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 233.6 TC(MIN.) = 14.11
 EFFECTIVE AREA(ACRES) = 187.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.365
 PEAK FLOW RATE(CFS) = 401.26

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	335.51	8.53	2.990	0.20(0.07)	0.36	109.4	300.00
2	362.48	9.95	2.736	0.20(0.07)	0.36	132.3	181.00
3	362.95	9.98	2.732	0.20(0.07)	0.36	132.7	170.00
4	368.28	10.37	2.672	0.20(0.07)	0.36	138.6	186.00
5	374.78	10.92	2.595	0.20(0.07)	0.36	146.4	176.00
6	376.04	11.04	2.578	0.20(0.07)	0.36	148.1	203.00
7	397.56	13.40	2.308	0.20(0.07)	0.36	178.6	107.00
8	400.03	13.80	2.269	0.20(0.07)	0.36	183.5	160.00
9	401.26	14.11	2.240	0.20(0.07)	0.36	187.1	151.00
10	401.11	16.93	2.018	0.20(0.07)	0.37	213.1	101.00
11	400.69	17.96	1.951	0.20(0.07)	0.37	221.6	118.00
12	400.40	18.06	1.945	0.20(0.07)	0.37	222.3	136.00
13	396.80	18.61	1.912	0.20(0.07)	0.37	224.7	146.00
14	395.48	18.80	1.901	0.20(0.07)	0.37	225.3	192.00
15	357.63	22.87	1.699	0.20(0.08)	0.38	231.7	112.00
16	337.54	25.33	1.602	0.20(0.08)	0.38	233.6	126.00

=====

END OF RATIONAL METHOD ANALYSIS

B.2

Existing Condition
 60" Conduit (Loop 1)
 10-year Hydrology
 w/ 3.8 Ac Harbor
 + 0.7 Ac Harbor
 Tributary Included

DPHOSR

 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
 (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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Analysis prepared by:

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 Suite 100
 Irvine, CA 92606

FILE NAME: DPHOSR.DAT
 TIME/DATE OF STUDY: 10:35 04/29/2013

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 10.00
 SPECIFIED MINIMUM PIPE SIZE (INCH) = 12.00
 SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
 DATA BANK RAINFALL USED
 ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0312 0.167	0.0150
2	18.0	5.0	0.020/0.020/0.020	0.50	1.50 0.0312 0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
 1. Relative Flow-Depth = 0.67 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)
 *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
 *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

 FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 280.00
 ELEVATION DATA: UPSTREAM (FEET) = 295.00 DOWNSTREAM (FEET) = 290.00

Tc = K * [(LENGTH** 3.00) / (ELEVATION CHANGE)] ** 0.20
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 8.288
 * 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.039
 SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.30	0.20	0.500	75	8.29

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
 SUBAREA RUNOFF (CFS) = 3.44
 TOTAL AREA (ACRES) = 1.30 PEAK FLOW RATE (CFS) = 3.44

 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION (FEET) = 290.00 DOWNSTREAM ELEVATION (FEET) = 285.00

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STREET LENGTH(FEET) = 135.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.64
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.35
 HALFSTREET FLOOD WIDTH(FEET) = 11.43
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.66
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.65
 STREET FLOW TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 8.77
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.942

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	2.50	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 2.50		SUBAREA RUNOFF(CFS) = 6.39			
EFFECTIVE AREA(ACRES) = 3.80		AREA-AVERAGED Fm(INCH/HR) = 0.10			
AREA-AVERAGED Fp(INCH/HR) = 0.20		AREA-AVERAGED Ap = 0.50			
TOTAL AREA(ACRES) = 3.8		PEAK FLOW RATE(CFS) = 9.72			

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.35
 FLOW VELOCITY(FEET/SEC.) = 5.11 DEPTH*VELOCITY(FT*FT/SEC.) = 2.01
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 103.00 = 415.00 FEET.

 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 285.00 DOWNSTREAM ELEVATION(FEET) = 253.00
 STREET LENGTH(FEET) = 345.00 CURB HEIGHT(INCHES) = 8.0
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 14.11
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.40
 HALFSTREET FLOOD WIDTH(FEET) = 13.48
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.77
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.13
 STREET FLOW TRAVEL TIME(MIN.) = 0.74 Tc(MIN.) = 9.51
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.808

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	3.60	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 3.60		SUBAREA RUNOFF(CFS) = 8.78			
EFFECTIVE AREA(ACRES) = 7.40		AREA-AVERAGED Fm(INCH/HR) = 0.10			

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AREA-AVERAGED F_p (INCH/HR) = 0.20 AREA-AVERAGED A_p = 0.50
TOTAL AREA(ACRES) = 7.4 PEAK FLOW RATE(CFS) = 18.04

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 14.96
FLOW VELOCITY(FEET/SEC.) = 8.23 DEPTH*VELOCITY(FT*FT/SEC.) = 3.54
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 104.00 = 760.00 FEET.

FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 253.00 DOWNSTREAM ELEVATION(FEET) = 225.00
STREET LENGTH(FEET) = 630.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 20.18
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.49
HALFSTREET FLOOD WIDTH(FEET) = 18.24
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.38
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.11
STREET FLOW TRAVEL TIME(MIN.) = 1.65 T_c (MIN.) = 11.16
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.563

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
RESIDENTIAL					
"5-7 DWELLINGS/ACRE"	D	0.70	0.20	0.500	75
PUBLIC PARK	D	0.10	0.20	0.850	75
COMMERCIAL	D	1.10	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.287
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 4.28
EFFECTIVE AREA(ACRES) = 9.30 AREA-AVERAGED F_m (INCH/HR) = 0.09
AREA-AVERAGED F_p (INCH/HR) = 0.20 AREA-AVERAGED A_p = 0.46
TOTAL AREA(ACRES) = 9.3 PEAK FLOW RATE(CFS) = 20.69

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.40
FLOW VELOCITY(FEET/SEC.) = 6.43 DEPTH*VELOCITY(FT*FT/SEC.) = 3.16
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 105.00 = 1390.00 FEET.

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 204.30 DOWNSTREAM(FEET) = 202.30
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.43
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 20.69
PIPE TRAVEL TIME(MIN.) = 0.02 T_c (MIN.) = 11.18
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 106.00 = 1415.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.18
RAINFALL INTENSITY(INCH/HR) = 2.56
AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.46
EFFECTIVE STREAM AREA(ACRES) = 9.30
TOTAL STREAM AREA(ACRES) = 9.30
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.69

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FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 270.00
ELEVATION DATA: UPSTREAM(FEET) = 330.00 DOWNSTREAM(FEET) = 320.00

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Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.880
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.699
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 1.00 0.20 0.200 75 5.88
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 3.29
TOTAL AREA(ACRES) = 1.00 PEAK FLOW RATE(CFS) = 3.29

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FLOW PROCESS FROM NODE 108.00 TO NODE 109.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 310.00 DOWNSTREAM(FEET) = 265.00
FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.15
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.29
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 6.14
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 109.00 = 505.00 FEET.

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*****
FLOW PROCESS FROM NODE 109.00 TO NODE 109.00 IS CODE = 81
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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
MAINLINE Tc(MIN.) = 6.14
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.609
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 3.90 0.20 0.200 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA(ACRES) = 3.90 SUBAREA RUNOFF(CFS) = 12.53
EFFECTIVE AREA(ACRES) = 4.90 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 4.9 PEAK FLOW RATE(CFS) = 15.74

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*****
FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

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DPHOSR

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 265.00 DOWNSTREAM(FEET) = 258.00
FLOW LENGTH(FEET) = 560.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.94
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.74
PIPE TRAVEL TIME(MIN.) = 1.18 Tc(MIN.) = 7.31
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 110.00 = 1065.00 FEET.

FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.31
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.265
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.30 0.20 0.500 75
PUBLIC PARK D 2.10 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.716
SUBAREA AREA(ACRES) = 3.40 SUBAREA RUNOFF(CFS) = 9.55
EFFECTIVE AREA(ACRES) = 8.30 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 8.3 PEAK FLOW RATE(CFS) = 23.77

FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 258.00 DOWNSTREAM(FEET) = 238.00
FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.66
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.77
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 7.45
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 111.00 = 1240.00 FEET.

FLOW PROCESS FROM NODE 111.00 TO NODE 111.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.229
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 5.50 0.20 0.500 75
PUBLIC PARK D 0.80 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.544
SUBAREA AREA(ACRES) = 6.30 SUBAREA RUNOFF(CFS) = 17.69
EFFECTIVE AREA(ACRES) = 14.60 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 14.6 PEAK FLOW RATE(CFS) = 41.20

FLOW PROCESS FROM NODE 111.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 238.00 DOWNSTREAM(FEET) = 202.30

DPHOSR

FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.0 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 26.38
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 41.20
 PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 7.60
 LONGEST FLOWPATH FROM NODE 107.00 TO NODE 106.00 = 1475.00 FEET.

 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

 TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 7.60
 RAINFALL INTENSITY(INCH/HR) = 3.19
 AREA-AVERAGED Fm(INCH/HR) = 0.09
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.47
 EFFECTIVE STREAM AREA(ACRES) = 14.60
 TOTAL STREAM AREA(ACRES) = 14.60
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 41.20

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	20.69	11.18	2.560	0.20(0.09)	0.46	9.3	101.00
2	41.20	7.60	3.193	0.20(0.09)	0.47	14.6	107.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	58.87	7.60	3.193	0.20(0.09)	0.47	20.9	107.00
2	53.47	11.18	2.560	0.20(0.09)	0.46	23.9	101.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 58.87 Tc(MIN.) = 7.60
 EFFECTIVE AREA(ACRES) = 20.92 AREA-AVERAGED Fm(INCH/HR) = 0.09
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
 TOTAL AREA(ACRES) = 23.9
 LONGEST FLOWPATH FROM NODE 107.00 TO NODE 106.00 = 1475.00 FEET.

 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

 FLOW PROCESS FROM NODE 112.00 TO NODE 113.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

 INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
 ELEVATION DATA: UPSTREAM(FEET) = 330.00 DOWNSTREAM(FEET) = 328.70

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.309
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.543
 SUBAREA Tc AND LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
 RESIDENTIAL
 "5-7 DWELLINGS/ACRE" D 1.10 0.20 0.500 75 11.31
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
 SUBAREA RUNOFF(CFS) = 2.42

DPHOSR
TOTAL AREA(ACRES) = 1.10 PEAK FLOW RATE(CFS) = 2.42

FLOW PROCESS FROM NODE 113.00 TO NODE 114.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

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UPSTREAM ELEVATION(FEET)	=	328.70	DOWNSTREAM ELEVATION(FEET)	=	327.40
STREET LENGTH(FEET)	=	225.00	CURB HEIGHT(INCHES)	=	6.0
STREET HALFWIDTH(FEET)	=	18.00			

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET)	=	5.00
INSIDE STREET CROSSFALL(DECIMAL)	=	0.020
OUTSIDE STREET CROSSFALL(DECIMAL)	=	0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF	=	2
STREET PARKWAY CROSSFALL(DECIMAL)	=	0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs)	=	0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section	=	0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS)	=	4.00			
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:					
STREET FLOW DEPTH(FEET)	=	0.33			
HALFSTREET FLOOD WIDTH(FEET)	=	10.17			
AVERAGE FLOW VELOCITY(FEET/SEC.)	=	1.74			
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.)	=	0.57			
STREET FLOW TRAVEL TIME(MIN.)	=	2.16	Tc(MIN.)	=	13.47
* 10 YEAR RAINFALL INTENSITY(INCH/HR)	=	2.301			

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.60	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 1.60 SUBAREA RUNOFF(CFS) = 3.17					
EFFECTIVE AREA(ACRES) = 2.70 AREA-AVERAGED Fm(INCH/HR) = 0.10					
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50					
TOTAL AREA(ACRES) = 2.7 PEAK FLOW RATE(CFS) = 5.35					

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET)	=	0.36	HALFSTREET FLOOD WIDTH(FEET)	=	11.52
FLOW VELOCITY(FEET/SEC.)	=	1.85	DEPTH*VELOCITY(FT*FT/SEC.)	=	0.66
LONGEST FLOWPATH FROM NODE	112.00 TO NODE	114.00	=	525.00 FEET.	

FLOW PROCESS FROM NODE 114.00 TO NODE 115.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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ELEVATION DATA: UPSTREAM(FEET)	=	312.40	DOWNSTREAM(FEET)	=	310.80
FLOW LENGTH(FEET)	=	180.00	MANNING'S N	=	0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS	11.4 INCHES				
PIPE-FLOW VELOCITY(FEET/SEC.)	=	5.34			
ESTIMATED PIPE DIAMETER(INCH)	=	15.00	NUMBER OF PIPES	=	1
PIPE-FLOW(CFS)	=	5.35			
PIPE TRAVEL TIME(MIN.)	=	0.56	Tc(MIN.)	=	14.03
LONGEST FLOWPATH FROM NODE	112.00 TO NODE	115.00	=	705.00 FEET.	

FLOW PROCESS FROM NODE 115.00 TO NODE 115.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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MAINLINE Tc(MIN.)	=	14.03			
* 10 YEAR RAINFALL INTENSITY(INCH/HR)	=	2.248			
SUBAREA LOSS RATE DATA(AMC II):					
DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.30	0.20	0.500	75

DPHOSR

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 2.51
EFFECTIVE AREA(ACRES) = 4.00 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50
TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 7.73

FLOW PROCESS FROM NODE 115.00 TO NODE 116.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
ELEVATION DATA: UPSTREAM(FEET) = 310.80 DOWNSTREAM(FEET) = 247.20
FLOW LENGTH(FEET) = 825.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.35
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.73
PIPE TRAVEL TIME(MIN.) = 1.03 Tc(MIN.) = 15.06
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 116.00 = 1530.00 FEET.

FLOW PROCESS FROM NODE 116.00 TO NODE 116.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
MAINLINE Tc(MIN.) = 15.06
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.158
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 4.60 0.20 0.500 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.461
SUBAREA AREA(ACRES) = 5.10 SUBAREA RUNOFF(CFS) = 9.48
EFFECTIVE AREA(ACRES) = 9.10 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 9.1 PEAK FLOW RATE(CFS) = 16.89

FLOW PROCESS FROM NODE 116.00 TO NODE 117.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
ELEVATION DATA: UPSTREAM(FEET) = 247.20 DOWNSTREAM(FEET) = 234.20
FLOW LENGTH(FEET) = 765.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.16
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 16.89
PIPE TRAVEL TIME(MIN.) = 1.39 Tc(MIN.) = 16.45
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 117.00 = 2295.00 FEET.

FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
MAINLINE Tc(MIN.) = 16.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.052
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.00 0.20 0.500 75
COMMERCIAL D 0.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.386
SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 2.49

DPHOSR

EFFECTIVE AREA(ACRES) = 10.50 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 10.5 PEAK FLOW RATE(CFS) = 18.51

FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 16.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.052
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 3.10 0.20 0.500 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 3.10 SUBAREA RUNOFF(CFS) = 5.44
EFFECTIVE AREA(ACRES) = 13.60 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 13.6 PEAK FLOW RATE(CFS) = 23.95

FLOW PROCESS FROM NODE 117.00 TO NODE 125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 234.20 DOWNSTREAM(FEET) = 228.00
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.99
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.95
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 16.56
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 125.00 = 2395.00 FEET.

FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.56
RAINFALL INTENSITY(INCH/HR) = 2.04
AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.47
EFFECTIVE STREAM AREA(ACRES) = 13.60
TOTAL STREAM AREA(ACRES) = 13.60
PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.95

FLOW PROCESS FROM NODE 118.00 TO NODE 119.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 275.00
ELEVATION DATA: UPSTREAM(FEET) = 336.00 DOWNSTREAM(FEET) = 328.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.463
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.227
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.70 0.20 0.500 75 7.46
PUBLIC PARK D 0.20 0.20 0.850 75 9.27
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

DPHOSR

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.537
SUBAREA RUNOFF(CFS) = 5.33
TOTAL AREA(ACRES) = 1.90 PEAK FLOW RATE(CFS) = 5.33

FLOW PROCESS FROM NODE 119.00 TO NODE 120.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 328.00 DOWNSTREAM ELEVATION(FEET) = 307.00
STREET LENGTH(FEET) = 675.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.07
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.33
HALFSTREET FLOOD WIDTH(FEET) = 10.08
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.00
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.31
STREET FLOW TRAVEL TIME(MIN.) = 2.81 Tc(MIN.) = 10.28
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.686

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	3.20	0.20	0.500	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 3.20 SUBAREA RUNOFF(CFS) = 7.45
EFFECTIVE AREA(ACRES) = 5.10 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51
TOTAL AREA(ACRES) = 5.1 PEAK FLOW RATE(CFS) = 11.86

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.34
FLOW VELOCITY(FEET/SEC.) = 4.22 DEPTH*VELOCITY(FT*FT/SEC.) = 1.49
LONGEST FLOWPATH FROM NODE 118.00 TO NODE 120.00 = 950.00 FEET.

FLOW PROCESS FROM NODE 120.00 TO NODE 121.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 307.00 DOWNSTREAM ELEVATION(FEET) = 301.00
STREET LENGTH(FEET) = 115.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.99
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 12.06
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.72
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.10

DPHOSR

STREET FLOW TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 10.61
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.638

SUBAREA LOSS RATE DATA(AMC II):

Table with 7 columns: DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN. Rows include Residential (5-7 dwellings/acre), Public Park, and Commercial.

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.59
FLOW VELOCITY(FEET/SEC.) = 6.09 DEPTH*VELOCITY(FT*FT/SEC.) = 2.42
LONGEST FLOWPATH FROM NODE 118.00 TO NODE 121.00 = 1065.00 FEET.

FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 296.00 DOWNSTREAM(FEET) = 280.00
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.89
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.91
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 10.80
LONGEST FLOWPATH FROM NODE 118.00 TO NODE 122.00 = 1265.00 FEET.

FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 280.00 DOWNSTREAM ELEVATION(FEET) = 262.00
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 34.22

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.53
HALFSTREET FLOOD WIDTH(FEET) = 20.82
AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.42
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 4.50
STREET FLOW TRAVEL TIME(MIN.) = 0.53 Tc(MIN.) = 11.33
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.540

SUBAREA LOSS RATE DATA(AMC II):

Table with 7 columns: DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN. Rows include Residential (5-7 dwellings/acre), Public Park, and Commercial.

DPHOSR

EFFECTIVE AREA(ACRES) = 19.90 AREA-AVERAGED Fm(INCH/HR) = 0.10
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.52
 TOTAL AREA(ACRES) = 19.9 PEAK FLOW RATE(CFS) = 43.61

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.57 HALFSTREET FLOOD WIDTH(FEET) = 22.85
 FLOW VELOCITY(FEET/SEC.) = 8.98 DEPTH*VELOCITY(FT*FT/SEC.) = 5.12
 LONGEST FLOWPATH FROM NODE 118.00 TO NODE 123.00 = 1535.00 FEET.

 FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 262.00 DOWNSTREAM ELEVATION(FEET) = 239.00
 STREET LENGTH(FEET) = 250.00 CURB HEIGHT(INCHES) = 8.0
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 44.16
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.55
 HALFSTREET FLOOD WIDTH(FEET) = 21.60
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 10.13
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 5.55
 STREET FLOW TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 11.74
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.489

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	D	0.20	0.20	0.850	75
COMMERCIAL	D	0.30	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
 SUBAREA AREA(ACRES) = 0.50 SUBAREA RUNOFF(CFS) = 1.08
 EFFECTIVE AREA(ACRES) = 20.40 AREA-AVERAGED Fm(INCH/HR) = 0.10
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.52
 TOTAL AREA(ACRES) = 20.4 PEAK FLOW RATE(CFS) = 43.78

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.55 HALFSTREET FLOOD WIDTH(FEET) = 21.52
 FLOW VELOCITY(FEET/SEC.) = 10.11 DEPTH*VELOCITY(FT*FT/SEC.) = 5.53
 LONGEST FLOWPATH FROM NODE 118.00 TO NODE 124.00 = 1785.00 FEET.

 FLOW PROCESS FROM NODE 124.00 TO NODE 125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 232.60 DOWNSTREAM(FEET) = 228.00
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.44
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 43.78
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 11.80
 LONGEST FLOWPATH FROM NODE 118.00 TO NODE 125.00 = 1855.00 FEET.

 FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

DPHOSR

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 11.80
RAINFALL INTENSITY(INCH/HR) = 2.48
AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.52
EFFECTIVE STREAM AREA(ACRES) = 20.40
TOTAL STREAM AREA(ACRES) = 20.40
PEAK FLOW RATE(CFS) AT CONFLUENCE = 43.78

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	23.95	16.56	2.044	0.20(0.09)	0.47	13.6	112.00
2	43.78	11.80	2.481	0.20(0.10)	0.52	20.4	118.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	64.69	11.80	2.481	0.20(0.10)	0.51	30.1	118.00
2	59.68	16.56	2.044	0.20(0.10)	0.50	34.0	112.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 64.69 Tc(MIN.) = 11.80
EFFECTIVE AREA(ACRES) = 30.10 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51
TOTAL AREA(ACRES) = 34.0
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 125.00 = 2395.00 FEET.

FLOW PROCESS FROM NODE 125.00 TO NODE 132.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 228.00 DOWNSTREAM(FEET) = 224.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.10
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 64.69
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 11.84
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 132.00 = 2445.00 FEET.

FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.84
RAINFALL INTENSITY(INCH/HR) = 2.48
AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.51
EFFECTIVE STREAM AREA(ACRES) = 30.10
TOTAL STREAM AREA(ACRES) = 34.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 64.69

FLOW PROCESS FROM NODE 126.00 TO NODE 127.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 322.00 DOWNSTREAM(FEET) = 320.50

DPHOSR

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.589
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.977

SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 0.40 0.20 0.200 75 9.15
COMMERCIAL D 0.20 0.20 0.100 75 8.59
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.167
SUBAREA RUNOFF(CFS) = 1.59
TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.59

FLOW PROCESS FROM NODE 127.00 TO NODE 128.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 320.50 DOWNSTREAM ELEVATION(FEET) = 318.00
STREET LENGTH(FEET) = 600.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.65
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.77
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.60
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.63
STREET FLOW TRAVEL TIME(MIN.) = 6.23 Tc(MIN.) = 14.82
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.178

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.40 0.20 0.500 75
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 0.20 0.20 0.200 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.264
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.10
EFFECTIVE AREA(ACRES) = 1.70 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.23
TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 3.26

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.02
FLOW VELOCITY(FEET/SEC.) = 1.67 DEPTH*VELOCITY(FT*FT/SEC.) = 0.69
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 128.00 = 900.00 FEET.

FLOW PROCESS FROM NODE 128.00 TO NODE 129.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 318.00 DOWNSTREAM ELEVATION(FEET) = 302.00
STREET LENGTH(FEET) = 640.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

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INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.75
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.42
HALFSTREET FLOOD WIDTH(FEET) = 14.57
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.19
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.77
STREET FLOW TRAVEL TIME(MIN.) = 2.55 Tc(MIN.) = 17.37
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.989

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 5.50 0.20 0.500 75
COMMERCIAL D 0.90 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.444
SUBAREA AREA(ACRES) = 6.40 SUBAREA RUNOFF(CFS) = 10.94
EFFECTIVE AREA(ACRES) = 8.10 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 8.1 PEAK FLOW RATE(CFS) = 13.92

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 17.62
FLOW VELOCITY(FEET/SEC.) = 4.69 DEPTH*VELOCITY(FT*FT/SEC.) = 2.24
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 129.00 = 1540.00 FEET.

FLOW PROCESS FROM NODE 129.00 TO NODE 130.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 302.00 DOWNSTREAM ELEVATION(FEET) = 264.00
STREET LENGTH(FEET) = 450.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 19.54
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.45
HALFSTREET FLOOD WIDTH(FEET) = 15.82
AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.05
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.58
STREET FLOW TRAVEL TIME(MIN.) = 0.93 Tc(MIN.) = 18.30
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.930

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 6.10 0.20 0.500 75
COMMERCIAL D 0.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.459
SUBAREA AREA(ACRES) = 6.80 SUBAREA RUNOFF(CFS) = 11.25
EFFECTIVE AREA(ACRES) = 14.90 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.43
TOTAL AREA(ACRES) = 14.9 PEAK FLOW RATE(CFS) = 24.74

DPHOSR

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 17.38
FLOW VELOCITY(FEET/SEC.) = 8.55 DEPTH*VELOCITY(FT*FT/SEC.) = 4.05
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 130.00 = 1990.00 FEET.

FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 264.00 DOWNSTREAM ELEVATION(FEET) = 242.00
STREET LENGTH(FEET) = 310.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 25.08
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.49
HALFSTREET FLOOD WIDTH(FEET) = 18.09
AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.05
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.91
STREET FLOW TRAVEL TIME(MIN.) = 0.64 Tc(MIN.) = 18.95
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.892

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 0.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.67
EFFECTIVE AREA(ACRES) = 15.30 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 15.3 PEAK FLOW RATE(CFS) = 24.91

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.09
FLOW VELOCITY(FEET/SEC.) = 8.00 DEPTH*VELOCITY(FT*FT/SEC.) = 3.88
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 131.00 = 2300.00 FEET.

FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 237.10 DOWNSTREAM(FEET) = 224.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 28.36
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 24.91
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 18.97
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 132.00 = 2350.00 FEET.

FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 18.97

DPHOSR

RAINFALL INTENSITY(INCH/HR) = 1.89
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.42
EFFECTIVE STREAM AREA(ACRES) = 15.30
TOTAL STREAM AREA(ACRES) = 15.30
PEAK FLOW RATE(CFS) AT CONFLUENCE = 24.91

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Rows 1, 1, 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Rows 1, 2, 3.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 85.27 Tc(MIN.) = 11.84
EFFECTIVE AREA(ACRES) = 39.64 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 49.3
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 132.00 = 2445.00 FEET.

FLOW PROCESS FROM NODE 132.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 224.00 DOWNSTREAM(FEET) = 202.30
FLOW LENGTH(FEET) = 445.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 30.0 INCH PIPE IS 24.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.96
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 85.27
PIPE TRAVEL TIME(MIN.) = 0.37 Tc(MIN.) = 12.21
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 106.00 = 2890.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

** MAIN STREAM CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Rows 1, 2, 3.

** MEMORY BANK # 1 CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Rows 1, 2.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Rows 1, 2.

DPHOSR

3	136.01	12.21	2.434	0.20(0.10)	0.48	63.5	118.00
4	124.96	16.97	2.016	0.20(0.09)	0.47	71.3	112.00
5	118.45	19.35	1.870	0.20(0.09)	0.47	73.2	126.00
TOTAL AREA(ACRES) =		73.2					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 136.01 Tc(MIN.) = 12.212
EFFECTIVE AREA(ACRES) = 63.54 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 73.2
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 106.00 = 2890.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 135.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 202.30 DOWNSTREAM(FEET) = 141.50
FLOW LENGTH(FEET) = 1090.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.96
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 136.01
PIPE TRAVEL TIME(MIN.) = 0.76 Tc(MIN.) = 12.97
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 135.00 = 3980.00 FEET.

FLOW PROCESS FROM NODE 135.00 TO NODE 135.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 12.97
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.351
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	D	5.70	0.20	0.400	75
COMMERCIAL	D	0.60	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.371
SUBAREA AREA(ACRES) = 6.30 SUBAREA RUNOFF(CFS) = 12.91
EFFECTIVE AREA(ACRES) = 69.84 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 79.5 PEAK FLOW RATE(CFS) = 141.91

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	136.87	8.37	3.023	0.20(0.09)	0.46	51.9	107.00
2	141.96	11.94	2.465	0.20(0.09)	0.47	66.5	101.00
3	141.91	12.97	2.351	0.20(0.09)	0.47	69.8	118.00
4	130.72	17.73	1.965	0.20(0.09)	0.47	77.6	112.00
5	124.06	20.15	1.827	0.20(0.09)	0.46	79.5	126.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE(CFS) = 141.96 Tc(MIN.) = 11.94
AREA-AVERAGED Fm(INCH/HR) = 0.09 AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.47 EFFECTIVE AREA(ACRES) = 66.50

FLOW PROCESS FROM NODE 135.00 TO NODE 144.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 141.50 DOWNSTREAM(FEET) = 141.00
FLOW LENGTH(FEET) = 15.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 31.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.65
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 141.96
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 11.95

DPHOSR
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 144.00 = 3995.00 FEET.

FLOW PROCESS FROM NODE 144.00 TO NODE 144.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	11.95
RAINFALL INTENSITY(INCH/HR) =	2.46
AREA-AVERAGED Fm(INCH/HR) =	0.09
AREA-AVERAGED Fp(INCH/HR) =	0.20
AREA-AVERAGED Ap =	0.47
EFFECTIVE STREAM AREA(ACRES) =	66.50
TOTAL STREAM AREA(ACRES) =	79.50
PEAK FLOW RATE(CFS) AT CONFLUENCE =	141.96

FLOW PROCESS FROM NODE 136.00 TO NODE 137.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) =	230.00
ELEVATION DATA: UPSTREAM(FEET) =	335.00
DOWNSTREAM(FEET) =	332.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20						
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =	6.794					
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	3.405					
SUBAREA Tc AND LOSS RATE DATA(AMC II):						
DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS	Tc
LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN	(MIN.)
RESIDENTIAL						
"11+ DWELLINGS/ACRE"	D	3.20	0.20	0.200	75	6.79
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =	0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =	0.200					
SUBAREA RUNOFF(CFS) =	9.69					
TOTAL AREA(ACRES) =	3.20	PEAK FLOW RATE(CFS) =	9.69			

FLOW PROCESS FROM NODE 137.00 TO NODE 138.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	332.00
DOWNSTREAM ELEVATION(FEET) =	308.00
STREET LENGHT(FEET) =	575.00
CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =	5.00
INSIDE STREET CROSSFALL(DECIMAL) =	0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =	0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =	1
STREET PARKWAY CROSSFALL(DECIMAL) =	0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =	0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =	0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	13.16
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:	
STREET FLOW DEPTH(FEET) =	0.42
HALFSTREET FLOOD WIDTH(FEET) =	14.76
AVERAGE FLOW VELOCITY(FEET/SEC.) =	5.73
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =	2.42
STREET FLOW TRAVEL TIME(MIN.) =	1.67
Tc(MIN.) =	8.47
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	3.002

SUBAREA LOSS RATE DATA(AMC II):					
DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS
LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
RESIDENTIAL					
"11+ DWELLINGS/ACRE"	D	2.60	0.20	0.200	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =	0.20				

DPHOSR
SUBAREA AVERAGE PERVIOUS AREA FRACTION, $A_p = 0.200$
SUBAREA AREA(ACRES) = 2.60 SUBAREA RUNOFF(CFS) = 6.93
EFFECTIVE AREA(ACRES) = 5.80 AREA-AVERAGED F_m (INCH/HR) = 0.04
AREA-AVERAGED F_p (INCH/HR) = 0.20 AREA-AVERAGED $A_p = 0.20$
TOTAL AREA(ACRES) = 5.8 PEAK FLOW RATE(CFS) = 15.46

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 15.70
FLOW VELOCITY(FEET/SEC.) = 5.99 DEPTH*VELOCITY(FT*FT/SEC.) = 2.64
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 138.00 = 805.00 FEET.

FLOW PROCESS FROM NODE 138.00 TO NODE 139.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 308.00 DOWNSTREAM ELEVATION(FEET) = 280.00
STREET LENGTH(FEET) = 440.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 22.35
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.48
HALFSTREET FLOOD WIDTH(FEET) = 17.70
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.47
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.58
STREET FLOW TRAVEL TIME(MIN.) = 0.98 T_c (MIN.) = 9.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.819

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
RESIDENTIAL					
"11+ DWELLINGS/ACRE"	D	4.80	0.20	0.200	75
COMMERCIAL	D	0.70	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, $A_p = 0.187$
SUBAREA AREA(ACRES) = 5.50 SUBAREA RUNOFF(CFS) = 13.77
EFFECTIVE AREA(ACRES) = 11.30 AREA-AVERAGED F_m (INCH/HR) = 0.04
AREA-AVERAGED F_p (INCH/HR) = 0.20 AREA-AVERAGED $A_p = 0.19$
TOTAL AREA(ACRES) = 11.3 PEAK FLOW RATE(CFS) = 28.28

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.51 HALFSTREET FLOOD WIDTH(FEET) = 19.41
FLOW VELOCITY(FEET/SEC.) = 7.94 DEPTH*VELOCITY(FT*FT/SEC.) = 4.05
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 139.00 = 1245.00 FEET.

FLOW PROCESS FROM NODE 139.00 TO NODE 140.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 280.00 DOWNSTREAM ELEVATION(FEET) = 255.00
STREET LENGTH(FEET) = 425.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

DPHOSR

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 29.69
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.52
HALFSTREET FLOOD WIDTH(FEET) = 20.12
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.80
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 4.07
STREET FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 10.36
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.675

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.50 0.20 0.500 75
COMMERCIAL D 0.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.267
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 2.83
EFFECTIVE AREA(ACRES) = 12.50 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 12.5 PEAK FLOW RATE(CFS) = 29.64

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.52 HALFSTREET FLOOD WIDTH(FEET) = 20.12
FLOW VELOCITY(FEET/SEC.) = 7.78 DEPTH*VELOCITY(FT*FT/SEC.) = 4.06
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 140.00 = 1670.00 FEET.

FLOW PROCESS FROM NODE 140.00 TO NODE 141.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 257.00 DOWNSTREAM(FEET) = 250.00
FLOW LENGTH(FEET) = 95.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.50
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 29.64
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.44
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 141.00 = 1765.00 FEET.

FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 250.00 DOWNSTREAM ELEVATION(FEET) = 160.00
STREET LENGTH(FEET) = 1225.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 41.58
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.56
HALFSTREET FLOOD WIDTH(FEET) = 21.99
AVERAGE FLOW VELOCITY(FEET/SEC.) = 9.21
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 5.12
STREET FLOW TRAVEL TIME(MIN.) = 2.22 Tc(MIN.) = 12.66
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.384

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN

DPHOSR

RESIDENTIAL

"8-10 DWELLINGS/ACRE" D 11.20 0.20 0.400 75
 COMMERCIAL D 0.30 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.392
 SUBAREA AREA(ACRES) = 11.50 SUBAREA RUNOFF(CFS) = 23.86
 EFFECTIVE AREA(ACRES) = 24.00 AREA-AVERAGED Fm(INCH/HR) = 0.06
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.29
 TOTAL AREA(ACRES) = 24.0 PEAK FLOW RATE(CFS) = 50.23

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.59 HALFSTREET FLOOD WIDTH(FEET) = 23.71
 FLOW VELOCITY(FEET/SEC.) = 9.63 DEPTH*VELOCITY(FT*FT/SEC.) = 5.65
 LONGEST FLOWPATH FROM NODE 136.00 TO NODE 142.00 = 2990.00 FEET.

 FLOW PROCESS FROM NODE 142.00 TO NODE 143.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 150.00 DOWNSTREAM(FEET) = 145.00
 FLOW LENGTH(FEET) = 285.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.9 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 11.97
 ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 50.23
 PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 13.05
 LONGEST FLOWPATH FROM NODE 136.00 TO NODE 143.00 = 3275.00 FEET.

 FLOW PROCESS FROM NODE 143.00 TO NODE 143.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 13.05
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.342
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 RESIDENTIAL
 "8-10 DWELLINGS/ACRE" D 5.60 0.20 0.400 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
 SUBAREA AREA(ACRES) = 5.60 SUBAREA RUNOFF(CFS) = 11.40
 EFFECTIVE AREA(ACRES) = 29.60 AREA-AVERAGED Fm(INCH/HR) = 0.06
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.31
 TOTAL AREA(ACRES) = 29.6 PEAK FLOW RATE(CFS) = 60.73

 FLOW PROCESS FROM NODE 143.00 TO NODE 144.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 145.00 DOWNSTREAM(FEET) = 141.00
 FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.7 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 23.17
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 60.73
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 13.09
 LONGEST FLOWPATH FROM NODE 136.00 TO NODE 144.00 = 3320.00 FEET.

 FLOW PROCESS FROM NODE 144.00 TO NODE 144.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 13.09

DPHOSR

RAINFALL INTENSITY(INCH/HR) = 2.34
AREA-AVERAGED Fm(INCH/HR) = 0.06
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.31
EFFECTIVE STREAM AREA(ACRES) = 29.60
TOTAL STREAM AREA(ACRES) = 29.60
PEAK FLOW RATE(CFS) AT CONFLUENCE = 60.73

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 6 rows of data.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 6 rows of data.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 202.44 Tc(MIN.) = 12.98
EFFECTIVE AREA(ACRES) = 99.21 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 109.1
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 144.00 = 3995.00 FEET.

FLOW PROCESS FROM NODE 144.00 TO NODE 145.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 141.00 DOWNSTREAM(FEET) = 139.00
FLOW LENGTH(FEET) = 325.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 63.0 INCH PIPE IS 47.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.57
ESTIMATED PIPE DIAMETER(INCH) = 63.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 202.44
PIPE TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 13.45
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 145.00 = 4320.00 FEET.

FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.45
RAINFALL INTENSITY(INCH/HR) = 2.30
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.42
EFFECTIVE STREAM AREA(ACRES) = 99.21
TOTAL STREAM AREA(ACRES) = 109.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 202.44

FLOW PROCESS FROM NODE 146.00 TO NODE 147.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

DPHOSR

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 270.00
ELEVATION DATA: UPSTREAM(FEET) = 218.00 DOWNSTREAM(FEET) = 216.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.364
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.833
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.20 0.20 0.400 75 9.36
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA RUNOFF(CFS) = 2.97
TOTAL AREA(ACRES) = 1.20 PEAK FLOW RATE(CFS) = 2.97

FLOW PROCESS FROM NODE 147.00 TO NODE 148.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 216.00 DOWNSTREAM ELEVATION(FEET) = 210.00
STREET LENGTH(FEET) = 405.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.50
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.38
HALFSTREET FLOOD WIDTH(FEET) = 12.78
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.14
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.20
STREET FLOW TRAVEL TIME(MIN.) = 2.15 Tc(MIN.) = 11.51
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.517

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 2.30 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 2.30 SUBAREA RUNOFF(CFS) = 5.05
EFFECTIVE AREA(ACRES) = 3.50 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 7.68

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.60
FLOW VELOCITY(FEET/SEC.) = 3.41 DEPTH*VELOCITY(FT*FT/SEC.) = 1.43
LONGEST FLOWPATH FROM NODE 146.00 TO NODE 148.00 = 675.00 FEET.

FLOW PROCESS FROM NODE 148.00 TO NODE 149.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 210.00 DOWNSTREAM ELEVATION(FEET) = 175.00
STREET LENGTH(FEET) = 475.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00

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INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.64
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.61
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.58
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.36
STREET FLOW TRAVEL TIME(MIN.) = 1.20 Tc(MIN.) = 12.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.378

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.90 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 3.93
EFFECTIVE AREA(ACRES) = 5.40 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 5.4 PEAK FLOW RATE(CFS) = 11.17

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.33
FLOW VELOCITY(FEET/SEC.) = 6.82 DEPTH*VELOCITY(FT*FT/SEC.) = 2.54
LONGEST FLOWPATH FROM NODE 146.00 TO NODE 149.00 = 1150.00 FEET.

FLOW PROCESS FROM NODE 149.00 TO NODE 149.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 12.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.378
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.50 0.20 0.400 75
COMMERCIAL D 1.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.255
SUBAREA AREA(ACRES) = 2.90 SUBAREA RUNOFF(CFS) = 6.07
EFFECTIVE AREA(ACRES) = 8.30 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA(ACRES) = 8.3 PEAK FLOW RATE(CFS) = 17.24

FLOW PROCESS FROM NODE 149.00 TO NODE 145.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 175.00 DOWNSTREAM ELEVATION(FEET) = 146.00
STREET LENGTH(FEET) = 580.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 25.63

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STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.51
 HALFSTREET FLOOD WIDTH(FEET) = 19.65
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.04
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.61
 STREET FLOW TRAVEL TIME(MIN.) = 1.37 Tc(MIN.) = 14.09
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.242
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 RESIDENTIAL
 "8-10 DWELLINGS/ACRE" D 7.90 0.20 0.400 75
 COMMERCIAL D 0.70 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.376
 SUBAREA AREA(ACRES) = 8.60 SUBAREA RUNOFF(CFS) = 16.77
 EFFECTIVE AREA(ACRES) = 16.90 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
 TOTAL AREA(ACRES) = 16.9 PEAK FLOW RATE(CFS) = 33.00

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.55 HALFSTREET FLOOD WIDTH(FEET) = 21.68
 FLOW VELOCITY(FEET/SEC.) = 7.52 DEPTH*VELOCITY(FT*FT/SEC.) = 4.13
 LONGEST FLOWPATH FROM NODE 146.00 TO NODE 145.00 = 1730.00 FEET.

 FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<
 =====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 14.09
 RAINFALL INTENSITY(INCH/HR) = 2.24
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.36
 EFFECTIVE STREAM AREA(ACRES) = 16.90
 TOTAL STREAM AREA(ACRES) = 16.90
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 33.00

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	187.38	8.86	2.925	0.20(0.08)	0.42	70.9	107.00
1	200.47	12.42	2.410	0.20(0.08)	0.42	93.5	101.00
1	202.44	13.45	2.302	0.20(0.08)	0.42	99.2	118.00
1	202.40	13.56	2.292	0.20(0.08)	0.42	99.6	136.00
1	181.46	18.23	1.934	0.20(0.08)	0.42	107.2	112.00
1	171.11	20.65	1.801	0.20(0.08)	0.42	109.1	126.00
2	33.00	14.09	2.242	0.20(0.07)	0.36	16.9	146.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	214.67	8.86	2.925	0.20(0.08)	0.42	81.5	107.00
2	231.81	12.42	2.410	0.20(0.08)	0.41	108.4	101.00
3	234.82	13.45	2.302	0.20(0.08)	0.41	115.3	118.00
4	234.88	13.56	2.292	0.20(0.08)	0.41	115.9	136.00
5	233.01	14.09	2.242	0.20(0.08)	0.41	117.4	146.00
6	209.78	18.23	1.934	0.20(0.08)	0.41	124.1	112.00
7	197.40	20.65	1.801	0.20(0.08)	0.41	126.0	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 234.88 Tc(MIN.) = 13.56
 EFFECTIVE AREA(ACRES) = 115.87 AREA-AVERAGED Fm(INCH/HR) = 0.08
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
 TOTAL AREA(ACRES) = 126.0
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 145.00 = 4320.00 FEET.

DPHOSR

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*****
FLOW PROCESS FROM NODE 145.00 TO NODE 150.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 139.00 DOWNSTREAM(FEET) = 125.00
FLOW LENGTH(FEET) = 780.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 54.0 INCH PIPE IS 41.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.87
ESTIMATED PIPE DIAMETER(INCH) = 54.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 234.88
PIPE TRAVEL TIME(MIN.) = 0.73 Tc(MIN.) = 14.28
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 150.00 = 5100.00 FEET.
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*****
FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.28
RAINFALL INTENSITY(INCH/HR) = 2.22
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.41
EFFECTIVE STREAM AREA(ACRES) = 115.87
TOTAL STREAM AREA(ACRES) = 126.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 234.88
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*****
FLOW PROCESS FROM NODE 151.00 TO NODE 152.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 235.00 DOWNSTREAM(FEET) = 230.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.751
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.418
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS  Tc
LAND USE                GROUP  (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
PUBLIC PARK             D      0.30    0.20    0.850   75  10.73
COMMERCIAL              D      0.30    0.20    0.100   75   6.75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.475
SUBAREA RUNOFF(CFS) = 1.79
TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.79
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*****
FLOW PROCESS FROM NODE 152.00 TO NODE 153.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 230.00 DOWNSTREAM ELEVATION(FEET) = 195.00
STREET LENGTH(FEET) = 390.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200
```

DPHOSR

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.02
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 6.22
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.61
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.53
STREET FLOW TRAVEL TIME(MIN.) = 1.16 Tc(MIN.) = 7.91
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.121

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK D 0.40 0.20 0.850 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.433
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 2.46
EFFECTIVE AREA(ACRES) = 1.50 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.45
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 4.09

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 7.47
FLOW VELOCITY(FEET/SEC.) = 5.91 DEPTH*VELOCITY(FT*FT/SEC.) = 1.75
LONGEST FLOWPATH FROM NODE 151.00 TO NODE 153.00 = 690.00 FEET.

FLOW PROCESS FROM NODE 153.00 TO NODE 154.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 195.00 DOWNSTREAM ELEVATION(FEET) = 180.00
STREET LENGTH(FEET) = 275.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.88
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.88
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.81
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.11
STREET FLOW TRAVEL TIME(MIN.) = 0.79 Tc(MIN.) = 8.70
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.956

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 3.70 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 3.70 SUBAREA RUNOFF(CFS) = 9.58
EFFECTIVE AREA(ACRES) = 5.20 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 5.2 PEAK FLOW RATE(CFS) = 13.45

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.13
FLOW VELOCITY(FEET/SEC.) = 6.36 DEPTH*VELOCITY(FT*FT/SEC.) = 2.60
LONGEST FLOWPATH FROM NODE 151.00 TO NODE 154.00 = 965.00 FEET.

FLOW PROCESS FROM NODE 154.00 TO NODE 155.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
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>>>>(STREET TABLE SECTION # 2 USED)<<<<

UPSTREAM ELEVATION(FEET) = 180.00 DOWNSTREAM ELEVATION(FEET) = 175.00
STREET LENGTH(FEET) = 125.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 21.04
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.48
HALFSTREET FLOOD WIDTH(FEET) = 17.88
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.35
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.07
STREET FLOW TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 9.03
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.894

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 6.00 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 6.00 SUBAREA RUNOFF(CFS) = 15.19
EFFECTIVE AREA(ACRES) = 11.20 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 11.2 PEAK FLOW RATE(CFS) = 28.35

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.00
FLOW VELOCITY(FEET/SEC.) = 6.35 DEPTH*VELOCITY(FT*FT/SEC.) = 3.09
LONGEST FLOWPATH FROM NODE 151.00 TO NODE 155.00 = 1090.00 FEET.

FLOW PROCESS FROM NODE 155.00 TO NODE 156.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

UPSTREAM ELEVATION(FEET) = 175.00 DOWNSTREAM ELEVATION(FEET) = 139.00
STREET LENGTH(FEET) = 570.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 41.26
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.45
HALFSTREET FLOOD WIDTH(FEET) = 16.24
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.48
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.38
STREET FLOW TRAVEL TIME(MIN.) = 1.27 Tc(MIN.) = 10.30
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.684

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 3.90 0.20 0.400 75
RESIDENTIAL

DPHOSR

"11+ DWELLINGS/ACRE" D 6.20 0.20 0.200 75
 COMMERCIAL D 0.80 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.264
 SUBAREA AREA(ACRES) = 10.90 SUBAREA RUNOFF(CFS) = 25.81
 EFFECTIVE AREA(ACRES) = 22.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.34
 TOTAL AREA(ACRES) = 22.1 PEAK FLOW RATE(CFS) = 52.04

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 17.80
 FLOW VELOCITY(FEET/SEC.) = 7.91 DEPTH*VELOCITY(FT*FT/SEC.) = 3.82
 LONGEST FLOWPATH FROM NODE 151.00 TO NODE 156.00 = 1660.00 FEET.

 FLOW PROCESS FROM NODE 156.00 TO NODE 150.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 133.50 DOWNSTREAM(FEET) = 125.00
 FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 31.62
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 52.04
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 10.32
 LONGEST FLOWPATH FROM NODE 151.00 TO NODE 150.00 = 1700.00 FEET.

 FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
 =====
 TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 10.32
 RAINFALL INTENSITY(INCH/HR) = 2.68
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.34
 EFFECTIVE STREAM AREA(ACRES) = 22.10
 TOTAL STREAM AREA(ACRES) = 22.10
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 52.04

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	214.67	9.60	2.794	0.20(0.08)	0.42	81.5	107.00
1	231.81	13.15	2.333	0.20(0.08)	0.41	108.4	101.00
1	234.82	14.18	2.234	0.20(0.08)	0.41	115.3	118.00
1	234.88	14.28	2.225	0.20(0.08)	0.41	115.9	136.00
1	233.01	14.82	2.178	0.20(0.08)	0.41	117.4	146.00
1	209.78	18.98	1.890	0.20(0.08)	0.41	124.1	112.00
1	197.40	21.40	1.765	0.20(0.08)	0.41	126.0	126.00
2	52.04	10.32	2.680	0.20(0.07)	0.34	22.1	151.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	265.17	9.60	2.794	0.20(0.08)	0.40	102.0	107.00
2	270.18	10.32	2.680	0.20(0.08)	0.40	109.0	151.00
3	276.92	13.15	2.333	0.20(0.08)	0.40	130.5	101.00
4	277.97	14.18	2.234	0.20(0.08)	0.40	137.4	118.00
5	277.84	14.28	2.225	0.20(0.08)	0.40	138.0	136.00
6	275.04	14.82	2.178	0.20(0.08)	0.40	139.5	146.00
7	246.08	18.98	1.890	0.20(0.08)	0.40	146.2	112.00
8	231.20	21.40	1.765	0.20(0.08)	0.40	148.1	126.00

DPHOSR

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 277.97 Tc(MIN.) = 14.18
EFFECTIVE AREA(ACRES) = 137.44 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 148.1
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 150.00 = 5100.00 FEET.

FLOW PROCESS FROM NODE 150.00 TO NODE 159.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 125.00 DOWNSTREAM(FEET) = 102.00
FLOW LENGTH(FEET) = 610.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 51.0 INCH PIPE IS 37.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.79
ESTIMATED PIPE DIAMETER(INCH) = 51.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 277.97
PIPE TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 14.59
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 159.00 = 5710.00 FEET.

FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 14.59
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.198
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 5.10 0.20 0.400 75
COMMERCIAL D 3.30 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.282
SUBAREA AREA(ACRES) = 8.40 SUBAREA RUNOFF(CFS) = 16.19
EFFECTIVE AREA(ACRES) = 145.84 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 156.5 PEAK FLOW RATE(CFS) = 278.14

FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.59
RAINFALL INTENSITY(INCH/HR) = 2.20
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.39
EFFECTIVE STREAM AREA(ACRES) = 145.84
TOTAL STREAM AREA(ACRES) = 156.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 278.14

FLOW PROCESS FROM NODE 160.00 TO NODE 161.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 260.00
ELEVATION DATA: UPSTREAM(FEET) = 145.00 DOWNSTREAM(FEET) = 143.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.441
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.232

SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)

DPHOSR

COMMERCIAL D 0.50 0.20 0.100 75 7.44
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 1.45
TOTAL AREA(ACRES) = 0.50 PEAK FLOW RATE(CFS) = 1.45

FLOW PROCESS FROM NODE 161.00 TO NODE 162.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 143.00 DOWNSTREAM ELEVATION(FEET) = 138.00
STREET LENGTH(FEET) = 345.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.58
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.05
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.79
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.00
STREET FLOW TRAVEL TIME(MIN.) = 2.06 Tc(MIN.) = 9.50
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.810
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	1.70	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 4.27
EFFECTIVE AREA(ACRES) = 2.20 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 5.52

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.40
FLOW VELOCITY(FEET/SEC.) = 3.07 DEPTH*VELOCITY(FT*FT/SEC.) = 1.24
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 162.00 = 605.00 FEET.

FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 9.50
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.810
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	2.50	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.50 SUBAREA RUNOFF(CFS) = 6.28
EFFECTIVE AREA(ACRES) = 4.70 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 4.7 PEAK FLOW RATE(CFS) = 11.80

FLOW PROCESS FROM NODE 162.00 TO NODE 163.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

DPHOSR

ELEVATION DATA: UPSTREAM(FEET) = 132.00 DOWNSTREAM(FEET) = 127.00
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.77
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.80
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 9.60
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 163.00 = 685.00 FEET.

FLOW PROCESS FROM NODE 163.00 TO NODE 163.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 9.60
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.793
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 1.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 4.24
EFFECTIVE AREA(ACRES) = 6.40 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 6.4 PEAK FLOW RATE(CFS) = 15.97

FLOW PROCESS FROM NODE 163.00 TO NODE 164.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 127.00 DOWNSTREAM(FEET) = 117.50
FLOW LENGTH(FEET) = 350.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.59
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.97
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 10.15
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 164.00 = 1035.00 FEET.

FLOW PROCESS FROM NODE 164.00 TO NODE 164.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.15
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.706
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.40 0.20 0.400 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.321
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 4.52
EFFECTIVE AREA(ACRES) = 8.30 AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.15
TOTAL AREA(ACRES) = 8.3 PEAK FLOW RATE(CFS) = 19.99

FLOW PROCESS FROM NODE 164.00 TO NODE 165.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 117.50 DOWNSTREAM(FEET) = 114.50
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.78
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

DPHOSR

PIPE-FLOW(CFS) = 19.99
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 10.18
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 165.00 = 1070.00 FEET.

FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.18
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.701
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 2.20 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 5.31
EFFECTIVE AREA(ACRES) = 10.50 AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.14
TOTAL AREA(ACRES) = 10.5 PEAK FLOW RATE(CFS) = 25.26

FLOW PROCESS FROM NODE 165.00 TO NODE 159.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 114.50 DOWNSTREAM(FEET) = 102.00
FLOW LENGTH(FEET) = 220.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.14
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 25.26
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 10.41
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 159.00 = 1290.00 FEET.

FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.41
RAINFALL INTENSITY(INCH/HR) = 2.67
AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.14
EFFECTIVE STREAM AREA(ACRES) = 10.50
TOTAL STREAM AREA(ACRES) = 10.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 25.26

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists data for 11 different stream segments.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists peak flow data for 2 streams.

	DPHOSR						
1	290.01	10.01	2.727	0.20(0.07)	0.37	120.5	107.00
2	293.22	10.41	2.667	0.20(0.07)	0.37	124.9	160.00
3	295.00	10.73	2.621	0.20(0.07)	0.37	127.9	151.00
4	298.59	13.56	2.292	0.20(0.08)	0.38	149.4	101.00
5	298.90	14.59	2.198	0.20(0.08)	0.38	156.3	118.00
6	298.65	14.69	2.189	0.20(0.08)	0.38	156.9	136.00
7	295.30	15.23	2.144	0.20(0.08)	0.38	158.4	146.00
8	266.20	19.41	1.866	0.20(0.08)	0.38	165.1	112.00
9	250.98	21.83	1.745	0.20(0.08)	0.38	167.0	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 298.90 Tc(MIN.) = 14.59
EFFECTIVE AREA(ACRES) = 156.34 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.38
TOTAL AREA(ACRES) = 167.0
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 159.00 = 5710.00 FEET.

FLOW PROCESS FROM NODE 159.00 TO NODE 168.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 102.00 DOWNSTREAM(FEET) = 94.30
FLOW LENGTH(FEET) = 1005.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 69.0 INCH PIPE IS 53.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.76
ESTIMATED PIPE DIAMETER(INCH) = 69.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 298.90
PIPE TRAVEL TIME(MIN.) = 1.22 Tc(MIN.) = 15.81
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 168.00 = 6715.00 FEET.

FLOW PROCESS FROM NODE 168.00 TO NODE 168.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 15.81
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.099
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	7.50	0.20	0.100	75
PUBLIC PARK	D	0.20	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.119
SUBAREA AREA(ACRES) = 7.70 SUBAREA RUNOFF(CFS) = 14.38
EFFECTIVE AREA(ACRES) = 164.04 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.37
TOTAL AREA(ACRES) = 174.7 PEAK FLOW RATE(CFS) = 299.14

FLOW PROCESS FROM NODE 168.00 TO NODE 169.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 94.30 DOWNSTREAM(FEET) = 93.50
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 75.0 INCH PIPE IS 56.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.09
ESTIMATED PIPE DIAMETER(INCH) = 75.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 299.14
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 16.01
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 169.00 = 6865.00 FEET.

FLOW PROCESS FROM NODE 169.00 TO NODE 169.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

DPHOSR

TIME OF CONCENTRATION(MIN.) = 16.01
RAINFALL INTENSITY(INCH/HR) = 2.08
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.37
EFFECTIVE STREAM AREA(ACRES) = 164.04
TOTAL STREAM AREA(ACRES) = 174.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 299.14

FLOW PROCESS FROM NODE 170.00 TO NODE 171.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 145.00 DOWNSTREAM(FEET) = 140.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.751
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.418

SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL D 0.90 0.20 0.100 75 6.75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 2.75
TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 2.75

FLOW PROCESS FROM NODE 171.00 TO NODE 172.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 130.00 DOWNSTREAM(FEET) = 128.00
FLOW LENGTH(FEET) = 265.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 9.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.24
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.75
PIPE TRAVEL TIME(MIN.) = 1.04 Tc(MIN.) = 7.79
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 172.00 = 565.00 FEET.

FLOW PROCESS FROM NODE 172.00 TO NODE 172.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 7.79
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.148
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 3.10 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 3.10 SUBAREA RUNOFF(CFS) = 8.73
EFFECTIVE AREA(ACRES) = 4.00 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 11.26

FLOW PROCESS FROM NODE 172.00 TO NODE 169.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 128.00 DOWNSTREAM(FEET) = 93.50
FLOW LENGTH(FEET) = 215.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.28

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ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 11.26
 PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 7.98
 LONGEST FLOWPATH FROM NODE 170.00 TO NODE 169.00 = 780.00 FEET.

 FLOW PROCESS FROM NODE 169.00 TO NODE 169.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 7.98
 RAINFALL INTENSITY(INCH/HR) = 3.11
 AREA-AVERAGED Fm(INCH/HR) = 0.02
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.10
 EFFECTIVE STREAM AREA(ACRES) = 4.00
 TOTAL STREAM AREA(ACRES) = 4.00
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.26

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	290.01	11.44	2.526	0.20(0.07)	0.35	128.2	107.00
1	293.22	11.84	2.477	0.20(0.07)	0.35	132.6	160.00
1	295.00	12.15	2.440	0.20(0.07)	0.36	135.6	151.00
1	298.59	14.98	2.164	0.20(0.07)	0.36	157.1	101.00
1	299.14	16.01	2.084	0.20(0.07)	0.37	164.0	118.00
1	298.94	16.12	2.076	0.20(0.07)	0.37	164.6	136.00
1	295.78	16.65	2.037	0.20(0.07)	0.37	166.1	146.00
1	268.52	20.87	1.790	0.20(0.07)	0.37	172.8	112.00
1	254.01	23.31	1.680	0.20(0.07)	0.37	174.7	126.00
2	11.26	7.98	3.106	0.20(0.02)	0.10	4.0	170.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	261.23	7.98	3.106	0.20(0.07)	0.34	93.4	170.00
2	299.16	11.44	2.526	0.20(0.07)	0.35	132.2	107.00
3	302.19	11.84	2.477	0.20(0.07)	0.35	136.6	160.00
4	303.83	12.15	2.440	0.20(0.07)	0.35	139.6	151.00
5	306.41	14.98	2.164	0.20(0.07)	0.36	161.1	101.00
6	306.67	16.01	2.084	0.20(0.07)	0.36	168.0	118.00
7	306.44	16.12	2.076	0.20(0.07)	0.36	168.6	136.00
8	303.14	16.65	2.037	0.20(0.07)	0.36	170.1	146.00
9	274.98	20.87	1.790	0.20(0.07)	0.36	176.8	112.00
10	260.07	23.31	1.680	0.20(0.07)	0.36	178.7	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 306.67 Tc(MIN.) = 16.01
 EFFECTIVE AREA(ACRES) = 168.04 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
 TOTAL AREA(ACRES) = 178.7
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 169.00 = 6865.00 FEET.

 FLOW PROCESS FROM NODE 169.00 TO NODE 173.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 93.50 DOWNSTREAM(FEET) = 91.80
 FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 66.0 INCH PIPE IS 53.5 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 14.86
 ESTIMATED PIPE DIAMETER(INCH) = 66.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 306.67
 PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 16.22

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LONGEST FLOWPATH FROM NODE 112.00 TO NODE 173.00 = 7045.00 FEET.
*****
FLOW PROCESS FROM NODE 173.00 TO NODE 173.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.22
RAINFALL INTENSITY(INCH/HR) = 2.07
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 168.04
TOTAL STREAM AREA(ACRES) = 178.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 306.67
*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 500.00
ELEVATION DATA: UPSTREAM(FEET) = 140.00 DOWNSTREAM(FEET) = 115.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.648
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.448
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL D 0.70 0.20 0.100 75 6.65
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.60 0.20 0.500 75 8.51
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.285
SUBAREA RUNOFF(CFS) = 3.97
TOTAL AREA(ACRES) = 1.30 PEAK FLOW RATE(CFS) = 3.97
*****
FLOW PROCESS FROM NODE 301.00 TO NODE 173.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 100.00 DOWNSTREAM(FEET) = 91.80
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.10
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.97
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 6.70
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 173.00 = 550.00 FEET.
*****
FLOW PROCESS FROM NODE 173.00 TO NODE 173.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.70
RAINFALL INTENSITY(INCH/HR) = 3.43
AREA-AVERAGED Fm(INCH/HR) = 0.06
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.28
EFFECTIVE STREAM AREA(ACRES) = 1.30
TOTAL STREAM AREA(ACRES) = 1.30
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.97

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** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	261.23	8.19	3.060	0.20(0.07)	0.34	93.4	170.00
1	299.16	11.64	2.501	0.20(0.07)	0.35	132.2	107.00
1	302.19	12.04	2.453	0.20(0.07)	0.35	136.6	160.00
1	303.83	12.36	2.417	0.20(0.07)	0.35	139.6	151.00
1	306.41	15.19	2.148	0.20(0.07)	0.36	161.1	101.00
1	306.67	16.22	2.069	0.20(0.07)	0.36	168.0	118.00
1	306.44	16.32	2.061	0.20(0.07)	0.36	168.6	136.00
1	303.14	16.86	2.023	0.20(0.07)	0.36	170.1	146.00
1	274.98	21.08	1.780	0.20(0.07)	0.36	176.8	112.00
1	260.07	23.52	1.672	0.20(0.07)	0.36	178.7	126.00
2	3.97	6.70	3.432	0.20(0.06)	0.28	1.3	300.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	244.42	6.70	3.432	0.20(0.07)	0.34	77.8	300.00
2	264.76	8.19	3.060	0.20(0.07)	0.34	94.7	170.00
3	302.03	11.64	2.501	0.20(0.07)	0.35	133.5	107.00
4	305.01	12.04	2.453	0.20(0.07)	0.35	137.9	160.00
5	306.61	12.36	2.417	0.20(0.07)	0.35	140.9	151.00
6	308.87	15.19	2.148	0.20(0.07)	0.36	162.4	101.00
7	309.04	16.22	2.069	0.20(0.07)	0.36	169.3	118.00
8	308.80	16.32	2.061	0.20(0.07)	0.36	169.9	136.00
9	305.45	16.86	2.023	0.20(0.07)	0.36	171.4	146.00
10	277.00	21.08	1.780	0.20(0.07)	0.36	178.1	112.00
11	261.96	23.52	1.672	0.20(0.07)	0.36	180.0	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 309.04 Tc(MIN.) = 16.22
EFFECTIVE AREA(ACRES) = 169.34 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 180.0
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 173.00 = 7045.00 FEET.

FLOW PROCESS FROM NODE 173.00 TO NODE 175.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 91.80 DOWNSTREAM(FEET) = 74.40
FLOW LENGTH(FEET) = 470.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 54.0 INCH PIPE IS 38.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 25.38
ESTIMATED PIPE DIAMETER(INCH) = 54.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 309.04
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 16.52
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 175.00 = 7515.00 FEET.

FLOW PROCESS FROM NODE 175.00 TO NODE 175.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.52
RAINFALL INTENSITY(INCH/HR) = 2.05
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 169.34
TOTAL STREAM AREA(ACRES) = 180.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 309.04

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FLOW PROCESS FROM NODE 176.00 TO NODE 177.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 125.00 DOWNSTREAM(FEET) = 120.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.994
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.102
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
CONDOMINIUMS D 0.90 0.20 0.350 75 7.99
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA RUNOFF(CFS) = 2.46
TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 2.46

FLOW PROCESS FROM NODE 177.00 TO NODE 178.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 110.00 DOWNSTREAM(FEET) = 105.00
FLOW LENGTH(FEET) = 290.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.79
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.46
PIPE TRAVEL TIME(MIN.) = 0.84 Tc(MIN.) = 8.83
LONGEST FLOWPATH FROM NODE 176.00 TO NODE 178.00 = 590.00 FEET.

FLOW PROCESS FROM NODE 178.00 TO NODE 178.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.83
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.931
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
CONDOMINIUMS D 1.50 0.20 0.350 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA AREA(ACRES) = 1.50 SUBAREA RUNOFF(CFS) = 3.86
EFFECTIVE AREA(ACRES) = 2.40 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 6.18

FLOW PROCESS FROM NODE 178.00 TO NODE 179.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 105.00 DOWNSTREAM(FEET) = 80.00
FLOW LENGTH(FEET) = 390.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.86
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.18
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 9.38
LONGEST FLOWPATH FROM NODE 176.00 TO NODE 179.00 = 980.00 FEET.

FLOW PROCESS FROM NODE 179.00 TO NODE 179.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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MAINLINE Tc(MIN.) = 9.38
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.831
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 CONDOMINIUMS D 3.00 0.20 0.350 75
 RESIDENTIAL
 "11+ DWELLINGS/ACRE" D 0.20 0.20 0.200 75
 PUBLIC PARK D 0.40 0.20 0.850 75
 COMMERCIAL D 0.90 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.338
 SUBAREA AREA(ACRES) = 4.50 SUBAREA RUNOFF(CFS) = 11.19
 EFFECTIVE AREA(ACRES) = 6.90 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.34
 TOTAL AREA(ACRES) = 6.9 PEAK FLOW RATE(CFS) = 17.16

FLOW PROCESS FROM NODE 179.00 TO NODE 175.00 IS CODE = 31

 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====

ELEVATION DATA: UPSTREAM(FEET) = 80.00 DOWNSTREAM(FEET) = 74.40
 FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 15.89
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 17.16
 PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 9.46
 LONGEST FLOWPATH FROM NODE 176.00 TO NODE 175.00 = 1060.00 FEET.

FLOW PROCESS FROM NODE 175.00 TO NODE 175.00 IS CODE = 1

 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
 =====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 9.46
 RAINFALL INTENSITY(INCH/HR) = 2.82
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.34
 EFFECTIVE STREAM AREA(ACRES) = 6.90
 TOTAL STREAM AREA(ACRES) = 6.90
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.16

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	244.42	7.03	3.339	0.20(0.07)	0.34	77.8	300.00
1	264.76	8.51	2.994	0.20(0.07)	0.34	94.7	170.00
1	302.03	11.96	2.463	0.20(0.07)	0.35	133.5	107.00
1	305.01	12.36	2.417	0.20(0.07)	0.35	137.9	160.00
1	306.61	12.67	2.383	0.20(0.07)	0.35	140.9	151.00
1	308.87	15.50	2.123	0.20(0.07)	0.36	162.4	101.00
1	309.04	16.52	2.046	0.20(0.07)	0.36	169.3	118.00
1	308.80	16.63	2.039	0.20(0.07)	0.36	169.9	136.00
1	305.45	17.17	2.002	0.20(0.07)	0.36	171.4	146.00
1	277.00	21.40	1.765	0.20(0.07)	0.36	178.1	112.00
1	261.96	23.85	1.658	0.20(0.07)	0.36	180.0	126.00
2	17.16	9.46	2.817	0.20(0.07)	0.34	6.9	176.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	259.59	7.03	3.339	0.20(0.07)	0.34	82.9	300.00
2	281.18	8.51	2.994	0.20(0.07)	0.34	100.9	170.00

	DPHOSR							
3	292.22	9.46	2.817	0.20(0.07)	0.34	112.3	176.00	
4	316.98	11.96	2.463	0.20(0.07)	0.35	140.4	107.00	
5	319.67	12.36	2.417	0.20(0.07)	0.35	144.8	160.00	
6	321.05	12.67	2.383	0.20(0.07)	0.35	147.8	151.00	
7	321.70	15.50	2.123	0.20(0.07)	0.36	169.3	101.00	
8	321.39	16.52	2.046	0.20(0.07)	0.36	176.2	118.00	
9	321.10	16.63	2.039	0.20(0.07)	0.36	176.8	136.00	
10	317.52	17.17	2.002	0.20(0.07)	0.36	178.3	146.00	
11	287.59	21.40	1.765	0.20(0.07)	0.36	185.0	112.00	
12	271.89	23.85	1.658	0.20(0.07)	0.36	186.9	126.00	

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 321.70 Tc(MIN.) = 15.50
EFFECTIVE AREA(ACRES) = 169.33 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 186.9
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 175.00 = 7515.00 FEET.

FLOW PROCESS FROM NODE 175.00 TO NODE 180.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 74.40 DOWNSTREAM(FEET) = 51.60
FLOW LENGTH(FEET) = 270.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 45.0 INCH PIPE IS 35.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.38
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 321.70
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 15.63
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 180.00 = 7785.00 FEET.

FLOW PROCESS FROM NODE 180.00 TO NODE 180.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 15.63
RAINFALL INTENSITY(INCH/HR) = 2.11
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 169.33
TOTAL STREAM AREA(ACRES) = 186.90
PEAK FLOW RATE(CFS) AT CONFLUENCE = 321.70

FLOW PROCESS FROM NODE 181.00 TO NODE 182.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 125.00 DOWNSTREAM(FEET) = 120.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.994
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.102
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
CONDOMINIUMS	D	1.10	0.20	0.350	75	7.99

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA RUNOFF(CFS) = 3.00
TOTAL AREA(ACRES) = 1.10 PEAK FLOW RATE(CFS) = 3.00

FLOW PROCESS FROM NODE 182.00 TO NODE 183.00 IS CODE = 31

DPHOSR

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 110.00 DOWNSTREAM(FEET) = 105.00
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.34
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.00
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 8.11
LONGEST FLOWPATH FROM NODE 181.00 TO NODE 183.00 = 370.00 FEET.

FLOW PROCESS FROM NODE 183.00 TO NODE 183.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.11
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.078
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
CONDOMINIUMS D 2.00 0.20 0.350 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA AREA(ACRES) = 2.00 SUBAREA RUNOFF(CFS) = 5.41
EFFECTIVE AREA(ACRES) = 3.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 8.39

FLOW PROCESS FROM NODE 183.00 TO NODE 184.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 105.00 DOWNSTREAM(FEET) = 60.00
FLOW LENGTH(FEET) = 415.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.57
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.39
PIPE TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 8.55
LONGEST FLOWPATH FROM NODE 181.00 TO NODE 184.00 = 785.00 FEET.

FLOW PROCESS FROM NODE 184.00 TO NODE 184.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.55
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.985
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
CONDOMINIUMS D 3.10 0.20 0.350 75
COMMERCIAL D 0.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.321
SUBAREA AREA(ACRES) = 3.50 SUBAREA RUNOFF(CFS) = 9.20
EFFECTIVE AREA(ACRES) = 6.60 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.33
TOTAL AREA(ACRES) = 6.6 PEAK FLOW RATE(CFS) = 17.33

FLOW PROCESS FROM NODE 184.00 TO NODE 180.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 60.00 DOWNSTREAM(FEET) = 51.60
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013

DPHOSR

DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.3 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 19.29
ESTIMATED PIPE DIAMETER (INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 17.33
PIPE TRAVEL TIME (MIN.) = 0.06 Tc (MIN.) = 8.61
LONGEST FLOWPATH FROM NODE 181.00 TO NODE 180.00 = 855.00 FEET.

FLOW PROCESS FROM NODE 180.00 TO NODE 180.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION (MIN.) = 8.61
RAINFALL INTENSITY (INCH/HR) = 2.97
AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.33
EFFECTIVE STREAM AREA (ACRES) = 6.60
TOTAL STREAM AREA (ACRES) = 6.60
PEAK FLOW RATE (CFS) AT CONFLUENCE = 17.33

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp (Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists 18 rows of data for different stream numbers and their respective flow characteristics.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp (Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists 13 rows of data for different stream numbers and their respective peak flow rates.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 334.78 Tc (MIN.) = 12.80
EFFECTIVE AREA (ACRES) = 154.45 AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA (ACRES) = 193.5
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 180.00 = 7785.00 FEET.

FLOW PROCESS FROM NODE 180.00 TO NODE 185.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

DPHOSR

ELEVATION DATA: UPSTREAM(FEET) = 51.60 DOWNSTREAM(FEET) = 46.80
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 45.0 INCH PIPE IS 36.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.98
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 334.78
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 12.83
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 185.00 = 7840.00 FEET.

FLOW PROCESS FROM NODE 185.00 TO NODE 185.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.83
RAINFALL INTENSITY(INCH/HR) = 2.37
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.35
EFFECTIVE STREAM AREA(ACRES) = 154.45
TOTAL STREAM AREA(ACRES) = 193.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 334.78

FLOW PROCESS FROM NODE 186.00 TO NODE 187.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 260.00
ELEVATION DATA: UPSTREAM(FEET) = 120.00 DOWNSTREAM(FEET) = 115.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.195
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.590
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL D 0.60 0.20 0.100 75 6.20
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 1.93
TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.93

FLOW PROCESS FROM NODE 187.00 TO NODE 188.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

UPSTREAM ELEVATION(FEET) = 115.00 DOWNSTREAM ELEVATION(FEET) = 105.00
STREET LENGTH(FEET) = 365.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.42
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.28
HALFSTREET FLOOD WIDTH(FEET) = 7.56
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.20
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.89
STREET FLOW TRAVEL TIME(MIN.) = 1.90 Tc(MIN.) = 8.10

DPHOSR

* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.080
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 COMMERCIAL D 1.80 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 1.80 SUBAREA RUNOFF(CFS) = 4.96
 EFFECTIVE AREA(ACRES) = 2.40 AREA-AVERAGED Fm(INCH/HR) = 0.02
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 6.61

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.09
 FLOW VELOCITY(FEET/SEC.) = 3.50 DEPTH*VELOCITY(FT*FT/SEC.) = 1.08
 LONGEST FLOWPATH FROM NODE 186.00 TO NODE 188.00 = 625.00 FEET.

FLOW PROCESS FROM NODE 188.00 TO NODE 189.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 105.00 DOWNSTREAM ELEVATION(FEET) = 70.00
 STREET LENGTH(FEET) = 360.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.35
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.30
 HALFSTREET FLOOD WIDTH(FEET) = 8.64
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.56
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.96
 STREET FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 9.01
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.896

SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 PUBLIC PARK D 0.70 0.20 0.850 75
 COMMERCIAL D 3.00 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.242
 SUBAREA AREA(ACRES) = 3.70 SUBAREA RUNOFF(CFS) = 9.48
 EFFECTIVE AREA(ACRES) = 6.10 AREA-AVERAGED Fm(INCH/HR) = 0.04
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.19
 TOTAL AREA(ACRES) = 6.1 PEAK FLOW RATE(CFS) = 15.70

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 9.99
 FLOW VELOCITY(FEET/SEC.) = 7.03 DEPTH*VELOCITY(FT*FT/SEC.) = 2.29
 LONGEST FLOWPATH FROM NODE 186.00 TO NODE 189.00 = 985.00 FEET.

FLOW PROCESS FROM NODE 189.00 TO NODE 185.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 60.00 DOWNSTREAM(FEET) = 46.80
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 8.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 22.58
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 15.70

DPHOSR
 PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 9.06
 LONGEST FLOWPATH FROM NODE 186.00 TO NODE 185.00 = 1055.00 FEET.

 FLOW PROCESS FROM NODE 185.00 TO NODE 185.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 9.06
 RAINFALL INTENSITY(INCH/HR) = 2.89
 AREA-AVERAGED Fm(INCH/HR) = 0.04
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.19
 EFFECTIVE STREAM AREA(ACRES) = 6.10
 TOTAL STREAM AREA(ACRES) = 6.10
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.70

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	275.66	7.20	3.295	0.20(0.07)	0.34	88.4	300.00
1	298.10	8.64	2.968	0.20(0.07)	0.34	107.2	181.00
1	298.48	8.67	2.962	0.20(0.07)	0.34	107.5	170.00
1	308.49	9.62	2.790	0.20(0.07)	0.34	118.9	176.00
1	331.18	12.12	2.445	0.20(0.07)	0.35	147.0	107.00
1	333.60	12.52	2.399	0.20(0.07)	0.35	151.4	160.00
1	334.78	12.83	2.366	0.20(0.07)	0.35	154.4	151.00
1	333.90	15.65	2.111	0.20(0.07)	0.35	175.9	101.00
1	333.14	16.68	2.035	0.20(0.07)	0.36	182.8	118.00
1	332.81	16.79	2.028	0.20(0.07)	0.36	183.4	136.00
1	329.01	17.33	1.991	0.20(0.07)	0.36	184.9	146.00
1	297.68	21.56	1.757	0.20(0.07)	0.36	191.6	112.00
1	281.35	24.01	1.652	0.20(0.07)	0.36	193.5	126.00
2	15.70	9.06	2.887	0.20(0.04)	0.19	6.1	186.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	289.91	7.20	3.295	0.20(0.07)	0.33	93.3	300.00
2	313.48	8.64	2.968	0.20(0.07)	0.33	113.0	181.00
3	313.88	8.67	2.962	0.20(0.07)	0.33	113.3	170.00
4	318.35	9.06	2.887	0.20(0.07)	0.33	118.4	186.00
5	323.65	9.62	2.790	0.20(0.07)	0.34	125.0	176.00
6	344.44	12.12	2.445	0.20(0.07)	0.34	153.1	107.00
7	346.61	12.52	2.399	0.20(0.07)	0.34	157.5	160.00
8	347.61	12.83	2.366	0.20(0.07)	0.34	160.5	151.00
9	345.33	15.65	2.111	0.20(0.07)	0.35	182.0	101.00
10	344.15	16.68	2.035	0.20(0.07)	0.35	188.9	118.00
11	343.78	16.79	2.028	0.20(0.07)	0.35	189.5	136.00
12	339.78	17.33	1.991	0.20(0.07)	0.35	191.0	146.00
13	307.16	21.56	1.757	0.20(0.07)	0.35	197.7	112.00
14	290.25	24.01	1.652	0.20(0.07)	0.36	199.6	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 347.61 Tc(MIN.) = 12.83
 EFFECTIVE AREA(ACRES) = 160.55 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.34
 TOTAL AREA(ACRES) = 199.6
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 185.00 = 7840.00 FEET.

 FLOW PROCESS FROM NODE 185.00 TO NODE 191.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 46.80 DOWNSTREAM(FEET) = 5.50

DPHOSR

FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 48.0 INCH PIPE IS 35.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 34.76
 ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 347.61
 PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 13.08
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 191.00 = 8355.00 FEET.

 FLOW PROCESS FROM NODE 191.00 TO NODE 191.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 13.08
 RAINFALL INTENSITY(INCH/HR) = 2.34
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.34
 EFFECTIVE STREAM AREA(ACRES) = 160.55
 TOTAL STREAM AREA(ACRES) = 199.60
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 347.61

 FLOW PROCESS FROM NODE 192.00 TO NODE 193.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 280.00
 ELEVATION DATA: UPSTREAM(FEET) = 142.00 DOWNSTREAM(FEET) = 140.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.955
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.736
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	0.70	0.20	0.500	75	9.95

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
 SUBAREA RUNOFF(CFS) = 1.66
 TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 1.66

 FLOW PROCESS FROM NODE 193.00 TO NODE 194.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 140.00 DOWNSTREAM ELEVATION(FEET) = 138.00
 STREET LENGTH(FEET) = 320.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.07
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.30
 HALFSTREET FLOOD WIDTH(FEET) = 8.91
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.68
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.51
 STREET FLOW TRAVEL TIME(MIN.) = 3.17 Tc(MIN.) = 13.12
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.335

DPHOSR

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.40	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 2.82					
EFFECTIVE AREA(ACRES) = 2.10 AREA-AVERAGED Fm(INCH/HR) = 0.10					
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50					
TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 4.22					

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.26
 FLOW VELOCITY(FEET/SEC.) = 1.80 DEPTH*VELOCITY(FT*FT/SEC.) = 0.60
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 194.00 = 600.00 FEET.

FLOW PROCESS FROM NODE 194.00 TO NODE 195.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 138.00 DOWNSTREAM ELEVATION(FEET) = 135.00
 STREET LENGTH(FEET) = 415.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.86
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.38
 HALFSTREET FLOOD WIDTH(FEET) = 12.87
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.22
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.85
 STREET FLOW TRAVEL TIME(MIN.) = 3.12 Tc(MIN.) = 16.25
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.066

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	4.10	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 4.10 SUBAREA RUNOFF(CFS) = 7.26					
EFFECTIVE AREA(ACRES) = 6.20 AREA-AVERAGED Fm(INCH/HR) = 0.10					
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50					
TOTAL AREA(ACRES) = 6.2 PEAK FLOW RATE(CFS) = 10.97					

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.76
 FLOW VELOCITY(FEET/SEC.) = 2.39 DEPTH*VELOCITY(FT*FT/SEC.) = 1.01
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 195.00 = 1015.00 FEET.

FLOW PROCESS FROM NODE 195.00 TO NODE 196.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 130.00 DOWNSTREAM(FEET) = 120.00
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 20.98
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 10.97

DPHOSR
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 16.29
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 196.00 = 1065.00 FEET.

FLOW PROCESS FROM NODE 196.00 TO NODE 196.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) =	16.29				
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	2.064				
SUBAREA LOSS RATE DATA(AMC II):					
DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	3.50	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) =		3.50	SUBAREA RUNOFF(CFS) = 6.19		
EFFECTIVE AREA(ACRES) =		9.70	AREA-AVERAGED Fm(INCH/HR) = 0.10		
AREA-AVERAGED Fp(INCH/HR) =		0.20	AREA-AVERAGED Ap = 0.50		
TOTAL AREA(ACRES) =		9.7	PEAK FLOW RATE(CFS) = 17.14		

FLOW PROCESS FROM NODE 196.00 TO NODE 197.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	120.00	DOWNSTREAM(FEET) =	110.00
FLOW LENGTH(FEET) =	135.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.4 INCHES			
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.24			
ESTIMATED PIPE DIAMETER(INCH) =		18.00	NUMBER OF PIPES = 1
PIPE-FLOW(CFS) =		17.14	
PIPE TRAVEL TIME(MIN.) =	0.14	Tc(MIN.) =	16.42
LONGEST FLOWPATH FROM NODE	192.00	TO NODE	197.00 = 1200.00 FEET.

FLOW PROCESS FROM NODE 197.00 TO NODE 197.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) =	16.42				
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	2.054				
SUBAREA LOSS RATE DATA(AMC II):					
DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	2.80	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) =		2.80	SUBAREA RUNOFF(CFS) = 4.92		
EFFECTIVE AREA(ACRES) =		12.50	AREA-AVERAGED Fm(INCH/HR) = 0.10		
AREA-AVERAGED Fp(INCH/HR) =		0.20	AREA-AVERAGED Ap = 0.50		
TOTAL AREA(ACRES) =		12.5	PEAK FLOW RATE(CFS) = 21.98		

FLOW PROCESS FROM NODE 197.00 TO NODE 198.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	110.00	DOWNSTREAM(FEET) =	100.00
FLOW LENGTH(FEET) =	50.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.2 INCHES			
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.82			
ESTIMATED PIPE DIAMETER(INCH) =		15.00	NUMBER OF PIPES = 1
PIPE-FLOW(CFS) =		21.98	
PIPE TRAVEL TIME(MIN.) =	0.03	Tc(MIN.) =	16.46
LONGEST FLOWPATH FROM NODE	192.00	TO NODE	198.00 = 1250.00 FEET.

FLOW PROCESS FROM NODE 198.00 TO NODE 198.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 16.46
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.051
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.70 0.20 0.500 75
PUBLIC PARK D 1.20 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.645
SUBAREA AREA(ACRES) = 2.90 SUBAREA RUNOFF(CFS) = 5.02
EFFECTIVE AREA(ACRES) = 15.40 AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.53
TOTAL AREA(ACRES) = 15.4 PEAK FLOW RATE(CFS) = 26.97

FLOW PROCESS FROM NODE 198.00 TO NODE 199.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 100.00 DOWNSTREAM(FEET) = 73.00
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.15
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 26.97
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 16.72
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 199.00 = 1550.00 FEET.

FLOW PROCESS FROM NODE 199.00 TO NODE 199.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 16.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.033
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 2.60 0.20 0.500 75
PUBLIC PARK D 1.30 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.617
SUBAREA AREA(ACRES) = 3.90 SUBAREA RUNOFF(CFS) = 6.70
EFFECTIVE AREA(ACRES) = 19.30 AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.55
TOTAL AREA(ACRES) = 19.3 PEAK FLOW RATE(CFS) = 33.41

FLOW PROCESS FROM NODE 199.00 TO NODE 200.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 73.00 DOWNSTREAM(FEET) = 59.00
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.53
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 33.41
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 16.90
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 200.00 = 1750.00 FEET.

FLOW PROCESS FROM NODE 200.00 TO NODE 200.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

DPHOSR

MAINLINE Tc(MIN.) = 16.90
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.020
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"5-7 DWELLINGS/ACRE"	D	2.20	0.20	0.500	75
PUBLIC PARK	D	1.20	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.624
 SUBAREA AREA(ACRES) = 3.40 SUBAREA RUNOFF(CFS) = 5.80
 EFFECTIVE AREA(ACRES) = 22.70 AREA-AVERAGED Fm(INCH/HR) = 0.11
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.56
 TOTAL AREA(ACRES) = 22.7 PEAK FLOW RATE(CFS) = 39.00

 FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 59.00 DOWNSTREAM(FEET) = 16.00
 FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.7 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 29.32
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 39.00
 PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 17.01
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 201.00 = 1950.00 FEET.

 FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 16.00 DOWNSTREAM(FEET) = 13.00
 FLOW LENGTH(FEET) = 355.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 23.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.71
 ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 39.00
 PIPE TRAVEL TIME(MIN.) = 0.68 Tc(MIN.) = 17.69
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 202.00 = 2305.00 FEET.

 FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
 =====
 MAINLINE Tc(MIN.) = 17.69
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.968
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	D	0.60	0.20	0.850	75
COMMERCIAL	D	4.90	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.182
 SUBAREA AREA(ACRES) = 5.50 SUBAREA RUNOFF(CFS) = 9.56
 EFFECTIVE AREA(ACRES) = 28.20 AREA-AVERAGED Fm(INCH/HR) = 0.10
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
 TOTAL AREA(ACRES) = 28.2 PEAK FLOW RATE(CFS) = 47.49

 FLOW PROCESS FROM NODE 202.00 TO NODE 191.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 13.00 DOWNSTREAM(FEET) = 5.50
 FLOW LENGTH(FEET) = 95.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.1 INCHES

DPHOSR

PIPE-FLOW VELOCITY(FEET/SEC.) = 21.26
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 47.49
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 17.77
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 191.00 = 2400.00 FEET.

FLOW PROCESS FROM NODE 191.00 TO NODE 191.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 17.77
RAINFALL INTENSITY(INCH/HR) = 1.96
AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 28.20
TOTAL STREAM AREA(ACRES) = 28.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 47.49

FLOW PROCESS FROM NODE 203.00 TO NODE 204.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 225.00
ELEVATION DATA: UPSTREAM(FEET) = 100.00 DOWNSTREAM(FEET) = 95.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.025
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.894
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
PUBLIC PARK D 0.70 0.20 0.850 75 9.03
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA RUNOFF(CFS) = 1.72
TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 1.72

FLOW PROCESS FROM NODE 204.00 TO NODE 205.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 95.00 DOWNSTREAM(FEET) = 90.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 155.00 CHANNEL SLOPE = 0.0323
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 2.00
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.823
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK D 1.10 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.03
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.43
AVERAGE FLOW DEPTH(FEET) = 0.49 TRAVEL TIME(MIN.) = 0.40
Tc(MIN.) = 9.43
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.63
EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.17
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.85
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.30

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.55 FLOW VELOCITY(FEET/SEC.) = 7.00
LONGEST FLOWPATH FROM NODE 203.00 TO NODE 205.00 = 380.00 FEET.

DPHOSR

FLOW PROCESS FROM NODE 205.00 TO NODE 206.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 90.00 DOWNSTREAM(FEET) = 28.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 345.00 CHANNEL SLOPE = 0.1797
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 2.00
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.757
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK D 1.50 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.04
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 14.60
AVERAGE FLOW DEPTH(FEET) = 0.45 TRAVEL TIME(MIN.) = 0.39
Tc(MIN.) = 9.82
SUBAREA AREA(ACRES) = 1.50 SUBAREA RUNOFF(CFS) = 3.49
EFFECTIVE AREA(ACRES) = 3.30 AREA-AVERAGED Fm(INCH/HR) = 0.17
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.85
TOTAL AREA(ACRES) = 3.3 PEAK FLOW RATE(CFS) = 7.68

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.50 FLOW VELOCITY(FEET/SEC.) = 15.44
LONGEST FLOWPATH FROM NODE 203.00 TO NODE 206.00 = 725.00 FEET.

FLOW PROCESS FROM NODE 206.00 TO NODE 207.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 18.00 DOWNSTREAM(FEET) = 13.00
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.91
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.68
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 9.91
LONGEST FLOWPATH FROM NODE 203.00 TO NODE 207.00 = 795.00 FEET.

FLOW PROCESS FROM NODE 207.00 TO NODE 207.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<<
=====

MAINLINE Tc(MIN.) = 9.91
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.743
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 1.90 0.20 0.100 75
PUBLIC PARK D 0.60 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.280
SUBAREA AREA(ACRES) = 2.50 SUBAREA RUNOFF(CFS) = 6.05
EFFECTIVE AREA(ACRES) = 5.80 AREA-AVERAGED Fm(INCH/HR) = 0.12
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.60
TOTAL AREA(ACRES) = 5.8 PEAK FLOW RATE(CFS) = 13.69

FLOW PROCESS FROM NODE 207.00 TO NODE 191.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 13.00 DOWNSTREAM(FEET) = 5.50
FLOW LENGTH(FEET) = 85.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.7 INCHES

DPHOSR

PIPE-FLOW VELOCITY(FEET/SEC.) = 16.29
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 13.69
 PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.00
 LONGEST FLOWPATH FROM NODE 203.00 TO NODE 191.00 = 880.00 FEET.

 FLOW PROCESS FROM NODE 191.00 TO NODE 191.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
 TIME OF CONCENTRATION(MIN.) = 10.00
 RAINFALL INTENSITY(INCH/HR) = 2.73
 AREA-AVERAGED Fm(INCH/HR) = 0.12
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.60
 EFFECTIVE STREAM AREA(ACRES) = 5.80
 TOTAL STREAM AREA(ACRES) = 5.80
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.69

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	289.91	7.46	3.229	0.20(0.07)	0.33	93.3	300.00
1	313.48	8.89	2.918	0.20(0.07)	0.33	113.0	181.00
1	313.88	8.92	2.913	0.20(0.07)	0.33	113.3	170.00
1	318.35	9.32	2.841	0.20(0.07)	0.33	118.4	186.00
1	323.65	9.88	2.748	0.20(0.07)	0.34	125.0	176.00
1	344.44	12.36	2.416	0.20(0.07)	0.34	153.1	107.00
1	346.61	12.76	2.373	0.20(0.07)	0.34	157.5	160.00
1	347.61	13.08	2.340	0.20(0.07)	0.34	160.5	151.00
1	345.33	15.90	2.092	0.20(0.07)	0.35	182.0	101.00
1	344.15	16.93	2.018	0.20(0.07)	0.35	188.9	118.00
1	343.78	17.03	2.011	0.20(0.07)	0.35	189.5	136.00
1	339.78	17.58	1.975	0.20(0.07)	0.35	191.0	146.00
1	307.16	21.81	1.745	0.20(0.07)	0.35	197.7	112.00
1	290.25	24.27	1.642	0.20(0.07)	0.36	199.6	126.00
2	47.49	17.77	1.963	0.20(0.10)	0.48	28.2	192.00
3	13.69	10.00	2.729	0.20(0.12)	0.60	5.8	203.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	335.51	7.46	3.229	0.20(0.07)	0.36	109.4	300.00
2	362.48	8.89	2.918	0.20(0.07)	0.36	132.3	181.00
3	362.95	8.92	2.913	0.20(0.07)	0.36	132.7	170.00
4	368.28	9.32	2.841	0.20(0.07)	0.36	138.6	186.00
5	374.78	9.88	2.748	0.20(0.07)	0.36	146.4	176.00
6	376.04	10.00	2.729	0.20(0.07)	0.36	148.1	203.00
7	397.56	12.36	2.416	0.20(0.07)	0.36	178.6	107.00
8	400.03	12.76	2.373	0.20(0.07)	0.36	183.5	160.00
9	401.26	13.08	2.340	0.20(0.07)	0.36	187.1	151.00
10	401.11	15.90	2.092	0.20(0.07)	0.37	213.1	101.00
11	400.69	16.93	2.018	0.20(0.07)	0.37	221.6	118.00
12	400.40	17.03	2.011	0.20(0.07)	0.37	222.3	136.00
13	396.80	17.58	1.975	0.20(0.07)	0.37	224.7	146.00
14	395.48	17.77	1.963	0.20(0.07)	0.37	225.3	192.00
15	357.63	21.81	1.745	0.20(0.08)	0.38	231.7	112.00
16	337.54	24.27	1.642	0.20(0.08)	0.38	233.6	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 401.26 Tc(MIN.) = 13.08
 EFFECTIVE AREA(ACRES) = 187.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
 TOTAL AREA(ACRES) = 233.6
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 191.00 = 8355.00 FEET.

DPHOSR

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*****
FLOW PROCESS FROM NODE 191.00 TO NODE 207.20 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 5.50 DOWNSTREAM(FEET) = 3.30
FLOW LENGTH(FEET) = 485.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 84.0 INCH PIPE IS 67.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.09
ESTIMATED PIPE DIAMETER(INCH) = 84.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 401.26
PIPE TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 13.75
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 207.20 = 8840.00 FEET.

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*****
FLOW PROCESS FROM NODE 207.20 TO NODE 208.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 3.30 DOWNSTREAM(FEET) = 2.20
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 72.0 INCH PIPE IS 58.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.20
ESTIMATED PIPE DIAMETER(INCH) = 72.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 401.26
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 13.86
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 208.00 = 8950.00 FEET.

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*****
FLOW PROCESS FROM NODE 208.00 TO NODE 208.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.86
RAINFALL INTENSITY(INCH/HR) = 2.26
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 187.10
TOTAL STREAM AREA(ACRES) = 233.60
PEAK FLOW RATE(CFS) AT CONFLUENCE = 401.26

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FLOW PROCESS FROM NODE 209.00 TO NODE 210.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 26.00 DOWNSTREAM(FEET) = 17.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.002
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.656
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS  Tc
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL            D      1.40    0.20    0.100    75   6.00
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 4.58
TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 4.58

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*****
FLOW PROCESS FROM NODE 210.00 TO NODE 211.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<
=====

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DPHOSR

UPSTREAM ELEVATION(FEET) = 17.00 DOWNSTREAM ELEVATION(FEET) = 14.00
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.16
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.41
HALFSTREET FLOOD WIDTH(FEET) = 14.21
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.88
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.18
STREET FLOW TRAVEL TIME(MIN.) = 1.56 Tc(MIN.) = 7.56
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.202

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 1.10 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 3.15
EFFECTIVE AREA(ACRES) = 2.50 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 7.16

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 15.07
FLOW VELOCITY(FEET/SEC.) = 3.00 DEPTH*VELOCITY(FT*FT/SEC.) = 1.28
LONGEST FLOWPATH FROM NODE 209.00 TO NODE 211.00 = 570.00 FEET.

FLOW PROCESS FROM NODE 211.00 TO NODE 208.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 9.00 DOWNSTREAM(FEET) = 2.20
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.50
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.16
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 7.70
LONGEST FLOWPATH FROM NODE 209.00 TO NODE 208.00 = 670.00 FEET.

FLOW PROCESS FROM NODE 208.00 TO NODE 208.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.70
RAINFALL INTENSITY(INCH/HR) = 3.17
AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 2.50
TOTAL STREAM AREA(ACRES) = 2.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.16

** CONFLUENCE DATA **
STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 335.51 8.26 3.044 0.20(0.07) 0.36 109.4 300.00

DPHOSR

1	362.48	9.69	2.778	0.20(0.07)	0.36	132.3	181.00
1	362.95	9.72	2.773	0.20(0.07)	0.36	132.7	170.00
1	368.28	10.12	2.711	0.20(0.07)	0.36	138.6	186.00
1	374.78	10.66	2.631	0.20(0.07)	0.36	146.4	176.00
1	376.04	10.78	2.613	0.20(0.07)	0.36	148.1	203.00
1	397.56	13.15	2.333	0.20(0.07)	0.36	178.6	107.00
1	400.03	13.55	2.293	0.20(0.07)	0.36	183.5	160.00
1	401.26	13.86	2.263	0.20(0.07)	0.36	187.1	151.00
1	401.11	16.68	2.035	0.20(0.07)	0.37	213.1	101.00
1	400.69	17.71	1.967	0.20(0.07)	0.37	221.6	118.00
1	400.40	17.81	1.960	0.20(0.07)	0.37	222.3	136.00
1	396.80	18.36	1.927	0.20(0.07)	0.37	224.7	146.00
1	395.48	18.55	1.915	0.20(0.07)	0.37	225.3	192.00
1	357.63	22.61	1.710	0.20(0.08)	0.38	231.7	112.00
1	337.54	25.08	1.611	0.20(0.08)	0.38	233.6	126.00
2	7.16	7.70	3.170	0.20(0.02)	0.10	2.5	209.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	332.99	7.70	3.170	0.20(0.07)	0.35	104.4	209.00
2	342.39	8.26	3.044	0.20(0.07)	0.35	111.9	300.00
3	368.75	9.69	2.778	0.20(0.07)	0.36	134.8	181.00
4	369.20	9.72	2.773	0.20(0.07)	0.36	135.2	170.00
5	374.40	10.12	2.711	0.20(0.07)	0.36	141.1	186.00
6	380.71	10.66	2.631	0.20(0.07)	0.36	148.9	176.00
7	381.94	10.78	2.613	0.20(0.07)	0.36	150.6	203.00
8	402.82	13.15	2.333	0.20(0.07)	0.36	181.1	107.00
9	405.20	13.55	2.293	0.20(0.07)	0.36	186.0	160.00
10	406.36	13.86	2.263	0.20(0.07)	0.36	189.6	151.00
11	405.69	16.68	2.035	0.20(0.07)	0.37	215.6	101.00
12	405.11	17.71	1.967	0.20(0.07)	0.37	224.1	118.00
13	404.80	17.81	1.960	0.20(0.07)	0.37	224.8	136.00
14	401.13	18.36	1.927	0.20(0.07)	0.37	227.2	146.00
15	399.78	18.55	1.915	0.20(0.07)	0.37	227.8	192.00
16	361.47	22.61	1.710	0.20(0.07)	0.37	234.2	112.00
17	341.16	25.08	1.611	0.20(0.07)	0.37	236.1	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 406.36 Tc(MIN.) = 13.86
EFFECTIVE AREA(ACRES) = 189.60 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 236.1
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 208.00 = 8950.00 FEET.

FLOW PROCESS FROM NODE 208.00 TO NODE 212.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 2.20 DOWNSTREAM(FEET) = 0.70
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 75.0 INCH PIPE IS 56.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.54
ESTIMATED PIPE DIAMETER(INCH) = 75.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 406.36
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 14.01
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 212.00 = 9100.00 FEET.

FLOW PROCESS FROM NODE 212.00 TO NODE 212.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.01
RAINFALL INTENSITY(INCH/HR) = 2.25
AREA-AVERAGED Fm(INCH/HR) = 0.07

DPHOSR

AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 189.60
TOTAL STREAM AREA(ACRES) = 236.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 406.36

FLOW PROCESS FROM NODE 213.00 TO NODE 214.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 27.00 DOWNSTREAM(FEET) = 20.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.311
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.552
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL D 0.50 0.20 0.100 75 6.31
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 1.59
TOTAL AREA(ACRES) = 0.50 PEAK FLOW RATE(CFS) = 1.59

FLOW PROCESS FROM NODE 214.00 TO NODE 215.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 20.00 DOWNSTREAM ELEVATION(FEET) = 11.50
STREET LENGTH(FEET) = 300.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020
SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.72
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 8.19
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.44
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.00
STREET FLOW TRAVEL TIME(MIN.) = 1.45 Tc(MIN.) = 7.76
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.155

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 0.80 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 2.26
EFFECTIVE AREA(ACRES) = 1.30 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 1.3 PEAK FLOW RATE(CFS) = 3.67

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.36
FLOW VELOCITY(FEET/SEC.) = 3.69 DEPTH*VELOCITY(FT*FT/SEC.) = 1.16
LONGEST FLOWPATH FROM NODE 213.00 TO NODE 215.00 = 600.00 FEET.

FLOW PROCESS FROM NODE 215.00 TO NODE 212.00 IS CODE = 31

DPHOSR

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM( FEET) = 6.50 DOWNSTREAM( FEET) = 0.70
FLOW LENGTH( FEET) = 150.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.4 INCHES
PIPE-FLOW VELOCITY( FEET/SEC.) = 8.67
ESTIMATED PIPE DIAMETER( INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW( CFS) = 3.67
PIPE TRAVEL TIME( MIN.) = 0.29 Tc( MIN.) = 8.05
LONGEST FLOWPATH FROM NODE 213.00 TO NODE 212.00 = 750.00 FEET.
  
```

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*****
FLOW PROCESS FROM NODE 212.00 TO NODE 212.00 IS CODE = 1
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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION( MIN.) = 8.05
RAINFALL INTENSITY( INCH/HR) = 3.09
AREA-AVERAGED Fm( INCH/HR) = 0.02
AREA-AVERAGED Fp( INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA( ACRES) = 1.30
TOTAL STREAM AREA( ACRES) = 1.30
PEAK FLOW RATE( CFS) AT CONFLUENCE = 3.67
  
```

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	332.99	7.86	3.133	0.20(0.07)	0.35	104.4	209.00
1	342.39	8.42	3.011	0.20(0.07)	0.35	111.9	300.00
1	368.75	9.85	2.753	0.20(0.07)	0.36	134.8	181.00
1	369.20	9.88	2.748	0.20(0.07)	0.36	135.2	170.00
1	374.40	10.27	2.687	0.20(0.07)	0.36	141.1	186.00
1	380.71	10.82	2.609	0.20(0.07)	0.36	148.9	176.00
1	381.94	10.94	2.592	0.20(0.07)	0.36	150.6	203.00
1	402.82	13.30	2.318	0.20(0.07)	0.36	181.1	107.00
1	405.20	13.70	2.279	0.20(0.07)	0.36	186.0	160.00
1	406.36	14.01	2.249	0.20(0.07)	0.36	189.6	151.00
1	405.69	16.83	2.025	0.20(0.07)	0.37	215.6	101.00
1	405.11	17.86	1.957	0.20(0.07)	0.37	224.1	118.00
1	404.80	17.97	1.951	0.20(0.07)	0.37	224.8	136.00
1	401.13	18.51	1.917	0.20(0.07)	0.37	227.2	146.00
1	399.78	18.70	1.906	0.20(0.07)	0.37	227.8	192.00
1	361.47	22.77	1.703	0.20(0.07)	0.37	234.2	112.00
1	341.16	25.24	1.606	0.20(0.07)	0.37	236.1	126.00
2	3.67	8.05	3.090	0.20(0.02)	0.10	1.3	213.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	336.61	7.86	3.133	0.20(0.07)	0.35	105.7	209.00
2	339.91	8.05	3.090	0.20(0.07)	0.35	108.3	213.00
3	345.96	8.42	3.011	0.20(0.07)	0.35	113.2	300.00
4	372.02	9.85	2.753	0.20(0.07)	0.35	136.1	181.00
5	372.46	9.88	2.748	0.20(0.07)	0.35	136.5	170.00
6	377.59	10.27	2.687	0.20(0.07)	0.35	142.4	186.00
7	383.80	10.82	2.609	0.20(0.07)	0.36	150.2	176.00
8	385.01	10.94	2.592	0.20(0.07)	0.36	151.9	203.00
9	405.56	13.30	2.318	0.20(0.07)	0.36	182.4	107.00
10	407.90	13.70	2.279	0.20(0.07)	0.36	187.3	160.00
11	409.03	14.01	2.249	0.20(0.07)	0.36	190.9	151.00
12	408.08	16.83	2.025	0.20(0.07)	0.37	216.9	101.00
13	407.43	17.86	1.957	0.20(0.07)	0.37	225.4	118.00
14	407.11	17.97	1.951	0.20(0.07)	0.37	226.1	136.00
15	403.40	18.51	1.917	0.20(0.07)	0.37	228.5	146.00
16	402.04	18.70	1.906	0.20(0.07)	0.37	229.1	192.00

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17	363.48	22.77	1.703	0.20(0.07)	0.37	235.5	112.00
18	343.05	25.24	1.606	0.20(0.07)	0.37	237.4	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 409.03 Tc(MIN.) = 14.01
 EFFECTIVE AREA(ACRES) = 190.90 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
 TOTAL AREA(ACRES) = 237.4
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 212.00 = 9100.00 FEET.

 FLOW PROCESS FROM NODE 212.00 TO NODE 213.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 0.70 DOWNSTREAM(FEET) = 0.20
 FLOW LENGTH(FEET) = 5.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 48.0 INCH PIPE IS 37.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 39.02
 ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 409.03
 PIPE TRAVEL TIME(MIN.) = 0.00 Tc(MIN.) = 14.01
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 213.00 = 9105.00 FEET.

 FLOW PROCESS FROM NODE 213.00 TO NODE 213.20 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 0.20 DOWNSTREAM(FEET) = 0.10
 FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 87.0 INCH PIPE IS 69.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 11.62
 ESTIMATED PIPE DIAMETER(INCH) = 87.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 409.03
 PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 14.05
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 213.20 = 9130.00 FEET.

 FLOW PROCESS FROM NODE 213.20 TO NODE 213.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 =====
 TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 14.05
 RAINFALL INTENSITY(INCH/HR) = 2.25
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.36
 EFFECTIVE STREAM AREA(ACRES) = 190.90
 TOTAL STREAM AREA(ACRES) = 237.40
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 409.03

 FLOW PROCESS FROM NODE 215.00 TO NODE 216.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
 =====
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 200.00
 ELEVATION DATA: UPSTREAM(FEET) = 11.80 DOWNSTREAM(FEET) = 8.90

 $Tc = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.902
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.691
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	D	0.20	0.20	0.100	75	5.90

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 0.66
TOTAL AREA(ACRES) = 0.20 PEAK FLOW RATE(CFS) = 0.66

FLOW PROCESS FROM NODE 216.00 TO NODE 217.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 3.90 DOWNSTREAM(FEET) = 2.90
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.14
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.66
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 6.00
LONGEST FLOWPATH FROM NODE 215.00 TO NODE 217.00 = 230.00 FEET.

FLOW PROCESS FROM NODE 217.00 TO NODE 217.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 6.00
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.657
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.50 SUBAREA RUNOFF(CFS) = 1.64
EFFECTIVE AREA(ACRES) = 0.70 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 0.7 PEAK FLOW RATE(CFS) = 2.29

FLOW PROCESS FROM NODE 217.00 TO NODE 213.20 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 2.90 DOWNSTREAM(FEET) = 0.10
FLOW LENGTH(FEET) = 60.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.23
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.29
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 6.12
LONGEST FLOWPATH FROM NODE 215.00 TO NODE 213.20 = 290.00 FEET.

FLOW PROCESS FROM NODE 213.20 TO NODE 213.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.12
RAINFALL INTENSITY(INCH/HR) = 3.62
AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 0.70
TOTAL STREAM AREA(ACRES) = 0.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.29

** CONFLUENCE DATA **

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
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DPHOSR							
NUMBER	(CFS)	(MIN.)	(INCH/HR)	(INCH/HR)		(ACRES)	NODE
1	336.61	7.90	3.124	0.20(0.07)	0.35	105.7	209.00
1	339.91	8.09	3.081	0.20(0.07)	0.35	108.3	213.00
1	345.96	8.46	3.003	0.20(0.07)	0.35	113.2	300.00
1	372.02	9.89	2.747	0.20(0.07)	0.35	136.1	181.00
1	372.46	9.92	2.742	0.20(0.07)	0.35	136.5	170.00
1	377.59	10.31	2.681	0.20(0.07)	0.35	142.4	186.00
1	383.80	10.85	2.604	0.20(0.07)	0.36	150.2	176.00
1	385.01	10.98	2.587	0.20(0.07)	0.36	151.9	203.00
1	405.56	13.34	2.314	0.20(0.07)	0.36	182.4	107.00
1	407.90	13.74	2.275	0.20(0.07)	0.36	187.3	160.00
1	409.03	14.05	2.246	0.20(0.07)	0.36	190.9	151.00
1	408.08	16.87	2.022	0.20(0.07)	0.37	216.9	101.00
1	407.43	17.90	1.955	0.20(0.07)	0.37	225.4	118.00
1	407.11	18.00	1.948	0.20(0.07)	0.37	226.1	136.00
1	403.40	18.55	1.915	0.20(0.07)	0.37	228.5	146.00
1	402.04	18.74	1.904	0.20(0.07)	0.37	229.1	192.00
1	363.48	22.81	1.701	0.20(0.07)	0.37	235.5	112.00
1	343.05	25.27	1.604	0.20(0.07)	0.37	237.4	126.00
2	2.29	6.12	3.615	0.20(0.02)	0.10	0.7	215.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	305.16	6.12	3.615	0.20(0.07)	0.35	82.6	215.00
2	338.59	7.90	3.124	0.20(0.07)	0.35	106.4	209.00
3	341.86	8.09	3.081	0.20(0.07)	0.35	109.0	213.00
4	347.86	8.46	3.003	0.20(0.07)	0.35	113.9	300.00
5	373.75	9.89	2.747	0.20(0.07)	0.35	136.8	181.00
6	374.20	9.92	2.742	0.20(0.07)	0.35	137.2	170.00
7	379.28	10.31	2.681	0.20(0.07)	0.35	143.1	186.00
8	385.45	10.85	2.604	0.20(0.07)	0.35	150.9	176.00
9	386.65	10.98	2.587	0.20(0.07)	0.35	152.6	203.00
10	407.03	13.34	2.314	0.20(0.07)	0.36	183.1	107.00
11	409.33	13.74	2.275	0.20(0.07)	0.36	188.0	160.00
12	410.45	14.05	2.246	0.20(0.07)	0.36	191.6	151.00
13	409.36	16.87	2.022	0.20(0.07)	0.37	217.6	101.00
14	408.66	17.90	1.955	0.20(0.07)	0.37	226.1	118.00
15	408.34	18.00	1.948	0.20(0.07)	0.37	226.8	136.00
16	404.60	18.55	1.915	0.20(0.07)	0.37	229.2	146.00
17	403.24	18.74	1.904	0.20(0.07)	0.37	229.8	192.00
18	364.56	22.81	1.701	0.20(0.07)	0.37	236.2	112.00
19	344.06	25.27	1.604	0.20(0.07)	0.37	238.1	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 410.45 Tc(MIN.) = 14.05
EFFECTIVE AREA(ACRES) = 191.60 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 238.1
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 213.20 = 9130.00 FEET.

=====
END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 238.1 TC(MIN.) = 14.05
EFFECTIVE AREA(ACRES) = 191.60 AREA-AVERAGED Fm(INCH/HR)= 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.359
PEAK FLOW RATE(CFS) = 410.45

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	305.16	6.12	3.615	0.20(0.07)	0.35	82.6	215.00
2	338.59	7.90	3.124	0.20(0.07)	0.35	106.4	209.00
3	341.86	8.09	3.081	0.20(0.07)	0.35	109.0	213.00
4	347.86	8.46	3.003	0.20(0.07)	0.35	113.9	300.00
5	373.75	9.89	2.747	0.20(0.07)	0.35	136.8	181.00
6	374.20	9.92	2.742	0.20(0.07)	0.35	137.2	170.00
7	379.28	10.31	2.681	0.20(0.07)	0.35	143.1	186.00
8	385.45	10.85	2.604	0.20(0.07)	0.35	150.9	176.00
9	386.65	10.98	2.587	0.20(0.07)	0.35	152.6	203.00
10	407.03	13.34	2.314	0.20(0.07)	0.36	183.1	107.00

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11	409.33	13.74	2.275	0.20	(0.07)	0.36	188.0	160.00
12	410.45	14.05	2.246	0.20	(0.07)	0.36	191.6	151.00
13	409.36	16.87	2.022	0.20	(0.07)	0.37	217.6	101.00
14	408.66	17.90	1.955	0.20	(0.07)	0.37	226.1	118.00
15	408.34	18.00	1.948	0.20	(0.07)	0.37	226.8	136.00
16	404.60	18.55	1.915	0.20	(0.07)	0.37	229.2	146.00
17	403.24	18.74	1.904	0.20	(0.07)	0.37	229.8	192.00
18	364.56	22.81	1.701	0.20	(0.07)	0.37	236.2	112.00
19	344.06	25.27	1.604	0.20	(0.07)	0.37	238.1	126.00

=====
 =====
 END OF RATIONAL METHOD ANALYSIS

♀

B.3

Proposed 10-Year
60" Hydrology
WI Harbor

DPHOSP2

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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Irvine, CA 92606

FILE NAME: DPHOSP2.DAT
TIME/DATE OF STUDY: 08:56 04/29/2013

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 10.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 12.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150
2	18.0	5.0	0.020/0.020/0.020	0.50	1.50 0.0313 0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.67 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 10.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

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INITIAL SUBAREA FLOW-LENGTH (FEET) = 280.00
ELEVATION DATA: UPSTREAM (FEET) = 295.00 DOWNSTREAM (FEET) = 290.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 8.288
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.039
SUBAREA T_c AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.30	0.20	0.500	75	8.29

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA RUNOFF (CFS) = 3.44
TOTAL AREA (ACRES) = 1.30 PEAK FLOW RATE (CFS) = 3.44

FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<<

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UPSTREAM ELEVATION (FEET) = 290.00 DOWNSTREAM ELEVATION (FEET) = 285.00

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STREET LENGTH(FEET) = 135.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.64
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.35
 HALFSTREET FLOOD WIDTH(FEET) = 11.43
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.66
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.65
 STREET FLOW TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 8.77
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.942

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	2.50	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 2.50		SUBAREA RUNOFF(CFS) = 6.39			
EFFECTIVE AREA(ACRES) = 3.80		AREA-AVERAGED Fm(INCH/HR) = 0.10			
AREA-AVERAGED Fp(INCH/HR) = 0.20		AREA-AVERAGED Ap = 0.50			
TOTAL AREA(ACRES) = 3.8		PEAK FLOW RATE(CFS) = 9.72			

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.35
 FLOW VELOCITY(FEET/SEC.) = 5.11 DEPTH*VELOCITY(FT*FT/SEC.) = 2.01
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 103.00 = 415.00 FEET.

 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<<
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<<

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UPSTREAM ELEVATION(FEET) = 285.00 DOWNSTREAM ELEVATION(FEET) = 253.00
 STREET LENGTH(FEET) = 345.00 CURB HEIGHT(INCHES) = 8.0
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 14.11
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.40
 HALFSTREET FLOOD WIDTH(FEET) = 13.48
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.77
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.13
 STREET FLOW TRAVEL TIME(MIN.) = 0.74 Tc(MIN.) = 9.51
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.808

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	3.60	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 3.60		SUBAREA RUNOFF(CFS) = 8.78			
EFFECTIVE AREA(ACRES) = 7.40		AREA-AVERAGED Fm(INCH/HR) = 0.10			

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AREA-AVERAGED F_p (INCH/HR) = 0.20 AREA-AVERAGED A_p = 0.50
TOTAL AREA(ACRES) = 7.4 PEAK FLOW RATE(CFS) = 18.04

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 14.96
FLOW VELOCITY(FEET/SEC.) = 8.23 DEPTH*VELOCITY(FT*FT/SEC.) = 3.54
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 104.00 = 760.00 FEET.

FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 253.00 DOWNSTREAM ELEVATION(FEET) = 225.00
STREET LENGTH(FEET) = 630.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 20.18
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.49
HALFSTREET FLOOD WIDTH(FEET) = 18.24
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.38
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.11
STREET FLOW TRAVEL TIME(MIN.) = 1.65 T_c (MIN.) = 11.16
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.563

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
RESIDENTIAL					
"5-7 DWELLINGS/ACRE"	D	0.70	0.20	0.500	75
PUBLIC PARK	D	0.10	0.20	0.850	75
COMMERCIAL	D	1.10	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.287
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 4.28
EFFECTIVE AREA(ACRES) = 9.30 AREA-AVERAGED F_m (INCH/HR) = 0.09
AREA-AVERAGED F_p (INCH/HR) = 0.20 AREA-AVERAGED A_p = 0.46
TOTAL AREA(ACRES) = 9.3 PEAK FLOW RATE(CFS) = 20.69

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.40
FLOW VELOCITY(FEET/SEC.) = 6.43 DEPTH*VELOCITY(FT*FT/SEC.) = 3.16
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 105.00 = 1390.00 FEET.

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 204.30 DOWNSTREAM(FEET) = 202.30
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.43
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 20.69
PIPE TRAVEL TIME(MIN.) = 0.02 T_c (MIN.) = 11.18
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 106.00 = 1415.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

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TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.18
RAINFALL INTENSITY(INCH/HR) = 2.56
AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.46
EFFECTIVE STREAM AREA(ACRES) = 9.30
TOTAL STREAM AREA(ACRES) = 9.30
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.69

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FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
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INITIAL SUBAREA FLOW-LENGTH(FEET) = 270.00
ELEVATION DATA: UPSTREAM(FEET) = 330.00 DOWNSTREAM(FEET) = 320.00

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Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.880
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.699
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 1.00 0.20 0.200 75 5.88
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 3.29
TOTAL AREA(ACRES) = 1.00 PEAK FLOW RATE(CFS) = 3.29

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FLOW PROCESS FROM NODE 108.00 TO NODE 109.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
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ELEVATION DATA: UPSTREAM(FEET) = 310.00 DOWNSTREAM(FEET) = 265.00
FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.15
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.29
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 6.14
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 109.00 = 505.00 FEET.

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FLOW PROCESS FROM NODE 109.00 TO NODE 109.00 IS CODE = 81
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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
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MAINLINE Tc(MIN.) = 6.14
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.609
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 3.90 0.20 0.200 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA(ACRES) = 3.90 SUBAREA RUNOFF(CFS) = 12.53
EFFECTIVE AREA(ACRES) = 4.90 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 4.9 PEAK FLOW RATE(CFS) = 15.74

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FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

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>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 265.00 DOWNSTREAM(FEET) = 258.00
FLOW LENGTH(FEET) = 560.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.94
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.74
PIPE TRAVEL TIME(MIN.) = 1.18 Tc(MIN.) = 7.31
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 110.00 = 1065.00 FEET.

FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.31
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.265
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.30 0.20 0.500 75
PUBLIC PARK D 2.10 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.716
SUBAREA AREA(ACRES) = 3.40 SUBAREA RUNOFF(CFS) = 9.55
EFFECTIVE AREA(ACRES) = 8.30 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 8.3 PEAK FLOW RATE(CFS) = 23.77

FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 258.00 DOWNSTREAM(FEET) = 238.00
FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.66
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.77
PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 7.45
LONGEST FLOWPATH FROM NODE 107.00 TO NODE 111.00 = 1240.00 FEET.

FLOW PROCESS FROM NODE 111.00 TO NODE 111.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.229
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 5.50 0.20 0.500 75
PUBLIC PARK D 0.80 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.544
SUBAREA AREA(ACRES) = 6.30 SUBAREA RUNOFF(CFS) = 17.69
EFFECTIVE AREA(ACRES) = 14.60 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 14.6 PEAK FLOW RATE(CFS) = 41.20

FLOW PROCESS FROM NODE 111.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 238.00 DOWNSTREAM(FEET) = 202.30

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FLOW LENGTH(FEET) = 235.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.0 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 26.38
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 41.20
 PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 7.60
 LONGEST FLOWPATH FROM NODE 107.00 TO NODE 106.00 = 1475.00 FEET.

 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

 TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 7.60
 RAINFALL INTENSITY(INCH/HR) = 3.19
 AREA-AVERAGED Fm(INCH/HR) = 0.09
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.47
 EFFECTIVE STREAM AREA(ACRES) = 14.60
 TOTAL STREAM AREA(ACRES) = 14.60
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 41.20

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	20.69	11.18	2.560	0.20(0.09)	0.46	9.3	101.00
2	41.20	7.60	3.193	0.20(0.09)	0.47	14.6	107.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	58.87	7.60	3.193	0.20(0.09)	0.47	20.9	107.00
2	53.47	11.18	2.560	0.20(0.09)	0.46	23.9	101.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 58.87 Tc(MIN.) = 7.60
 EFFECTIVE AREA(ACRES) = 20.92 AREA-AVERAGED Fm(INCH/HR) = 0.09
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
 TOTAL AREA(ACRES) = 23.9
 LONGEST FLOWPATH FROM NODE 107.00 TO NODE 106.00 = 1475.00 FEET.

 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

 FLOW PROCESS FROM NODE 112.00 TO NODE 113.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

 INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
 ELEVATION DATA: UPSTREAM(FEET) = 330.00 DOWNSTREAM(FEET) = 328.70

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.309
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.543
 SUBAREA Tc AND LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
 RESIDENTIAL
 "5-7 DWELLINGS/ACRE" D 1.10 0.20 0.500 75 11.31
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
 SUBAREA RUNOFF(CFS) = 2.42

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TOTAL AREA(ACRES) = 1.10 PEAK FLOW RATE(CFS) = 2.42

FLOW PROCESS FROM NODE 113.00 TO NODE 114.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

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UPSTREAM ELEVATION(FEET) = 328.70 DOWNSTREAM ELEVATION(FEET) = 327.40
STREET LENGTH(FEET) = 225.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.00
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.33
HALFSTREET FLOOD WIDTH(FEET) = 10.17
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.74
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.57
STREET FLOW TRAVEL TIME(MIN.) = 2.16 Tc(MIN.) = 13.47
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.301

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.60	0.20	0.500	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 1.60 SUBAREA RUNOFF(CFS) = 3.17
EFFECTIVE AREA(ACRES) = 2.70 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50
TOTAL AREA(ACRES) = 2.7 PEAK FLOW RATE(CFS) = 5.35

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.52
FLOW VELOCITY(FEET/SEC.) = 1.85 DEPTH*VELOCITY(FT*FT/SEC.) = 0.66
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 114.00 = 525.00 FEET.

FLOW PROCESS FROM NODE 114.00 TO NODE 115.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 312.40 DOWNSTREAM(FEET) = 310.80
FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 11.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.34
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.35
PIPE TRAVEL TIME(MIN.) = 0.56 Tc(MIN.) = 14.03
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 115.00 = 705.00 FEET.

FLOW PROCESS FROM NODE 115.00 TO NODE 115.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 14.03
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.248
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.30	0.20	0.500	75

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SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 2.51
EFFECTIVE AREA(ACRES) = 4.00 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50
TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 7.73

FLOW PROCESS FROM NODE 115.00 TO NODE 116.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 310.80 DOWNSTREAM(FEET) = 247.20
FLOW LENGTH(FEET) = 825.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.35
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.73
PIPE TRAVEL TIME(MIN.) = 1.03 Tc(MIN.) = 15.06
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 116.00 = 1530.00 FEET.

FLOW PROCESS FROM NODE 116.00 TO NODE 116.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====
MAINLINE Tc(MIN.) = 15.06
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.158
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 4.60 0.20 0.500 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.461
SUBAREA AREA(ACRES) = 5.10 SUBAREA RUNOFF(CFS) = 9.48
EFFECTIVE AREA(ACRES) = 9.10 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 9.1 PEAK FLOW RATE(CFS) = 16.89

FLOW PROCESS FROM NODE 116.00 TO NODE 117.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 247.20 DOWNSTREAM(FEET) = 234.20
FLOW LENGTH(FEET) = 765.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.16
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 16.89
PIPE TRAVEL TIME(MIN.) = 1.39 Tc(MIN.) = 16.45
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 117.00 = 2295.00 FEET.

FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====
MAINLINE Tc(MIN.) = 16.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.052
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.00 0.20 0.500 75
COMMERCIAL D 0.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.386
SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 2.49

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EFFECTIVE AREA(ACRES) = 10.50 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 10.5 PEAK FLOW RATE(CFS) = 18.51

FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 16.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.052
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 3.10 0.20 0.500 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 3.10 SUBAREA RUNOFF(CFS) = 5.44
EFFECTIVE AREA(ACRES) = 13.60 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 13.6 PEAK FLOW RATE(CFS) = 23.95

FLOW PROCESS FROM NODE 117.00 TO NODE 125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 234.20 DOWNSTREAM(FEET) = 228.00
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.99
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.95
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 16.56
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 125.00 = 2395.00 FEET.

FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.56
RAINFALL INTENSITY(INCH/HR) = 2.04
AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.47
EFFECTIVE STREAM AREA(ACRES) = 13.60
TOTAL STREAM AREA(ACRES) = 13.60
PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.95

FLOW PROCESS FROM NODE 118.00 TO NODE 119.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 275.00
ELEVATION DATA: UPSTREAM(FEET) = 336.00 DOWNSTREAM(FEET) = 328.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.463
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.227
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.70 0.20 0.500 75 7.46
PUBLIC PARK D 0.20 0.20 0.850 75 9.27
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

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SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.537
SUBAREA RUNOFF(CFS) = 5.33
TOTAL AREA(ACRES) = 1.90 PEAK FLOW RATE(CFS) = 5.33

FLOW PROCESS FROM NODE 119.00 TO NODE 120.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET)	=	328.00	DOWNSTREAM ELEVATION(FEET)	=	307.00
STREET LENGTH(FEET)	=	675.00	CURB HEIGHT(INCHES)	=	6.0
STREET HALFWIDTH(FEET)	=	18.00			

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.07
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.33
HALFSTREET FLOOD WIDTH(FEET) = 10.08
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.00
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.31
STREET FLOW TRAVEL TIME(MIN.) = 2.81 Tc(MIN.) = 10.28
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.686

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	3.20	0.20	0.500	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA AREA(ACRES) = 3.20 SUBAREA RUNOFF(CFS) = 7.45
EFFECTIVE AREA(ACRES) = 5.10 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51
TOTAL AREA(ACRES) = 5.1 PEAK FLOW RATE(CFS) = 11.86

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.34
FLOW VELOCITY(FEET/SEC.) = 4.22 DEPTH*VELOCITY(FT*FT/SEC.) = 1.49
LONGEST FLOWPATH FROM NODE 118.00 TO NODE 120.00 = 950.00 FEET.

FLOW PROCESS FROM NODE 120.00 TO NODE 121.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET)	=	307.00	DOWNSTREAM ELEVATION(FEET)	=	301.00
STREET LENGTH(FEET)	=	115.00	CURB HEIGHT(INCHES)	=	6.0
STREET HALFWIDTH(FEET)	=	18.00			

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.99
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.37
HALFSTREET FLOOD WIDTH(FEET) = 12.06
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.72
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.10

DPHOSP2

STREET FLOW TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 10.61
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.638

SUBAREA LOSS RATE DATA(AMC II):

Table with 6 columns: DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN. Rows include Residential (5-7 dwellings/acre), Public Park, and Commercial.

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.59
FLOW VELOCITY(FEET/SEC.) = 6.09 DEPTH*VELOCITY(FT*FT/SEC.) = 2.42
LONGEST FLOWPATH FROM NODE 118.00 TO NODE 121.00 = 1065.00 FEET.

FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 296.00 DOWNSTREAM(FEET) = 280.00
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.89
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.91
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 10.80
LONGEST FLOWPATH FROM NODE 118.00 TO NODE 122.00 = 1265.00 FEET.

FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 280.00 DOWNSTREAM ELEVATION(FEET) = 262.00
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 34.22

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.53
HALFSTREET FLOOD WIDTH(FEET) = 20.82
AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.42
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 4.50
STREET FLOW TRAVEL TIME(MIN.) = 0.53 Tc(MIN.) = 11.33
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.540

SUBAREA LOSS RATE DATA(AMC II):

Table with 6 columns: DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN. Rows include Residential (5-7 dwellings/acre), Public Park, and Commercial.

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EFFECTIVE AREA(ACRES) = 19.90 AREA-AVERAGED Fm(INCH/HR) = 0.10
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.52
 TOTAL AREA(ACRES) = 19.9 PEAK FLOW RATE(CFS) = 43.61

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.57 HALFSTREET FLOOD WIDTH(FEET) = 22.85
 FLOW VELOCITY(FEET/SEC.) = 8.98 DEPTH*VELOCITY(FT*FT/SEC.) = 5.12
 LONGEST FLOWPATH FROM NODE 118.00 TO NODE 123.00 = 1535.00 FEET.

 FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 262.00 DOWNSTREAM ELEVATION(FEET) = 239.00
 STREET LENGTH(FEET) = 250.00 CURB HEIGHT(INCHES) = 8.0
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 44.16
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.55
 HALFSTREET FLOOD WIDTH(FEET) = 21.60
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 10.13
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 5.55
 STREET FLOW TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 11.74
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.489

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	D	0.20	0.20	0.850	75
COMMERCIAL	D	0.30	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
 SUBAREA AREA(ACRES) = 0.50 SUBAREA RUNOFF(CFS) = 1.08
 EFFECTIVE AREA(ACRES) = 20.40 AREA-AVERAGED Fm(INCH/HR) = 0.10
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.52
 TOTAL AREA(ACRES) = 20.4 PEAK FLOW RATE(CFS) = 43.78

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.55 HALFSTREET FLOOD WIDTH(FEET) = 21.52
 FLOW VELOCITY(FEET/SEC.) = 10.11 DEPTH*VELOCITY(FT*FT/SEC.) = 5.53
 LONGEST FLOWPATH FROM NODE 118.00 TO NODE 124.00 = 1785.00 FEET.

 FLOW PROCESS FROM NODE 124.00 TO NODE 125.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 232.60 DOWNSTREAM(FEET) = 228.00
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.44
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 43.78
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 11.80
 LONGEST FLOWPATH FROM NODE 118.00 TO NODE 125.00 = 1855.00 FEET.

 FLOW PROCESS FROM NODE 125.00 TO NODE 125.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

DPHOSP2

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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 11.80
RAINFALL INTENSITY(INCH/HR) = 2.48
AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.52
EFFECTIVE STREAM AREA(ACRES) = 20.40
TOTAL STREAM AREA(ACRES) = 20.40
PEAK FLOW RATE(CFS) AT CONFLUENCE = 43.78
    
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** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	23.95	16.56	2.044	0.20(0.09)	0.47	13.6	112.00
2	43.78	11.80	2.481	0.20(0.10)	0.52	20.4	118.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	64.69	11.80	2.481	0.20(0.10)	0.51	30.1	118.00
2	59.68	16.56	2.044	0.20(0.10)	0.50	34.0	112.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

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PEAK FLOW RATE(CFS) = 64.69 Tc(MIN.) = 11.80
EFFECTIVE AREA(ACRES) = 30.10 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51
TOTAL AREA(ACRES) = 34.0
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 125.00 = 2395.00 FEET.
    
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FLOW PROCESS FROM NODE 125.00 TO NODE 132.00 IS CODE = 31
    
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
    
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ELEVATION DATA: UPSTREAM(FEET) = 228.00 DOWNSTREAM(FEET) = 224.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.10
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 64.69
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 11.84
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 132.00 = 2445.00 FEET.
    
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*****
FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1
    
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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
    
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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.84
RAINFALL INTENSITY(INCH/HR) = 2.48
AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.51
EFFECTIVE STREAM AREA(ACRES) = 30.10
TOTAL STREAM AREA(ACRES) = 34.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 64.69
    
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*****
FLOW PROCESS FROM NODE 126.00 TO NODE 127.00 IS CODE = 21
    
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
    
```

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=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 322.00 DOWNSTREAM(FEET) = 320.50
    
```

DPHOSP2

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.589
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.977

SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 0.40 0.20 0.200 75 9.15
COMMERCIAL D 0.20 0.20 0.100 75 8.59
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.167
SUBAREA RUNOFF(CFS) = 1.59
TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.59

FLOW PROCESS FROM NODE 127.00 TO NODE 128.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 320.50 DOWNSTREAM ELEVATION(FEET) = 318.00
STREET LENGTH(FEET) = 600.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.65
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.77
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.60
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.63
STREET FLOW TRAVEL TIME(MIN.) = 6.23 Tc(MIN.) = 14.82
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.178

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.40 0.20 0.500 75
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 0.20 0.20 0.200 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.264
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.10
EFFECTIVE AREA(ACRES) = 1.70 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.23
TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 3.26

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.02
FLOW VELOCITY(FEET/SEC.) = 1.67 DEPTH*VELOCITY(FT*FT/SEC.) = 0.69
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 128.00 = 900.00 FEET.

FLOW PROCESS FROM NODE 128.00 TO NODE 129.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 318.00 DOWNSTREAM ELEVATION(FEET) = 302.00
STREET LENGTH(FEET) = 640.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.75
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.42
HALFSTREET FLOOD WIDTH(FEET) = 14.57
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.19
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.77
STREET FLOW TRAVEL TIME(MIN.) = 2.55 Tc(MIN.) = 17.37
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.989

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 5.50 0.20 0.500 75
COMMERCIAL D 0.90 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.444
SUBAREA AREA(ACRES) = 6.40 SUBAREA RUNOFF(CFS) = 10.94
EFFECTIVE AREA(ACRES) = 8.10 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 8.1 PEAK FLOW RATE(CFS) = 13.92

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 17.62
FLOW VELOCITY(FEET/SEC.) = 4.69 DEPTH*VELOCITY(FT*FT/SEC.) = 2.24
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 129.00 = 1540.00 FEET.

FLOW PROCESS FROM NODE 129.00 TO NODE 130.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 302.00 DOWNSTREAM ELEVATION(FEET) = 264.00
STREET LENGTH(FEET) = 450.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 19.54
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.45
HALFSTREET FLOOD WIDTH(FEET) = 15.82
AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.05
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.58
STREET FLOW TRAVEL TIME(MIN.) = 0.93 Tc(MIN.) = 18.30
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.930

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 6.10 0.20 0.500 75
COMMERCIAL D 0.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.459
SUBAREA AREA(ACRES) = 6.80 SUBAREA RUNOFF(CFS) = 11.25
EFFECTIVE AREA(ACRES) = 14.90 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.43
TOTAL AREA(ACRES) = 14.9 PEAK FLOW RATE(CFS) = 24.74

DPHOSP2

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 17.38
FLOW VELOCITY(FEET/SEC.) = 8.55 DEPTH*VELOCITY(FT*FT/SEC.) = 4.05
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 130.00 = 1990.00 FEET.

FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 264.00 DOWNSTREAM ELEVATION(FEET) = 242.00
STREET LENGTH(FEET) = 310.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALfstREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 25.08
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.49
HALFSTREET FLOOD WIDTH(FEET) = 18.09
AVERAGE FLOW VELOCITY(FEET/SEC.) = 8.05
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.91
STREET FLOW TRAVEL TIME(MIN.) = 0.64 Tc(MIN.) = 18.95
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.892

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 0.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.67
EFFECTIVE AREA(ACRES) = 15.30 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 15.3 PEAK FLOW RATE(CFS) = 24.91

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.09
FLOW VELOCITY(FEET/SEC.) = 8.00 DEPTH*VELOCITY(FT*FT/SEC.) = 3.88
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 131.00 = 2300.00 FEET.

FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 237.10 DOWNSTREAM(FEET) = 224.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 28.36
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 24.91
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 18.97
LONGEST FLOWPATH FROM NODE 126.00 TO NODE 132.00 = 2350.00 FEET.

FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 18.97

DPHOSP2

3	136.01	12.21	2.434	0.20(0.10)	0.48	63.5	118.00
4	124.96	16.97	2.016	0.20(0.09)	0.47	71.3	112.00
5	118.45	19.35	1.870	0.20(0.09)	0.47	73.2	126.00
TOTAL AREA(ACRES) =			73.2				

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 136.01 Tc(MIN.) = 12.212
EFFECTIVE AREA(ACRES) = 63.54 AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
TOTAL AREA(ACRES) = 73.2
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 106.00 = 2890.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 135.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 202.30 DOWNSTREAM(FEET) = 141.50
FLOW LENGTH(FEET) = 1090.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.96
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 136.01
PIPE TRAVEL TIME(MIN.) = 0.76 Tc(MIN.) = 12.97
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 135.00 = 3980.00 FEET.

FLOW PROCESS FROM NODE 135.00 TO NODE 135.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 12.97
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.351
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	D	5.70	0.20	0.400	75
COMMERCIAL	D	0.60	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.371
SUBAREA AREA(ACRES) = 6.30 SUBAREA RUNOFF(CFS) = 12.91
EFFECTIVE AREA(ACRES) = 69.84 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47
TOTAL AREA(ACRES) = 79.5 PEAK FLOW RATE(CFS) = 141.91

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	136.87	8.37	3.023	0.20(0.09)	0.46	51.9	107.00
2	141.96	11.94	2.465	0.20(0.09)	0.47	66.5	101.00
3	141.91	12.97	2.351	0.20(0.09)	0.47	69.8	118.00
4	130.72	17.73	1.965	0.20(0.09)	0.47	77.6	112.00
5	124.06	20.15	1.827	0.20(0.09)	0.46	79.5	126.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE(CFS) = 141.96 Tc(MIN.) = 11.94
AREA-AVERAGED Fm(INCH/HR) = 0.09 AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.47 EFFECTIVE AREA(ACRES) = 66.50

FLOW PROCESS FROM NODE 135.00 TO NODE 144.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 141.50 DOWNSTREAM(FEET) = 141.00
FLOW LENGTH(FEET) = 15.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 31.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.65
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 141.96
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 11.95

DPHOSP2
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 144.00 = 3995.00 FEET.

FLOW PROCESS FROM NODE 144.00 TO NODE 144.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.95
RAINFALL INTENSITY(INCH/HR) = 2.46
AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.47
EFFECTIVE STREAM AREA(ACRES) = 66.50
TOTAL STREAM AREA(ACRES) = 79.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 141.96

FLOW PROCESS FROM NODE 136.00 TO NODE 137.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 230.00
ELEVATION DATA: UPSTREAM(FEET) = 335.00 DOWNSTREAM(FEET) = 332.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.794
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.405
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 3.20 0.20 0.200 75 6.79
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 9.69
TOTAL AREA(ACRES) = 3.20 PEAK FLOW RATE(CFS) = 9.69

FLOW PROCESS FROM NODE 137.00 TO NODE 138.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 332.00 DOWNSTREAM ELEVATION(FEET) = 308.00
STREET LENGTH(FEET) = 575.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.16
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.42
HALFSTREET FLOOD WIDTH(FEET) = 14.76
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.73
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.42
STREET FLOW TRAVEL TIME(MIN.) = 1.67 Tc(MIN.) = 8.47
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.002
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 2.60 0.20 0.200 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

DPHOSP2

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA(ACRES) = 2.60 SUBAREA RUNOFF(CFS) = 6.93
EFFECTIVE AREA(ACRES) = 5.80 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 5.8 PEAK FLOW RATE(CFS) = 15.46

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 15.70
FLOW VELOCITY(FEET/SEC.) = 5.99 DEPTH*VELOCITY(FT*FT/SEC.) = 2.64
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 138.00 = 805.00 FEET.

FLOW PROCESS FROM NODE 138.00 TO NODE 139.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 308.00 DOWNSTREAM ELEVATION(FEET) = 280.00
STREET LENGTH(FEET) = 440.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 22.35
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.48
HALFSTREET FLOOD WIDTH(FEET) = 17.70
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.47
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.58
STREET FLOW TRAVEL TIME(MIN.) = 0.98 Tc(MIN.) = 9.45
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.819

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"11+ DWELLINGS/ACRE" D 4.80 0.20 0.200 75
COMMERCIAL D 0.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.187
SUBAREA AREA(ACRES) = 5.50 SUBAREA RUNOFF(CFS) = 13.77
EFFECTIVE AREA(ACRES) = 11.30 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.19
TOTAL AREA(ACRES) = 11.3 PEAK FLOW RATE(CFS) = 28.28

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.51 HALFSTREET FLOOD WIDTH(FEET) = 19.41
FLOW VELOCITY(FEET/SEC.) = 7.94 DEPTH*VELOCITY(FT*FT/SEC.) = 4.05
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 139.00 = 1245.00 FEET.

FLOW PROCESS FROM NODE 139.00 TO NODE 140.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 280.00 DOWNSTREAM ELEVATION(FEET) = 255.00
STREET LENGTH(FEET) = 425.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

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Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 29.69
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.52
HALFSTREET FLOOD WIDTH(FEET) = 20.12
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.80
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 4.07
STREET FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 10.36
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.675

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.50 0.20 0.500 75
COMMERCIAL D 0.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.267
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 2.83
EFFECTIVE AREA(ACRES) = 12.50 AREA-AVERAGED Fm(INCH/HR) = 0.04
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 12.5 PEAK FLOW RATE(CFS) = 29.64

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.52 HALFSTREET FLOOD WIDTH(FEET) = 20.12
FLOW VELOCITY(FEET/SEC.) = 7.78 DEPTH*VELOCITY(FT*FT/SEC.) = 4.06
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 140.00 = 1670.00 FEET.

FLOW PROCESS FROM NODE 140.00 TO NODE 141.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 257.00 DOWNSTREAM(FEET) = 250.00
FLOW LENGTH(FEET) = 95.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.50
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 29.64
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.44
LONGEST FLOWPATH FROM NODE 136.00 TO NODE 141.00 = 1765.00 FEET.

FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 250.00 DOWNSTREAM ELEVATION(FEET) = 160.00
STREET LENGTH(FEET) = 1225.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 41.58
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.56
HALFSTREET FLOOD WIDTH(FEET) = 21.99
AVERAGE FLOW VELOCITY(FEET/SEC.) = 9.21
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 5.12
STREET FLOW TRAVEL TIME(MIN.) = 2.22 Tc(MIN.) = 12.66
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.384

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN

DPHOSP2

RESIDENTIAL

"8-10 DWELLINGS/ACRE" D 11.20 0.20 0.400 75
 COMMERCIAL D 0.30 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.392
 SUBAREA AREA(ACRES) = 11.50 SUBAREA RUNOFF(CFS) = 23.86
 EFFECTIVE AREA(ACRES) = 24.00 AREA-AVERAGED Fm(INCH/HR) = 0.06
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.29
 TOTAL AREA(ACRES) = 24.0 PEAK FLOW RATE(CFS) = 50.23

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.59 HALFSTREET FLOOD WIDTH(FEET) = 23.71
 FLOW VELOCITY(FEET/SEC.) = 9.63 DEPTH*VELOCITY(FT*FT/SEC.) = 5.65
 LONGEST FLOWPATH FROM NODE 136.00 TO NODE 142.00 = 2990.00 FEET.

 FLOW PROCESS FROM NODE 142.00 TO NODE 143.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 150.00 DOWNSTREAM(FEET) = 145.00
 FLOW LENGTH(FEET) = 285.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.9 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 11.97
 ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 50.23
 PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 13.05
 LONGEST FLOWPATH FROM NODE 136.00 TO NODE 143.00 = 3275.00 FEET.

 FLOW PROCESS FROM NODE 143.00 TO NODE 143.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 13.05
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.342
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 RESIDENTIAL
 "8-10 DWELLINGS/ACRE" D 5.60 0.20 0.400 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
 SUBAREA AREA(ACRES) = 5.60 SUBAREA RUNOFF(CFS) = 11.40
 EFFECTIVE AREA(ACRES) = 29.60 AREA-AVERAGED Fm(INCH/HR) = 0.06
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.31
 TOTAL AREA(ACRES) = 29.6 PEAK FLOW RATE(CFS) = 60.73

 FLOW PROCESS FROM NODE 143.00 TO NODE 144.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 145.00 DOWNSTREAM(FEET) = 141.00
 FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.7 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 23.17
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 60.73
 PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 13.09
 LONGEST FLOWPATH FROM NODE 136.00 TO NODE 144.00 = 3320.00 FEET.

 FLOW PROCESS FROM NODE 144.00 TO NODE 144.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 13.09

DPHOSP2

RAINFALL INTENSITY(INCH/HR) = 2.34
AREA-AVERAGED Fm(INCH/HR) = 0.06
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.31
EFFECTIVE STREAM AREA(ACRES) = 29.60
TOTAL STREAM AREA(ACRES) = 29.60
PEAK FLOW RATE(CFS) AT CONFLUENCE = 60.73

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 6 rows of data for different stream nodes.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 6 rows of data for different stream nodes.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 202.44 Tc(MIN.) = 12.98
EFFECTIVE AREA(ACRES) = 99.21 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 109.1
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 144.00 = 3995.00 FEET.

FLOW PROCESS FROM NODE 144.00 TO NODE 145.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 141.00 DOWNSTREAM(FEET) = 139.00
FLOW LENGTH(FEET) = 325.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 63.0 INCH PIPE IS 47.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.57
ESTIMATED PIPE DIAMETER(INCH) = 63.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 202.44
PIPE TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 13.45
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 145.00 = 4320.00 FEET.

FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 13.45
RAINFALL INTENSITY(INCH/HR) = 2.30
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.42
EFFECTIVE STREAM AREA(ACRES) = 99.21
TOTAL STREAM AREA(ACRES) = 109.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 202.44

FLOW PROCESS FROM NODE 146.00 TO NODE 147.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

DPHOSP2

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 270.00
ELEVATION DATA: UPSTREAM(FEET) = 218.00 DOWNSTREAM(FEET) = 216.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.364
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.833
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.20 0.20 0.400 75 9.36
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA RUNOFF(CFS) = 2.97
TOTAL AREA(ACRES) = 1.20 PEAK FLOW RATE(CFS) = 2.97

FLOW PROCESS FROM NODE 147.00 TO NODE 148.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 216.00 DOWNSTREAM ELEVATION(FEET) = 210.00
STREET LENGTH(FEET) = 405.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.50
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.38
HALFSTREET FLOOD WIDTH(FEET) = 12.78
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.14
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.20
STREET FLOW TRAVEL TIME(MIN.) = 2.15 Tc(MIN.) = 11.51
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.517

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 2.30 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 2.30 SUBAREA RUNOFF(CFS) = 5.05
EFFECTIVE AREA(ACRES) = 3.50 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 7.68

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.60
FLOW VELOCITY(FEET/SEC.) = 3.41 DEPTH*VELOCITY(FT*FT/SEC.) = 1.43
LONGEST FLOWPATH FROM NODE 146.00 TO NODE 148.00 = 675.00 FEET.

FLOW PROCESS FROM NODE 148.00 TO NODE 149.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 210.00 DOWNSTREAM ELEVATION(FEET) = 175.00
STREET LENGTH(FEET) = 475.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.64
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.61
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.58
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.36
STREET FLOW TRAVEL TIME(MIN.) = 1.20 Tc(MIN.) = 12.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.378

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.90 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 3.93
EFFECTIVE AREA(ACRES) = 5.40 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 5.4 PEAK FLOW RATE(CFS) = 11.17

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.33
FLOW VELOCITY(FEET/SEC.) = 6.82 DEPTH*VELOCITY(FT*FT/SEC.) = 2.54
LONGEST FLOWPATH FROM NODE 146.00 TO NODE 149.00 = 1150.00 FEET.

FLOW PROCESS FROM NODE 149.00 TO NODE 149.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 12.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.378
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.50 0.20 0.400 75
COMMERCIAL D 1.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.255
SUBAREA AREA(ACRES) = 2.90 SUBAREA RUNOFF(CFS) = 6.07
EFFECTIVE AREA(ACRES) = 8.30 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA(ACRES) = 8.3 PEAK FLOW RATE(CFS) = 17.24

FLOW PROCESS FROM NODE 149.00 TO NODE 145.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 175.00 DOWNSTREAM ELEVATION(FEET) = 146.00
STREET LENGTH(FEET) = 580.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 25.63

DPHOSP2

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.51
 HALFSTREET FLOOD WIDTH(FEET) = 19.65
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.04
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.61
 STREET FLOW TRAVEL TIME(MIN.) = 1.37 Tc(MIN.) = 14.09
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.242
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 RESIDENTIAL
 "8-10 DWELLINGS/ACRE" D 7.90 0.20 0.400 75
 COMMERCIAL D 0.70 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.376
 SUBAREA AREA(ACRES) = 8.60 SUBAREA RUNOFF(CFS) = 16.77
 EFFECTIVE AREA(ACRES) = 16.90 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
 TOTAL AREA(ACRES) = 16.9 PEAK FLOW RATE(CFS) = 33.00

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.55 HALFSTREET FLOOD WIDTH(FEET) = 21.68
 FLOW VELOCITY(FEET/SEC.) = 7.52 DEPTH*VELOCITY(FT*FT/SEC.) = 4.13
 LONGEST FLOWPATH FROM NODE 146.00 TO NODE 145.00 = 1730.00 FEET.

 FLOW PROCESS FROM NODE 145.00 TO NODE 145.00 IS CODE = 1

 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
 =====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 14.09
 RAINFALL INTENSITY(INCH/HR) = 2.24
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.36
 EFFECTIVE STREAM AREA(ACRES) = 16.90
 TOTAL STREAM AREA(ACRES) = 16.90
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 33.00

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	187.38	8.86	2.925	0.20(0.08)	0.42	70.9	107.00
1	200.47	12.42	2.410	0.20(0.08)	0.42	93.5	101.00
1	202.44	13.45	2.302	0.20(0.08)	0.42	99.2	118.00
1	202.40	13.56	2.292	0.20(0.08)	0.42	99.6	136.00
1	181.46	18.23	1.934	0.20(0.08)	0.42	107.2	112.00
1	171.11	20.65	1.801	0.20(0.08)	0.42	109.1	126.00
2	33.00	14.09	2.242	0.20(0.07)	0.36	16.9	146.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	214.67	8.86	2.925	0.20(0.08)	0.42	81.5	107.00
2	231.81	12.42	2.410	0.20(0.08)	0.41	108.4	101.00
3	234.82	13.45	2.302	0.20(0.08)	0.41	115.3	118.00
4	234.88	13.56	2.292	0.20(0.08)	0.41	115.9	136.00
5	233.01	14.09	2.242	0.20(0.08)	0.41	117.4	146.00
6	209.78	18.23	1.934	0.20(0.08)	0.41	124.1	112.00
7	197.40	20.65	1.801	0.20(0.08)	0.41	126.0	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 234.88 Tc(MIN.) = 13.56
 EFFECTIVE AREA(ACRES) = 115.87 AREA-AVERAGED Fm(INCH/HR) = 0.08
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
 TOTAL AREA(ACRES) = 126.0
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 145.00 = 4320.00 FEET.

DPHOSP2

 FLOW PROCESS FROM NODE 145.00 TO NODE 150.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 139.00 DOWNSTREAM(FEET) = 125.00
 FLOW LENGTH(FEET) = 780.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 54.0 INCH PIPE IS 41.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 17.87
 ESTIMATED PIPE DIAMETER(INCH) = 54.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 234.88
 PIPE TRAVEL TIME(MIN.) = 0.73 Tc(MIN.) = 14.28
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 150.00 = 5100.00 FEET.

 FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 14.28
 RAINFALL INTENSITY(INCH/HR) = 2.22
 AREA-AVERAGED Fm(INCH/HR) = 0.08
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.41
 EFFECTIVE STREAM AREA(ACRES) = 115.87
 TOTAL STREAM AREA(ACRES) = 126.00
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 234.88

 FLOW PROCESS FROM NODE 151.00 TO NODE 152.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
 ELEVATION DATA: UPSTREAM(FEET) = 235.00 DOWNSTREAM(FEET) = 230.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.751
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.418
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	D	0.30	0.20	0.850	75	10.73
COMMERCIAL	D	0.30	0.20	0.100	75	6.75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.475
 SUBAREA RUNOFF(CFS) = 1.79
 TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.79

 FLOW PROCESS FROM NODE 152.00 TO NODE 153.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 230.00 DOWNSTREAM ELEVATION(FEET) = 195.00
 STREET LENGTH(FEET) = 390.00 CURB HEIGHT(INCHES) = 8.0
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.018
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

DPHOSP2

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.02
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 6.22
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.61
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.53
STREET FLOW TRAVEL TIME(MIN.) = 1.16 Tc(MIN.) = 7.91
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.121

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK D 0.40 0.20 0.850 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.433
SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 2.46
EFFECTIVE AREA(ACRES) = 1.50 AREA-AVERAGED Fm(INCH/HR) = 0.09
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.45
TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 4.09

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 7.47
FLOW VELOCITY(FEET/SEC.) = 5.91 DEPTH*VELOCITY(FT*FT/SEC.) = 1.75
LONGEST FLOWPATH FROM NODE 151.00 TO NODE 153.00 = 690.00 FEET.

FLOW PROCESS FROM NODE 153.00 TO NODE 154.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 195.00 DOWNSTREAM ELEVATION(FEET) = 180.00
STREET LENGTH(FEET) = 275.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.88
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.88
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.81
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 2.11
STREET FLOW TRAVEL TIME(MIN.) = 0.79 Tc(MIN.) = 8.70
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.956

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 3.70 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 3.70 SUBAREA RUNOFF(CFS) = 9.58
EFFECTIVE AREA(ACRES) = 5.20 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 5.2 PEAK FLOW RATE(CFS) = 13.45

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.13
FLOW VELOCITY(FEET/SEC.) = 6.36 DEPTH*VELOCITY(FT*FT/SEC.) = 2.60
LONGEST FLOWPATH FROM NODE 151.00 TO NODE 154.00 = 965.00 FEET.

FLOW PROCESS FROM NODE 154.00 TO NODE 155.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
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>>>>(STREET TABLE SECTION # 2 USED)<<<<

UPSTREAM ELEVATION(FEET) = 180.00 DOWNSTREAM ELEVATION(FEET) = 175.00
STREET LENGTH(FEET) = 125.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 21.04
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.48
HALFSTREET FLOOD WIDTH(FEET) = 17.88
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.35
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.07
STREET FLOW TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 9.03
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.894

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 6.00 0.20 0.400 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 6.00 SUBAREA RUNOFF(CFS) = 15.19
EFFECTIVE AREA(ACRES) = 11.20 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41
TOTAL AREA(ACRES) = 11.2 PEAK FLOW RATE(CFS) = 28.35

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.00
FLOW VELOCITY(FEET/SEC.) = 6.35 DEPTH*VELOCITY(FT*FT/SEC.) = 3.09
LONGEST FLOWPATH FROM NODE 151.00 TO NODE 155.00 = 1090.00 FEET.

FLOW PROCESS FROM NODE 155.00 TO NODE 156.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<

UPSTREAM ELEVATION(FEET) = 175.00 DOWNSTREAM ELEVATION(FEET) = 139.00
STREET LENGTH(FEET) = 570.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 41.26
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.45
HALFSTREET FLOOD WIDTH(FEET) = 16.24
AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.48
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 3.38
STREET FLOW TRAVEL TIME(MIN.) = 1.27 Tc(MIN.) = 10.30
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.684

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 3.90 0.20 0.400 75
RESIDENTIAL

DPHOSP2

"11+ DWELLINGS/ACRE" D 6.20 0.20 0.200 75
 COMMERCIAL D 0.80 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.264
 SUBAREA AREA(ACRES) = 10.90 SUBAREA RUNOFF(CFS) = 25.81
 EFFECTIVE AREA(ACRES) = 22.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.34
 TOTAL AREA(ACRES) = 22.1 PEAK FLOW RATE(CFS) = 52.04

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 17.80
 FLOW VELOCITY(FEET/SEC.) = 7.91 DEPTH*VELOCITY(FT*FT/SEC.) = 3.82
 LONGEST FLOWPATH FROM NODE 151.00 TO NODE 156.00 = 1660.00 FEET.

 FLOW PROCESS FROM NODE 156.00 TO NODE 150.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 133.50 DOWNSTREAM(FEET) = 125.00
 FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 31.62
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 52.04
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 10.32
 LONGEST FLOWPATH FROM NODE 151.00 TO NODE 150.00 = 1700.00 FEET.

 FLOW PROCESS FROM NODE 150.00 TO NODE 150.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
 =====
 TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 10.32
 RAINFALL INTENSITY(INCH/HR) = 2.68
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.34
 EFFECTIVE STREAM AREA(ACRES) = 22.10
 TOTAL STREAM AREA(ACRES) = 22.10
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 52.04

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	214.67	9.60	2.794	0.20(0.08)	0.42	81.5	107.00
1	231.81	13.15	2.333	0.20(0.08)	0.41	108.4	101.00
1	234.82	14.18	2.234	0.20(0.08)	0.41	115.3	118.00
1	234.88	14.28	2.225	0.20(0.08)	0.41	115.9	136.00
1	233.01	14.82	2.178	0.20(0.08)	0.41	117.4	146.00
1	209.78	18.98	1.890	0.20(0.08)	0.41	124.1	112.00
1	197.40	21.40	1.765	0.20(0.08)	0.41	126.0	126.00
2	52.04	10.32	2.680	0.20(0.07)	0.34	22.1	151.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	265.17	9.60	2.794	0.20(0.08)	0.40	102.0	107.00
2	270.18	10.32	2.680	0.20(0.08)	0.40	109.0	151.00
3	276.92	13.15	2.333	0.20(0.08)	0.40	130.5	101.00
4	277.97	14.18	2.234	0.20(0.08)	0.40	137.4	118.00
5	277.84	14.28	2.225	0.20(0.08)	0.40	138.0	136.00
6	275.04	14.82	2.178	0.20(0.08)	0.40	139.5	146.00
7	246.08	18.98	1.890	0.20(0.08)	0.40	146.2	112.00
8	231.20	21.40	1.765	0.20(0.08)	0.40	148.1	126.00

DPHOSP2

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 277.97 Tc(MIN.) = 14.18
EFFECTIVE AREA(ACRES) = 137.44 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.40
TOTAL AREA(ACRES) = 148.1
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 150.00 = 5100.00 FEET.

FLOW PROCESS FROM NODE 150.00 TO NODE 159.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 125.00 DOWNSTREAM(FEET) = 102.00
FLOW LENGTH(FEET) = 610.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 51.0 INCH PIPE IS 37.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.79
ESTIMATED PIPE DIAMETER(INCH) = 51.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 277.97
PIPE TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 14.59
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 159.00 = 5710.00 FEET.

FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 14.59
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.198
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 5.10 0.20 0.400 75
COMMERCIAL D 3.30 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.282
SUBAREA AREA(ACRES) = 8.40 SUBAREA RUNOFF(CFS) = 16.19
EFFECTIVE AREA(ACRES) = 145.84 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.39
TOTAL AREA(ACRES) = 156.5 PEAK FLOW RATE(CFS) = 278.14

FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.59
RAINFALL INTENSITY(INCH/HR) = 2.20
AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.39
EFFECTIVE STREAM AREA(ACRES) = 145.84
TOTAL STREAM AREA(ACRES) = 156.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 278.14

FLOW PROCESS FROM NODE 160.00 TO NODE 161.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 260.00
ELEVATION DATA: UPSTREAM(FEET) = 145.00 DOWNSTREAM(FEET) = 143.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.441
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.232
SUBAREA Tc AND LOSS RATE DATA(AMC II):

Table with 7 columns: DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN, Tc (MIN.).

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COMMERCIAL D 0.50 0.20 0.100 75 7.44
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 1.45
TOTAL AREA(ACRES) = 0.50 PEAK FLOW RATE(CFS) = 1.45

FLOW PROCESS FROM NODE 161.00 TO NODE 162.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====

UPSTREAM ELEVATION(FEET) = 143.00 DOWNSTREAM ELEVATION(FEET) = 138.00
STREET LENGTH(FEET) = 345.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.018
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.018

SPECIFIED NUMBER OF HALfstREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.58
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 11.05
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.79
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.00
STREET FLOW TRAVEL TIME(MIN.) = 2.06 Tc(MIN.) = 9.50
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.810

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 1.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 4.27
EFFECTIVE AREA(ACRES) = 2.20 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 5.52

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.40
FLOW VELOCITY(FEET/SEC.) = 3.07 DEPTH*VELOCITY(FT*FT/SEC.) = 1.24
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 162.00 = 605.00 FEET.

FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE Tc(MIN.) = 9.50
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.810
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 2.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.50 SUBAREA RUNOFF(CFS) = 6.28
EFFECTIVE AREA(ACRES) = 4.70 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 4.7 PEAK FLOW RATE(CFS) = 11.80

FLOW PROCESS FROM NODE 162.00 TO NODE 163.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

DPHOSP2

ELEVATION DATA: UPSTREAM(FEET) = 132.00 DOWNSTREAM(FEET) = 127.00
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.77
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.80
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 9.60
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 163.00 = 685.00 FEET.

FLOW PROCESS FROM NODE 163.00 TO NODE 163.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 9.60
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.793
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 1.70 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 4.24
EFFECTIVE AREA(ACRES) = 6.40 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 6.4 PEAK FLOW RATE(CFS) = 15.97

FLOW PROCESS FROM NODE 163.00 TO NODE 164.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 127.00 DOWNSTREAM(FEET) = 117.50
FLOW LENGTH(FEET) = 350.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.59
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.97
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 10.15
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 164.00 = 1035.00 FEET.

FLOW PROCESS FROM NODE 164.00 TO NODE 164.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.15
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.706
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"8-10 DWELLINGS/ACRE" D 1.40 0.20 0.400 75
COMMERCIAL D 0.50 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.321
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 4.52
EFFECTIVE AREA(ACRES) = 8.30 AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.15
TOTAL AREA(ACRES) = 8.3 PEAK FLOW RATE(CFS) = 19.99

FLOW PROCESS FROM NODE 164.00 TO NODE 165.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 117.50 DOWNSTREAM(FEET) = 114.50
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.78
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

DPHOSP2

PIPE-FLOW(CFS) = 19.99
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 10.18
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 165.00 = 1070.00 FEET.

FLOW PROCESS FROM NODE 165.00 TO NODE 165.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.18
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.701
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 2.20 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 5.31
EFFECTIVE AREA(ACRES) = 10.50 AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.14
TOTAL AREA(ACRES) = 10.5 PEAK FLOW RATE(CFS) = 25.26

FLOW PROCESS FROM NODE 165.00 TO NODE 159.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 114.50 DOWNSTREAM(FEET) = 102.00
FLOW LENGTH(FEET) = 220.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.14
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 25.26
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 10.41
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 159.00 = 1290.00 FEET.

FLOW PROCESS FROM NODE 159.00 TO NODE 159.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.41
RAINFALL INTENSITY(INCH/HR) = 2.67
AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.14
EFFECTIVE STREAM AREA(ACRES) = 10.50
TOTAL STREAM AREA(ACRES) = 10.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 25.26

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists data for 2 streams and their 11 contributing nodes.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE.

DPHOSP2

1	290.01	10.01	2.727	0.20(0.07)	0.37	120.5	107.00
2	293.22	10.41	2.667	0.20(0.07)	0.37	124.9	160.00
3	295.00	10.73	2.621	0.20(0.07)	0.37	127.9	151.00
4	298.59	13.56	2.292	0.20(0.08)	0.38	149.4	101.00
5	298.90	14.59	2.198	0.20(0.08)	0.38	156.3	118.00
6	298.65	14.69	2.189	0.20(0.08)	0.38	156.9	136.00
7	295.30	15.23	2.144	0.20(0.08)	0.38	158.4	146.00
8	266.20	19.41	1.866	0.20(0.08)	0.38	165.1	112.00
9	250.98	21.83	1.745	0.20(0.08)	0.38	167.0	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 298.90 Tc(MIN.) = 14.59
EFFECTIVE AREA(ACRES) = 156.34 AREA-AVERAGED Fm(INCH/HR) = 0.08
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.38
TOTAL AREA(ACRES) = 167.0
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 159.00 = 5710.00 FEET.

FLOW PROCESS FROM NODE 159.00 TO NODE 168.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 102.00 DOWNSTREAM(FEET) = 94.30
FLOW LENGTH(FEET) = 1005.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 69.0 INCH PIPE IS 53.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.76
ESTIMATED PIPE DIAMETER(INCH) = 69.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 298.90
PIPE TRAVEL TIME(MIN.) = 1.22 Tc(MIN.) = 15.81
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 168.00 = 6715.00 FEET.

FLOW PROCESS FROM NODE 168.00 TO NODE 168.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 15.81
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.099
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	7.50	0.20	0.100	75
PUBLIC PARK	D	0.20	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.119
SUBAREA AREA(ACRES) = 7.70 SUBAREA RUNOFF(CFS) = 14.38
EFFECTIVE AREA(ACRES) = 164.04 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.37
TOTAL AREA(ACRES) = 174.7 PEAK FLOW RATE(CFS) = 299.14

FLOW PROCESS FROM NODE 168.00 TO NODE 169.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 94.30 DOWNSTREAM(FEET) = 93.50
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 75.0 INCH PIPE IS 56.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.09
ESTIMATED PIPE DIAMETER(INCH) = 75.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 299.14
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 16.01
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 169.00 = 6865.00 FEET.

FLOW PROCESS FROM NODE 169.00 TO NODE 169.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

DPHOSP2

TIME OF CONCENTRATION(MIN.) = 16.01
RAINFALL INTENSITY(INCH/HR) = 2.08
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.37
EFFECTIVE STREAM AREA(ACRES) = 164.04
TOTAL STREAM AREA(ACRES) = 174.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 299.14

FLOW PROCESS FROM NODE 170.00 TO NODE 171.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 145.00 DOWNSTREAM(FEET) = 140.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.751
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.418

SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL D 0.90 0.20 0.100 75 6.75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 2.75
TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 2.75

FLOW PROCESS FROM NODE 171.00 TO NODE 172.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 130.00 DOWNSTREAM(FEET) = 128.00
FLOW LENGTH(FEET) = 265.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 9.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.24
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.75
PIPE TRAVEL TIME(MIN.) = 1.04 Tc(MIN.) = 7.79
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 172.00 = 565.00 FEET.

FLOW PROCESS FROM NODE 172.00 TO NODE 172.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 7.79
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.148
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 3.10 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 3.10 SUBAREA RUNOFF(CFS) = 8.73
EFFECTIVE AREA(ACRES) = 4.00 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 11.26

FLOW PROCESS FROM NODE 172.00 TO NODE 169.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 128.00 DOWNSTREAM(FEET) = 93.50
FLOW LENGTH(FEET) = 215.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.28

DPHOSP2

ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.26
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 7.98
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 169.00 = 780.00 FEET.

FLOW PROCESS FROM NODE 169.00 TO NODE 169.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.98
RAINFALL INTENSITY(INCH/HR) = 3.11
AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 4.00
TOTAL STREAM AREA(ACRES) = 4.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.26

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 15 rows of data for stream 1 and 2.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 10 rows of data for streams 1 through 10.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 306.67 Tc(MIN.) = 16.01
EFFECTIVE AREA(ACRES) = 168.04 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 178.7
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 169.00 = 6865.00 FEET.

FLOW PROCESS FROM NODE 169.00 TO NODE 173.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 93.50 DOWNSTREAM(FEET) = 91.80
FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 66.0 INCH PIPE IS 53.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.86
ESTIMATED PIPE DIAMETER(INCH) = 66.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 306.67
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 16.22

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DPHOSP2
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 173.00 = 7045.00 FEET.
*****
FLOW PROCESS FROM NODE 173.00 TO NODE 173.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.22
RAINFALL INTENSITY(INCH/HR) = 2.07
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 168.04
TOTAL STREAM AREA(ACRES) = 178.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 306.67
*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 500.00
ELEVATION DATA: UPSTREAM(FEET) = 140.00 DOWNSTREAM(FEET) = 115.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.648
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.448
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL D 0.70 0.20 0.100 75 6.65
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.60 0.20 0.500 75 8.51
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.285
SUBAREA RUNOFF(CFS) = 3.97
TOTAL AREA(ACRES) = 1.30 PEAK FLOW RATE(CFS) = 3.97
*****
FLOW PROCESS FROM NODE 301.00 TO NODE 173.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 100.00 DOWNSTREAM(FEET) = 91.80
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.10
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.97
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 6.70
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 173.00 = 550.00 FEET.
*****
FLOW PROCESS FROM NODE 173.00 TO NODE 173.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.70
RAINFALL INTENSITY(INCH/HR) = 3.43
AREA-AVERAGED Fm(INCH/HR) = 0.06
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.28
EFFECTIVE STREAM AREA(ACRES) = 1.30
TOTAL STREAM AREA(ACRES) = 1.30
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.97

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DPHOSP2

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	261.23	8.19	3.060	0.20(0.07)	0.34	93.4	170.00
1	299.16	11.64	2.501	0.20(0.07)	0.35	132.2	107.00
1	302.19	12.04	2.453	0.20(0.07)	0.35	136.6	160.00
1	303.83	12.36	2.417	0.20(0.07)	0.35	139.6	151.00
1	306.41	15.19	2.148	0.20(0.07)	0.36	161.1	101.00
1	306.67	16.22	2.069	0.20(0.07)	0.36	168.0	118.00
1	306.44	16.32	2.061	0.20(0.07)	0.36	168.6	136.00
1	303.14	16.86	2.023	0.20(0.07)	0.36	170.1	146.00
1	274.98	21.08	1.780	0.20(0.07)	0.36	176.8	112.00
1	260.07	23.52	1.672	0.20(0.07)	0.36	178.7	126.00
2	3.97	6.70	3.432	0.20(0.06)	0.28	1.3	300.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	244.42	6.70	3.432	0.20(0.07)	0.34	77.8	300.00
2	264.76	8.19	3.060	0.20(0.07)	0.34	94.7	170.00
3	302.03	11.64	2.501	0.20(0.07)	0.35	133.5	107.00
4	305.01	12.04	2.453	0.20(0.07)	0.35	137.9	160.00
5	306.61	12.36	2.417	0.20(0.07)	0.35	140.9	151.00
6	308.87	15.19	2.148	0.20(0.07)	0.36	162.4	101.00
7	309.04	16.22	2.069	0.20(0.07)	0.36	169.3	118.00
8	308.80	16.32	2.061	0.20(0.07)	0.36	169.9	136.00
9	305.45	16.86	2.023	0.20(0.07)	0.36	171.4	146.00
10	277.00	21.08	1.780	0.20(0.07)	0.36	178.1	112.00
11	261.96	23.52	1.672	0.20(0.07)	0.36	180.0	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 309.04 Tc(MIN.) = 16.22
EFFECTIVE AREA(ACRES) = 169.34 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 180.0
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 173.00 = 7045.00 FEET.

FLOW PROCESS FROM NODE 173.00 TO NODE 175.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 91.80 DOWNSTREAM(FEET) = 74.40
FLOW LENGTH(FEET) = 470.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 54.0 INCH PIPE IS 38.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 25.38
ESTIMATED PIPE DIAMETER(INCH) = 54.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 309.04
PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 16.52
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 175.00 = 7515.00 FEET.

FLOW PROCESS FROM NODE 175.00 TO NODE 175.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.52
RAINFALL INTENSITY(INCH/HR) = 2.05
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 169.34
TOTAL STREAM AREA(ACRES) = 180.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 309.04

DPHOSP2

FLOW PROCESS FROM NODE 176.00 TO NODE 177.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 125.00 DOWNSTREAM(FEET) = 120.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.994
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.102
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
CONDOMINIUMS D 0.90 0.20 0.350 75 7.99
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA RUNOFF(CFS) = 2.46
TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 2.46

FLOW PROCESS FROM NODE 177.00 TO NODE 178.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 110.00 DOWNSTREAM(FEET) = 105.00
FLOW LENGTH(FEET) = 290.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.79
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.46
PIPE TRAVEL TIME(MIN.) = 0.84 Tc(MIN.) = 8.83
LONGEST FLOWPATH FROM NODE 176.00 TO NODE 178.00 = 590.00 FEET.

FLOW PROCESS FROM NODE 178.00 TO NODE 178.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.83
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.931
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
CONDOMINIUMS D 1.50 0.20 0.350 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA AREA(ACRES) = 1.50 SUBAREA RUNOFF(CFS) = 3.86
EFFECTIVE AREA(ACRES) = 2.40 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 6.18

FLOW PROCESS FROM NODE 178.00 TO NODE 179.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 105.00 DOWNSTREAM(FEET) = 80.00
FLOW LENGTH(FEET) = 390.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.86
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.18
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 9.38
LONGEST FLOWPATH FROM NODE 176.00 TO NODE 179.00 = 980.00 FEET.

FLOW PROCESS FROM NODE 179.00 TO NODE 179.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

DPHOSP2

MAINLINE Tc(MIN.) = 9.38
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.831
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 CONDOMINIUMS D 3.00 0.20 0.350 75
 RESIDENTIAL
 "11+ DWELLINGS/ACRE" D 0.20 0.20 0.200 75
 PUBLIC PARK D 0.40 0.20 0.850 75
 COMMERCIAL D 0.90 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.338
 SUBAREA AREA(ACRES) = 4.50 SUBAREA RUNOFF(CFS) = 11.19
 EFFECTIVE AREA(ACRES) = 6.90 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.34
 TOTAL AREA(ACRES) = 6.9 PEAK FLOW RATE(CFS) = 17.16

FLOW PROCESS FROM NODE 179.00 TO NODE 175.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 80.00 DOWNSTREAM(FEET) = 74.40
 FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 15.89
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 17.16
 PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 9.46
 LONGEST FLOWPATH FROM NODE 176.00 TO NODE 175.00 = 1060.00 FEET.

FLOW PROCESS FROM NODE 175.00 TO NODE 175.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 9.46
 RAINFALL INTENSITY(INCH/HR) = 2.82
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.34
 EFFECTIVE STREAM AREA(ACRES) = 6.90
 TOTAL STREAM AREA(ACRES) = 6.90
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.16

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	244.42	7.03	3.339	0.20(0.07)	0.34	77.8	300.00
1	264.76	8.51	2.994	0.20(0.07)	0.34	94.7	170.00
1	302.03	11.96	2.463	0.20(0.07)	0.35	133.5	107.00
1	305.01	12.36	2.417	0.20(0.07)	0.35	137.9	160.00
1	306.61	12.67	2.383	0.20(0.07)	0.35	140.9	151.00
1	308.87	15.50	2.123	0.20(0.07)	0.36	162.4	101.00
1	309.04	16.52	2.046	0.20(0.07)	0.36	169.3	118.00
1	308.80	16.63	2.039	0.20(0.07)	0.36	169.9	136.00
1	305.45	17.17	2.002	0.20(0.07)	0.36	171.4	146.00
1	277.00	21.40	1.765	0.20(0.07)	0.36	178.1	112.00
1	261.96	23.85	1.658	0.20(0.07)	0.36	180.0	126.00
2	17.16	9.46	2.817	0.20(0.07)	0.34	6.9	176.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	259.59	7.03	3.339	0.20(0.07)	0.34	82.9	300.00
2	281.18	8.51	2.994	0.20(0.07)	0.34	100.9	170.00

DPHOSP2

3	292.22	9.46	2.817	0.20(0.07)	0.34	112.3	176.00
4	316.98	11.96	2.463	0.20(0.07)	0.35	140.4	107.00
5	319.67	12.36	2.417	0.20(0.07)	0.35	144.8	160.00
6	321.05	12.67	2.383	0.20(0.07)	0.35	147.8	151.00
7	321.70	15.50	2.123	0.20(0.07)	0.36	169.3	101.00
8	321.39	16.52	2.046	0.20(0.07)	0.36	176.2	118.00
9	321.10	16.63	2.039	0.20(0.07)	0.36	176.8	136.00
10	317.52	17.17	2.002	0.20(0.07)	0.36	178.3	146.00
11	287.59	21.40	1.765	0.20(0.07)	0.36	185.0	112.00
12	271.89	23.85	1.658	0.20(0.07)	0.36	186.9	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 321.70 Tc(MIN.) = 15.50
EFFECTIVE AREA(ACRES) = 169.33 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 186.9
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 175.00 = 7515.00 FEET.

FLOW PROCESS FROM NODE 175.00 TO NODE 180.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 74.40 DOWNSTREAM(FEET) = 51.60
FLOW LENGTH(FEET) = 270.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 45.0 INCH PIPE IS 35.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.38
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 321.70
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 15.63
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 180.00 = 7785.00 FEET.

FLOW PROCESS FROM NODE 180.00 TO NODE 180.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 15.63
RAINFALL INTENSITY(INCH/HR) = 2.11
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 169.33
TOTAL STREAM AREA(ACRES) = 186.90
PEAK FLOW RATE(CFS) AT CONFLUENCE = 321.70

FLOW PROCESS FROM NODE 181.00 TO NODE 182.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 125.00 DOWNSTREAM(FEET) = 120.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.994
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.102
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
CONDOMINIUMS	D	1.10	0.20	0.350	75	7.99

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA RUNOFF(CFS) = 3.00
TOTAL AREA(ACRES) = 1.10 PEAK FLOW RATE(CFS) = 3.00

FLOW PROCESS FROM NODE 182.00 TO NODE 183.00 IS CODE = 31

DPHOSP2

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 110.00 DOWNSTREAM(FEET) = 105.00
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.34
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.00
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 8.11
LONGEST FLOWPATH FROM NODE 181.00 TO NODE 183.00 = 370.00 FEET.

FLOW PROCESS FROM NODE 183.00 TO NODE 183.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.11
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.078
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
CONDOMINIUMS D 2.00 0.20 0.350 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.350
SUBAREA AREA(ACRES) = 2.00 SUBAREA RUNOFF(CFS) = 5.41
EFFECTIVE AREA(ACRES) = 3.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 8.39

FLOW PROCESS FROM NODE 183.00 TO NODE 184.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 105.00 DOWNSTREAM(FEET) = 60.00
FLOW LENGTH(FEET) = 415.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.57
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.39
PIPE TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 8.55
LONGEST FLOWPATH FROM NODE 181.00 TO NODE 184.00 = 785.00 FEET.

FLOW PROCESS FROM NODE 184.00 TO NODE 184.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.55
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.985
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
CONDOMINIUMS D 3.10 0.20 0.350 75
COMMERCIAL D 0.40 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.321
SUBAREA AREA(ACRES) = 3.50 SUBAREA RUNOFF(CFS) = 9.20
EFFECTIVE AREA(ACRES) = 6.60 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.33
TOTAL AREA(ACRES) = 6.6 PEAK FLOW RATE(CFS) = 17.33

FLOW PROCESS FROM NODE 184.00 TO NODE 180.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 60.00 DOWNSTREAM(FEET) = 51.60
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013

DPHOSP2

DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 19.29
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 17.33
 PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 8.61
 LONGEST FLOWPATH FROM NODE 181.00 TO NODE 180.00 = 855.00 FEET.

 FLOW PROCESS FROM NODE 180.00 TO NODE 180.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 8.61
 RAINFALL INTENSITY(INCH/HR) = 2.97
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.33
 EFFECTIVE STREAM AREA(ACRES) = 6.60
 TOTAL STREAM AREA(ACRES) = 6.60
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.33

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	259.59	7.17	3.302	0.20(0.07)	0.34	82.9	300.00
1	281.18	8.64	2.967	0.20(0.07)	0.34	100.9	170.00
1	292.22	9.59	2.795	0.20(0.07)	0.34	112.3	176.00
1	316.98	12.09	2.448	0.20(0.07)	0.35	140.4	107.00
1	319.67	12.49	2.402	0.20(0.07)	0.35	144.8	160.00
1	321.05	12.80	2.369	0.20(0.07)	0.35	147.8	151.00
1	321.70	15.63	2.113	0.20(0.07)	0.36	169.3	101.00
1	321.39	16.65	2.037	0.20(0.07)	0.36	176.2	118.00
1	321.10	16.76	2.030	0.20(0.07)	0.36	176.8	136.00
1	317.52	17.30	1.993	0.20(0.07)	0.36	178.3	146.00
1	287.59	21.53	1.759	0.20(0.07)	0.36	185.0	112.00
1	271.89	23.98	1.653	0.20(0.07)	0.36	186.9	126.00
2	17.33	8.61	2.973	0.20(0.07)	0.33	6.6	181.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	275.66	7.17	3.302	0.20(0.07)	0.34	88.4	300.00
2	298.10	8.61	2.973	0.20(0.07)	0.34	107.2	181.00
3	298.48	8.64	2.967	0.20(0.07)	0.34	107.5	170.00
4	308.49	9.59	2.795	0.20(0.07)	0.34	118.9	176.00
5	331.18	12.09	2.448	0.20(0.07)	0.35	147.0	107.00
6	333.60	12.49	2.402	0.20(0.07)	0.35	151.4	160.00
7	334.78	12.80	2.369	0.20(0.07)	0.35	154.4	151.00
8	333.90	15.63	2.113	0.20(0.07)	0.35	175.9	101.00
9	333.14	16.65	2.037	0.20(0.07)	0.36	182.8	118.00
10	332.81	16.76	2.030	0.20(0.07)	0.36	183.4	136.00
11	329.01	17.30	1.993	0.20(0.07)	0.36	184.9	146.00
12	297.68	21.53	1.759	0.20(0.07)	0.36	191.6	112.00
13	281.35	23.98	1.653	0.20(0.07)	0.36	193.5	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 334.78 Tc(MIN.) = 12.80
 EFFECTIVE AREA(ACRES) = 154.45 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.35
 TOTAL AREA(ACRES) = 193.5
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 180.00 = 7785.00 FEET.

 FLOW PROCESS FROM NODE 180.00 TO NODE 185.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

DPHOSP2

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ELEVATION DATA: UPSTREAM(FEET) = 51.60 DOWNSTREAM(FEET) = 46.80
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 45.0 INCH PIPE IS 36.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.98
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 334.78
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 12.83
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 185.00 = 7840.00 FEET.

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FLOW PROCESS FROM NODE 185.00 TO NODE 185.00 IS CODE = 1
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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
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TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.83
RAINFALL INTENSITY(INCH/HR) = 2.37
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.35
EFFECTIVE STREAM AREA(ACRES) = 154.45
TOTAL STREAM AREA(ACRES) = 193.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 334.78

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FLOW PROCESS FROM NODE 186.00 TO NODE 187.00 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
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INITIAL SUBAREA FLOW-LENGTH(FEET) = 260.00
ELEVATION DATA: UPSTREAM(FEET) = 120.00 DOWNSTREAM(FEET) = 115.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.195
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.590
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap      SCS      Tc
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL            D      0.60    0.20    0.100    75    6.20
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 1.93
TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 1.93

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FLOW PROCESS FROM NODE 187.00 TO NODE 188.00 IS CODE = 62
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>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<
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UPSTREAM ELEVATION(FEET) = 115.00 DOWNSTREAM ELEVATION(FEET) = 105.00
STREET LENGTH(FEET) = 365.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

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**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.42
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.28
HALFSTREET FLOOD WIDTH(FEET) = 7.56
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.20
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.89
STREET FLOW TRAVEL TIME(MIN.) = 1.90 Tc(MIN.) = 8.10

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DPHOSP2

* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.080
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 COMMERCIAL D 1.80 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 1.80 SUBAREA RUNOFF(CFS) = 4.96
 EFFECTIVE AREA(ACRES) = 2.40 AREA-AVERAGED Fm(INCH/HR) = 0.02
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 6.61

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 9.09
 FLOW VELOCITY(FEET/SEC.) = 3.50 DEPTH*VELOCITY(FT*FT/SEC.) = 1.08
 LONGEST FLOWPATH FROM NODE 186.00 TO NODE 188.00 = 625.00 FEET.

FLOW PROCESS FROM NODE 188.00 TO NODE 189.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 2 USED)<<<<<

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UPSTREAM ELEVATION(FEET) = 105.00 DOWNSTREAM ELEVATION(FEET) = 70.00
 STREET LENGTH(FEET) = 360.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.35
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.30
 HALFSTREET FLOOD WIDTH(FEET) = 8.64
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.56
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.96
 STREET FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 9.01
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.896

SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 PUBLIC PARK D 0.70 0.20 0.850 75
 COMMERCIAL D 3.00 0.20 0.100 75
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.242
 SUBAREA AREA(ACRES) = 3.70 SUBAREA RUNOFF(CFS) = 9.48
 EFFECTIVE AREA(ACRES) = 6.10 AREA-AVERAGED Fm(INCH/HR) = 0.04
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.19
 TOTAL AREA(ACRES) = 6.1 PEAK FLOW RATE(CFS) = 15.70

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 9.99
 FLOW VELOCITY(FEET/SEC.) = 7.03 DEPTH*VELOCITY(FT*FT/SEC.) = 2.29
 LONGEST FLOWPATH FROM NODE 186.00 TO NODE 189.00 = 985.00 FEET.

FLOW PROCESS FROM NODE 189.00 TO NODE 185.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 60.00 DOWNSTREAM(FEET) = 46.80
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 8.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 22.58
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 15.70

DPHOSP2
 PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 9.06
 LONGEST FLOWPATH FROM NODE 186.00 TO NODE 185.00 = 1055.00 FEET.

 FLOW PROCESS FROM NODE 185.00 TO NODE 185.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 9.06
 RAINFALL INTENSITY(INCH/HR) = 2.89
 AREA-AVERAGED Fm(INCH/HR) = 0.04
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.19
 EFFECTIVE STREAM AREA(ACRES) = 6.10
 TOTAL STREAM AREA(ACRES) = 6.10
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.70

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	275.66	7.20	3.295	0.20(0.07)	0.34	88.4	300.00
1	298.10	8.64	2.968	0.20(0.07)	0.34	107.2	181.00
1	298.48	8.67	2.962	0.20(0.07)	0.34	107.5	170.00
1	308.49	9.62	2.790	0.20(0.07)	0.34	118.9	176.00
1	331.18	12.12	2.445	0.20(0.07)	0.35	147.0	107.00
1	333.60	12.52	2.399	0.20(0.07)	0.35	151.4	160.00
1	334.78	12.83	2.366	0.20(0.07)	0.35	154.4	151.00
1	333.90	15.65	2.111	0.20(0.07)	0.35	175.9	101.00
1	333.14	16.68	2.035	0.20(0.07)	0.36	182.8	118.00
1	332.81	16.79	2.028	0.20(0.07)	0.36	183.4	136.00
1	329.01	17.33	1.991	0.20(0.07)	0.36	184.9	146.00
1	297.68	21.56	1.757	0.20(0.07)	0.36	191.6	112.00
1	281.35	24.01	1.652	0.20(0.07)	0.36	193.5	126.00
2	15.70	9.06	2.887	0.20(0.04)	0.19	6.1	186.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	289.91	7.20	3.295	0.20(0.07)	0.33	93.3	300.00
2	313.48	8.64	2.968	0.20(0.07)	0.33	113.0	181.00
3	313.88	8.67	2.962	0.20(0.07)	0.33	113.3	170.00
4	318.35	9.06	2.887	0.20(0.07)	0.33	118.4	186.00
5	323.65	9.62	2.790	0.20(0.07)	0.34	125.0	176.00
6	344.44	12.12	2.445	0.20(0.07)	0.34	153.1	107.00
7	346.61	12.52	2.399	0.20(0.07)	0.34	157.5	160.00
8	347.61	12.83	2.366	0.20(0.07)	0.34	160.5	151.00
9	345.33	15.65	2.111	0.20(0.07)	0.35	182.0	101.00
10	344.15	16.68	2.035	0.20(0.07)	0.35	188.9	118.00
11	343.78	16.79	2.028	0.20(0.07)	0.35	189.5	136.00
12	339.78	17.33	1.991	0.20(0.07)	0.35	191.0	146.00
13	307.16	21.56	1.757	0.20(0.07)	0.35	197.7	112.00
14	290.25	24.01	1.652	0.20(0.07)	0.36	199.6	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 347.61 Tc(MIN.) = 12.83
 EFFECTIVE AREA(ACRES) = 160.55 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.34
 TOTAL AREA(ACRES) = 199.6
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 185.00 = 7840.00 FEET.

 FLOW PROCESS FROM NODE 185.00 TO NODE 191.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 46.80 DOWNSTREAM(FEET) = 5.50

DPHOSP2

FLOW LENGTH(FEET) = 515.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 48.0 INCH PIPE IS 35.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 34.76
 ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 347.61
 PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 13.08
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 191.00 = 8355.00 FEET.

 FLOW PROCESS FROM NODE 191.00 TO NODE 191.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 13.08
 RAINFALL INTENSITY(INCH/HR) = 2.34
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.34
 EFFECTIVE STREAM AREA(ACRES) = 160.55
 TOTAL STREAM AREA(ACRES) = 199.60
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 347.61

 FLOW PROCESS FROM NODE 192.00 TO NODE 193.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 280.00
 ELEVATION DATA: UPSTREAM(FEET) = 142.00 DOWNSTREAM(FEET) = 140.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.955
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.736
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	0.70	0.20	0.500	75	9.95

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
 SUBAREA RUNOFF(CFS) = 1.66
 TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 1.66

 FLOW PROCESS FROM NODE 193.00 TO NODE 194.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 140.00 DOWNSTREAM ELEVATION(FEET) = 138.00
 STREET LENGTH(FEET) = 320.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.07
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.30
 HALFSTREET FLOOD WIDTH(FEET) = 8.91
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.68
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.51
 STREET FLOW TRAVEL TIME(MIN.) = 3.17 Tc(MIN.) = 13.12
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.335

DPHOSP2

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.40	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 2.82					
EFFECTIVE AREA(ACRES) = 2.10 AREA-AVERAGED Fm(INCH/HR) = 0.10					
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50					
TOTAL AREA(ACRES) = 2.1 PEAK FLOW RATE(CFS) = 4.22					

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.26
 FLOW VELOCITY(FEET/SEC.) = 1.80 DEPTH*VELOCITY(FT*FT/SEC.) = 0.60
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 194.00 = 600.00 FEET.

FLOW PROCESS FROM NODE 194.00 TO NODE 195.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 138.00 DOWNSTREAM ELEVATION(FEET) = 135.00
 STREET LENGTH(FEET) = 415.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 5.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.86
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
 STREET FLOW DEPTH(FEET) = 0.38
 HALFSTREET FLOOD WIDTH(FEET) = 12.87
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.22
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.85
 STREET FLOW TRAVEL TIME(MIN.) = 3.12 Tc(MIN.) = 16.25
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.066

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	4.10	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 4.10 SUBAREA RUNOFF(CFS) = 7.26					
EFFECTIVE AREA(ACRES) = 6.20 AREA-AVERAGED Fm(INCH/HR) = 0.10					
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50					
TOTAL AREA(ACRES) = 6.2 PEAK FLOW RATE(CFS) = 10.97					

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.76
 FLOW VELOCITY(FEET/SEC.) = 2.39 DEPTH*VELOCITY(FT*FT/SEC.) = 1.01
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 195.00 = 1015.00 FEET.

FLOW PROCESS FROM NODE 195.00 TO NODE 196.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 130.00 DOWNSTREAM(FEET) = 120.00
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 20.98
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 10.97

DPHOSP2
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 16.29
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 196.00 = 1065.00 FEET.

FLOW PROCESS FROM NODE 196.00 TO NODE 196.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) =	16.29				
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	2.064				
SUBAREA LOSS RATE DATA(AMC II):					
DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	3.50	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 3.50		SUBAREA RUNOFF(CFS) = 6.19			
EFFECTIVE AREA(ACRES) = 9.70		AREA-AVERAGED Fm(INCH/HR) = 0.10			
AREA-AVERAGED Fp(INCH/HR) = 0.20		AREA-AVERAGED Ap = 0.50			
TOTAL AREA(ACRES) = 9.7		PEAK FLOW RATE(CFS) = 17.14			

FLOW PROCESS FROM NODE 196.00 TO NODE 197.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	120.00	DOWNSTREAM(FEET) =	110.00
FLOW LENGTH(FEET) =	135.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.4 INCHES			
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.24			
ESTIMATED PIPE DIAMETER(INCH) = 18.00		NUMBER OF PIPES = 1	
PIPE-FLOW(CFS) = 17.14			
PIPE TRAVEL TIME(MIN.) =	0.14	Tc(MIN.) =	16.42
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 197.00 =	1200.00 FEET.		

FLOW PROCESS FROM NODE 197.00 TO NODE 197.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) =	16.42				
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =	2.054				
SUBAREA LOSS RATE DATA(AMC II):					
DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	2.80	0.20	0.500	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500					
SUBAREA AREA(ACRES) = 2.80		SUBAREA RUNOFF(CFS) = 4.92			
EFFECTIVE AREA(ACRES) = 12.50		AREA-AVERAGED Fm(INCH/HR) = 0.10			
AREA-AVERAGED Fp(INCH/HR) = 0.20		AREA-AVERAGED Ap = 0.50			
TOTAL AREA(ACRES) = 12.5		PEAK FLOW RATE(CFS) = 21.98			

FLOW PROCESS FROM NODE 197.00 TO NODE 198.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	110.00	DOWNSTREAM(FEET) =	100.00
FLOW LENGTH(FEET) =	50.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.2 INCHES			
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.82			
ESTIMATED PIPE DIAMETER(INCH) = 15.00		NUMBER OF PIPES = 1	
PIPE-FLOW(CFS) = 21.98			
PIPE TRAVEL TIME(MIN.) =	0.03	Tc(MIN.) =	16.46
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 198.00 =	1250.00 FEET.		

FLOW PROCESS FROM NODE 198.00 TO NODE 198.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 16.46
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.051
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 1.70 0.20 0.500 75
PUBLIC PARK D 1.20 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.645
SUBAREA AREA(ACRES) = 2.90 SUBAREA RUNOFF(CFS) = 5.02
EFFECTIVE AREA(ACRES) = 15.40 AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.53
TOTAL AREA(ACRES) = 15.4 PEAK FLOW RATE(CFS) = 26.97

FLOW PROCESS FROM NODE 198.00 TO NODE 199.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 100.00 DOWNSTREAM(FEET) = 73.00
FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.15
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 26.97
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 16.72
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 199.00 = 1550.00 FEET.

FLOW PROCESS FROM NODE 199.00 TO NODE 199.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 16.72
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.033
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 2.60 0.20 0.500 75
PUBLIC PARK D 1.30 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.617
SUBAREA AREA(ACRES) = 3.90 SUBAREA RUNOFF(CFS) = 6.70
EFFECTIVE AREA(ACRES) = 19.30 AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.55
TOTAL AREA(ACRES) = 19.3 PEAK FLOW RATE(CFS) = 33.41

FLOW PROCESS FROM NODE 199.00 TO NODE 200.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 73.00 DOWNSTREAM(FEET) = 59.00
FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.53
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 33.41
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 16.90
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 200.00 = 1750.00 FEET.

FLOW PROCESS FROM NODE 200.00 TO NODE 200.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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MAINLINE Tc(MIN.) = 16.90
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.020
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"5-7 DWELLINGS/ACRE"	D	2.20	0.20	0.500	75
PUBLIC PARK	D	1.20	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.624
 SUBAREA AREA(ACRES) = 3.40 SUBAREA RUNOFF(CFS) = 5.80
 EFFECTIVE AREA(ACRES) = 22.70 AREA-AVERAGED Fm(INCH/HR) = 0.11
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.56
 TOTAL AREA(ACRES) = 22.7 PEAK FLOW RATE(CFS) = 39.00

 FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 59.00 DOWNSTREAM(FEET) = 16.00
 FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.7 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 29.32
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 39.00
 PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 17.01
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 201.00 = 1950.00 FEET.

 FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 16.00 DOWNSTREAM(FEET) = 13.00
 FLOW LENGTH(FEET) = 355.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 23.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.71
 ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 39.00
 PIPE TRAVEL TIME(MIN.) = 0.68 Tc(MIN.) = 17.69
 LONGEST FLOWPATH FROM NODE 192.00 TO NODE 202.00 = 2305.00 FEET.

 FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
 =====
 MAINLINE Tc(MIN.) = 17.69
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.968
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	D	0.60	0.20	0.850	75
COMMERCIAL	D	4.90	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.182
 SUBAREA AREA(ACRES) = 5.50 SUBAREA RUNOFF(CFS) = 9.56
 EFFECTIVE AREA(ACRES) = 28.20 AREA-AVERAGED Fm(INCH/HR) = 0.10
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.48
 TOTAL AREA(ACRES) = 28.2 PEAK FLOW RATE(CFS) = 47.49

 FLOW PROCESS FROM NODE 202.00 TO NODE 191.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 13.00 DOWNSTREAM(FEET) = 5.50
 FLOW LENGTH(FEET) = 95.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.1 INCHES

DPHOSP2

PIPE-FLOW VELOCITY(FEET/SEC.) = 21.26
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 47.49
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 17.77
LONGEST FLOWPATH FROM NODE 192.00 TO NODE 191.00 = 2400.00 FEET.

FLOW PROCESS FROM NODE 191.00 TO NODE 191.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 17.77
RAINFALL INTENSITY(INCH/HR) = 1.96
AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.48
EFFECTIVE STREAM AREA(ACRES) = 28.20
TOTAL STREAM AREA(ACRES) = 28.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 47.49

FLOW PROCESS FROM NODE 203.00 TO NODE 204.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 225.00
ELEVATION DATA: UPSTREAM(FEET) = 100.00 DOWNSTREAM(FEET) = 95.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.025
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.894
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
PUBLIC PARK D 0.70 0.20 0.850 75 9.03
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA RUNOFF(CFS) = 1.72
TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 1.72

FLOW PROCESS FROM NODE 204.00 TO NODE 205.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 95.00 DOWNSTREAM(FEET) = 90.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 155.00 CHANNEL SLOPE = 0.0323
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 2.00
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.823

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK D 1.10 0.20 0.850 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.03
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.43
AVERAGE FLOW DEPTH(FEET) = 0.49 TRAVEL TIME(MIN.) = 0.40
Tc(MIN.) = 9.43
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 2.63
EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.17
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.85
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.30

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.55 FLOW VELOCITY(FEET/SEC.) = 7.00
LONGEST FLOWPATH FROM NODE 203.00 TO NODE 205.00 = 380.00 FEET.

DPHOSP2

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*****
FLOW PROCESS FROM NODE    205.00 TO NODE    206.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    90.00  DOWNSTREAM(FEET) =    28.00
CHANNEL LENGTH THRU SUBAREA(FEET) =   345.00  CHANNEL SLOPE =  0.1797
CHANNEL BASE(FEET) =    0.00  "Z" FACTOR =    2.000
MANNING'S FACTOR = 0.015  MAXIMUM DEPTH(FEET) =    2.00
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =  2.757
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp      Ap      SCS
  LAND USE             GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
PUBLIC PARK            D       1.50     0.20    0.850   75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.850
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    6.04
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =  14.60
AVERAGE FLOW DEPTH(FEET) =  0.45  TRAVEL TIME(MIN.) =  0.39
Tc(MIN.) =    9.82
SUBAREA AREA(ACRES) =    1.50     SUBAREA RUNOFF(CFS) =    3.49
EFFECTIVE AREA(ACRES) =    3.30   AREA-AVERAGED Fm(INCH/HR) =  0.17
AREA-AVERAGED Fp(INCH/HR) =  0.20  AREA-AVERAGED Ap =  0.85
TOTAL AREA(ACRES) =    3.3       PEAK FLOW RATE(CFS) =    7.68

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) =  0.50  FLOW VELOCITY(FEET/SEC.) =  15.44
LONGEST FLOWPATH FROM NODE    203.00 TO NODE    206.00 =    725.00 FEET.
```

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*****
FLOW PROCESS FROM NODE    206.00 TO NODE    207.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    18.00  DOWNSTREAM(FEET) =    13.00
FLOW LENGTH(FEET) =    70.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS  8.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  12.91
ESTIMATED PIPE DIAMETER(INCH) =  12.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =    7.68
PIPE TRAVEL TIME(MIN.) =  0.09  Tc(MIN.) =    9.91
LONGEST FLOWPATH FROM NODE    203.00 TO NODE    207.00 =    795.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE    207.00 TO NODE    207.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
MAINLINE Tc(MIN.) =    9.91
* 10 YEAR RAINFALL INTENSITY(INCH/HR) =  2.743
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp      Ap      SCS
  LAND USE             GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
COMMERCIAL            D       1.90     0.20    0.100   75
PUBLIC PARK            D       0.60     0.20    0.850   75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.280
SUBAREA AREA(ACRES) =    2.50     SUBAREA RUNOFF(CFS) =    6.05
EFFECTIVE AREA(ACRES) =    5.80   AREA-AVERAGED Fm(INCH/HR) =  0.12
AREA-AVERAGED Fp(INCH/HR) =  0.20  AREA-AVERAGED Ap =  0.60
TOTAL AREA(ACRES) =    5.8       PEAK FLOW RATE(CFS) =   13.69
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*****
FLOW PROCESS FROM NODE    207.00 TO NODE    191.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    13.00  DOWNSTREAM(FEET) =    5.50
FLOW LENGTH(FEET) =    85.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS  9.7 INCHES
```


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PIPE-FLOW VELOCITY(FEET/SEC.) = 16.29
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 13.69
 PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.00
 LONGEST FLOWPATH FROM NODE 203.00 TO NODE 191.00 = 880.00 FEET.

 FLOW PROCESS FROM NODE 191.00 TO NODE 191.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
 TIME OF CONCENTRATION(MIN.) = 10.00
 RAINFALL INTENSITY(INCH/HR) = 2.73
 AREA-AVERAGED Fm(INCH/HR) = 0.12
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.60
 EFFECTIVE STREAM AREA(ACRES) = 5.80
 TOTAL STREAM AREA(ACRES) = 5.80
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.69

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	289.91	7.46	3.229	0.20(0.07)	0.33	93.3	300.00
1	313.48	8.89	2.918	0.20(0.07)	0.33	113.0	181.00
1	313.88	8.92	2.913	0.20(0.07)	0.33	113.3	170.00
1	318.35	9.32	2.841	0.20(0.07)	0.33	118.4	186.00
1	323.65	9.88	2.748	0.20(0.07)	0.34	125.0	176.00
1	344.44	12.36	2.416	0.20(0.07)	0.34	153.1	107.00
1	346.61	12.76	2.373	0.20(0.07)	0.34	157.5	160.00
1	347.61	13.08	2.340	0.20(0.07)	0.34	160.5	151.00
1	345.33	15.90	2.092	0.20(0.07)	0.35	182.0	101.00
1	344.15	16.93	2.018	0.20(0.07)	0.35	188.9	118.00
1	343.78	17.03	2.011	0.20(0.07)	0.35	189.5	136.00
1	339.78	17.58	1.975	0.20(0.07)	0.35	191.0	146.00
1	307.16	21.81	1.745	0.20(0.07)	0.35	197.7	112.00
1	290.25	24.27	1.642	0.20(0.07)	0.36	199.6	126.00
2	47.49	17.77	1.963	0.20(0.10)	0.48	28.2	192.00
3	13.69	10.00	2.729	0.20(0.12)	0.60	5.8	203.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	335.51	7.46	3.229	0.20(0.07)	0.36	109.4	300.00
2	362.48	8.89	2.918	0.20(0.07)	0.36	132.3	181.00
3	362.95	8.92	2.913	0.20(0.07)	0.36	132.7	170.00
4	368.28	9.32	2.841	0.20(0.07)	0.36	138.6	186.00
5	374.78	9.88	2.748	0.20(0.07)	0.36	146.4	176.00
6	376.04	10.00	2.729	0.20(0.07)	0.36	148.1	203.00
7	397.56	12.36	2.416	0.20(0.07)	0.36	178.6	107.00
8	400.03	12.76	2.373	0.20(0.07)	0.36	183.5	160.00
9	401.26	13.08	2.340	0.20(0.07)	0.36	187.1	151.00
10	401.11	15.90	2.092	0.20(0.07)	0.37	213.1	101.00
11	400.69	16.93	2.018	0.20(0.07)	0.37	221.6	118.00
12	400.40	17.03	2.011	0.20(0.07)	0.37	222.3	136.00
13	396.80	17.58	1.975	0.20(0.07)	0.37	224.7	146.00
14	395.48	17.77	1.963	0.20(0.07)	0.37	225.3	192.00
15	357.63	21.81	1.745	0.20(0.08)	0.38	231.7	112.00
16	337.54	24.27	1.642	0.20(0.08)	0.38	233.6	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 401.26 Tc(MIN.) = 13.08
 EFFECTIVE AREA(ACRES) = 187.10 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
 TOTAL AREA(ACRES) = 233.6
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 191.00 = 8355.00 FEET.

DPHOSP2

 FLOW PROCESS FROM NODE 191.00 TO NODE 207.20 IS CODE = 31

 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 5.50 DOWNSTREAM(FEET) = 3.30
 FLOW LENGTH(FEET) = 485.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 84.0 INCH PIPE IS 67.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 12.09
 ESTIMATED PIPE DIAMETER(INCH) = 84.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 401.26
 PIPE TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 13.75
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 207.20 = 8840.00 FEET.

 FLOW PROCESS FROM NODE 207.20 TO NODE 208.00 IS CODE = 31

 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 3.30 DOWNSTREAM(FEET) = 1.38
 FLOW LENGTH(FEET) = 190.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 72.0 INCH PIPE IS 58.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 16.28
 ESTIMATED PIPE DIAMETER(INCH) = 72.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 401.26
 PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 13.94
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 208.00 = 9030.00 FEET.

 FLOW PROCESS FROM NODE 208.00 TO NODE 208.00 IS CODE = 1

 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 =====
 TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 13.94
 RAINFALL INTENSITY(INCH/HR) = 2.26
 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.36
 EFFECTIVE STREAM AREA(ACRES) = 187.10
 TOTAL STREAM AREA(ACRES) = 233.60
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 401.26

 FLOW PROCESS FROM NODE 2001.00 TO NODE 2002.00 IS CODE = 21

 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
 =====
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 323.00
 ELEVATION DATA: UPSTREAM(FEET) = 24.30 DOWNSTREAM(FEET) = 14.70

 $T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.194
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.591
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	D	0.88	0.20	0.100	75	6.19

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA RUNOFF(CFS) = 2.83
 TOTAL AREA(ACRES) = 0.88 PEAK FLOW RATE(CFS) = 2.83

 FLOW PROCESS FROM NODE 2002.00 TO NODE 2003.00 IS CODE = 31

 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====

DPHOSP2

ELEVATION DATA: UPSTREAM(FEET) = 10.70 DOWNSTREAM(FEET) = 8.50
FLOW LENGTH(FEET) = 279.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 9.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.34
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.83
PIPE TRAVEL TIME(MIN.) = 1.07 Tc(MIN.) = 7.27
LONGEST FLOWPATH FROM NODE 2001.00 TO NODE 2003.00 = 602.00 FEET.

FLOW PROCESS FROM NODE 2003.00 TO NODE 2003.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====

MAINLINE Tc(MIN.) = 7.27
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.277
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 1.29 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.29 SUBAREA RUNOFF(CFS) = 3.78
EFFECTIVE AREA(ACRES) = 2.17 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 6.36

FLOW PROCESS FROM NODE 2003.00 TO NODE 208.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 8.50 DOWNSTREAM(FEET) = 1.38
FLOW LENGTH(FEET) = 206.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 15.0 INCH PIPE IS 8.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.54
ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.36
PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 7.62
LONGEST FLOWPATH FROM NODE 2001.00 TO NODE 208.00 = 808.00 FEET.

FLOW PROCESS FROM NODE 208.00 TO NODE 208.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.62
RAINFALL INTENSITY(INCH/HR) = 3.19
AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 2.17
TOTAL STREAM AREA(ACRES) = 2.17
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.36

FLOW PROCESS FROM NODE 2011.00 TO NODE 2012.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 293.00
ELEVATION DATA: UPSTREAM(FEET) = 23.00 DOWNSTREAM(FEET) = 9.70

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.473
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.855
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)

DPHOSP2

COMMERCIAL D 0.29 0.20 0.100 75 5.47
SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.100
SUBAREA RUNOFF(CFS) = 1.00
TOTAL AREA(ACRES) = 0.29 PEAK FLOW RATE(CFS) = 1.00

FLOW PROCESS FROM NODE 2012.00 TO NODE 2013.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 5.70 DOWNSTREAM(FEET) = 4.00
FLOW LENGTH(FEET) = 153.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.90
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.00
PIPE TRAVEL TIME(MIN.) = 0.65 T_c (MIN.) = 6.13
LONGEST FLOWPATH FROM NODE 2011.00 TO NODE 2013.00 = 446.00 FEET.

FLOW PROCESS FROM NODE 2013.00 TO NODE 2013.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====

MAINLINE T_c (MIN.) = 6.13
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.613
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
COMMERCIAL	D	0.56	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.100
SUBAREA AREA(ACRES) = 0.56 SUBAREA RUNOFF(CFS) = 1.81
EFFECTIVE AREA(ACRES) = 0.85 AREA-AVERAGED F_m (INCH/HR) = 0.02
AREA-AVERAGED F_p (INCH/HR) = 0.20 AREA-AVERAGED A_p = 0.10
TOTAL AREA(ACRES) = 0.9 PEAK FLOW RATE(CFS) = 2.75

FLOW PROCESS FROM NODE 2013.00 TO NODE 208.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 4.00 DOWNSTREAM(FEET) = 1.38
FLOW LENGTH(FEET) = 18.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.05
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.75
PIPE TRAVEL TIME(MIN.) = 0.02 T_c (MIN.) = 6.15
LONGEST FLOWPATH FROM NODE 2011.00 TO NODE 208.00 = 464.00 FEET.

FLOW PROCESS FROM NODE 208.00 TO NODE 208.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 6.15
RAINFALL INTENSITY(INCH/HR) = 3.61
AREA-AVERAGED F_m (INCH/HR) = 0.02
AREA-AVERAGED F_p (INCH/HR) = 0.20
AREA-AVERAGED A_p = 0.10
EFFECTIVE STREAM AREA(ACRES) = 0.85
TOTAL STREAM AREA(ACRES) = 0.85
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.75

DPHOSP2

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	335.51	8.35	3.027	0.20(0.07)	0.36	109.4	300.00
1	362.48	9.78	2.765	0.20(0.07)	0.36	132.3	181.00
1	362.95	9.80	2.760	0.20(0.07)	0.36	132.7	170.00
1	368.28	10.20	2.698	0.20(0.07)	0.36	138.6	186.00
1	374.78	10.74	2.619	0.20(0.07)	0.36	146.4	176.00
1	376.04	10.87	2.602	0.20(0.07)	0.36	148.1	203.00
1	397.56	13.23	2.325	0.20(0.07)	0.36	178.6	107.00
1	400.03	13.63	2.285	0.20(0.07)	0.36	183.5	160.00
1	401.26	13.94	2.256	0.20(0.07)	0.36	187.1	151.00
1	401.11	16.76	2.030	0.20(0.07)	0.37	213.1	101.00
1	400.69	17.79	1.962	0.20(0.07)	0.37	221.6	118.00
1	400.40	17.90	1.955	0.20(0.07)	0.37	222.3	136.00
1	396.80	18.44	1.922	0.20(0.07)	0.37	224.7	146.00
1	395.48	18.63	1.911	0.20(0.07)	0.37	225.3	192.00
1	357.63	22.70	1.706	0.20(0.08)	0.38	231.7	112.00
1	337.54	25.16	1.608	0.20(0.08)	0.38	233.6	126.00
2	6.36	7.62	3.188	0.20(0.02)	0.10	2.2	2001.00
3	2.75	6.15	3.606	0.20(0.02)	0.10	0.9	2011.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	304.20	6.15	3.606	0.20(0.07)	0.35	83.2	2011.00
2	332.00	7.62	3.188	0.20(0.07)	0.35	103.0	2001.00
3	343.86	8.35	3.027	0.20(0.07)	0.35	112.4	300.00
4	370.10	9.78	2.765	0.20(0.07)	0.35	135.3	181.00
5	370.55	9.80	2.760	0.20(0.07)	0.35	135.7	170.00
6	375.72	10.20	2.698	0.20(0.07)	0.36	141.6	186.00
7	381.99	10.74	2.619	0.20(0.07)	0.36	149.5	176.00
8	383.21	10.87	2.602	0.20(0.07)	0.36	151.1	203.00
9	403.96	13.23	2.325	0.20(0.07)	0.36	181.6	107.00
10	406.32	13.63	2.285	0.20(0.07)	0.36	186.5	160.00
11	407.47	13.94	2.256	0.20(0.07)	0.36	190.1	151.00
12	406.68	16.76	2.030	0.20(0.07)	0.37	216.1	101.00
13	406.08	17.79	1.962	0.20(0.07)	0.37	224.6	118.00
14	405.76	17.90	1.955	0.20(0.07)	0.37	225.3	136.00
15	402.07	18.44	1.922	0.20(0.07)	0.37	227.7	146.00
16	400.72	18.63	1.911	0.20(0.07)	0.37	228.3	192.00
17	362.31	22.70	1.706	0.20(0.07)	0.37	234.7	112.00
18	341.95	25.16	1.608	0.20(0.07)	0.37	236.6	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 407.47 Tc(MIN.) = 13.94
EFFECTIVE AREA(ACRES) = 190.12 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 236.6
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 208.00 = 9030.00 FEET.

FLOW PROCESS FROM NODE 208.00 TO NODE 209.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====

ELEVATION DATA: UPSTREAM(FEET) = 1.38 DOWNSTREAM(FEET) = 0.20
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 78.0 INCH PIPE IS 60.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 14.65
ESTIMATED PIPE DIAMETER(INCH) = 78.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 407.47
PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 14.12
LONGEST FLOWPATH FROM NODE 112.00 TO NODE 209.00 = 9190.00 FEET.

FLOW PROCESS FROM NODE 209.00 TO NODE 209.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

DPHOSP2

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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.12
RAINFALL INTENSITY(INCH/HR) = 2.24
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.36
EFFECTIVE STREAM AREA(ACRES) = 190.12
TOTAL STREAM AREA(ACRES) = 236.62
PEAK FLOW RATE(CFS) AT CONFLUENCE = 407.47

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FLOW PROCESS FROM NODE 2021.00 TO NODE 2022.00 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 155.00
ELEVATION DATA: UPSTREAM(FEET) = 10.30 DOWNSTREAM(FEET) = 9.50

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Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.553
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.477
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS  Tc
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL            D      0.15      0.20      0.100    75   6.55
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 0.47
TOTAL AREA(ACRES) = 0.15 PEAK FLOW RATE(CFS) = 0.47

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FLOW PROCESS FROM NODE 2022.00 TO NODE 2023.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 6.50 DOWNSTREAM(FEET) = 5.20
FLOW LENGTH(FEET) = 250.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.40
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.47
PIPE TRAVEL TIME(MIN.) = 1.73 Tc(MIN.) = 8.29
LONGEST FLOWPATH FROM NODE 2021.00 TO NODE 2023.00 = 405.00 FEET.

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*****
FLOW PROCESS FROM NODE 2023.00 TO NODE 2023.00 IS CODE = 81
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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
MAINLINE Tc(MIN.) = 8.29
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.039
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS
LAND USE              GROUP  (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL            D      0.11      0.20      0.100    75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.30
EFFECTIVE AREA(ACRES) = 0.26 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 0.71

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FLOW PROCESS FROM NODE 2023.00 TO NODE 2024.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====

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DPHOSP2

ELEVATION DATA: UPSTREAM(FEET) = 5.20 DOWNSTREAM(FEET) = 4.00
FLOW LENGTH(FEET) = 207.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.80
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.71
PIPE TRAVEL TIME(MIN.) = 1.23 Tc(MIN.) = 9.52
LONGEST FLOWPATH FROM NODE 2021.00 TO NODE 2024.00 = 612.00 FEET.

FLOW PROCESS FROM NODE 2024.00 TO NODE 2024.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 9.52
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.807
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 0.21 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.21 SUBAREA RUNOFF(CFS) = 0.53
EFFECTIVE AREA(ACRES) = 0.47 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 1.18

FLOW PROCESS FROM NODE 2024.00 TO NODE 209.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 4.00 DOWNSTREAM(FEET) = 0.20
FLOW LENGTH(FEET) = 16.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 12.000
DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.12
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.18
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 9.54
LONGEST FLOWPATH FROM NODE 2021.00 TO NODE 209.00 = 628.00 FEET.

FLOW PROCESS FROM NODE 209.00 TO NODE 209.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.54
RAINFALL INTENSITY(INCH/HR) = 2.80
AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 0.47
TOTAL STREAM AREA(ACRES) = 0.47
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.18

** CONFLUENCE DATA **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists 11 rows of stream data.

DPHOSP2

1	406.32	13.81	2.268	0.20(0.07)	0.36	186.5	160.00
1	407.47	14.12	2.239	0.20(0.07)	0.36	190.1	151.00
1	406.68	16.94	2.017	0.20(0.07)	0.37	216.1	101.00
1	406.08	17.97	1.950	0.20(0.07)	0.37	224.6	118.00
1	405.76	18.08	1.944	0.20(0.07)	0.37	225.3	136.00
1	402.07	18.62	1.911	0.20(0.07)	0.37	227.7	146.00
1	400.72	18.81	1.900	0.20(0.07)	0.37	228.3	192.00
1	362.31	22.88	1.698	0.20(0.07)	0.37	234.7	112.00
1	341.95	25.35	1.601	0.20(0.07)	0.37	236.6	126.00
2	1.18	9.54	2.803	0.20(0.02)	0.10	0.5	2021.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	305.19	6.35	3.541	0.20(0.07)	0.35	83.5	2011.00
2	333.08	7.82	3.143	0.20(0.07)	0.35	103.4	2001.00
3	344.98	8.54	2.988	0.20(0.07)	0.35	112.9	300.00
4	363.55	9.54	2.803	0.20(0.07)	0.35	129.0	2021.00
5	371.25	9.96	2.735	0.20(0.07)	0.35	135.8	181.00
6	371.70	9.99	2.730	0.20(0.07)	0.35	136.2	170.00
7	376.84	10.39	2.670	0.20(0.07)	0.35	142.1	186.00
8	383.08	10.93	2.593	0.20(0.07)	0.36	149.9	176.00
9	384.29	11.05	2.577	0.20(0.07)	0.36	151.6	203.00
10	404.93	13.41	2.307	0.20(0.07)	0.36	182.1	107.00
11	407.27	13.81	2.268	0.20(0.07)	0.36	187.0	160.00
12	408.41	14.12	2.239	0.20(0.07)	0.36	190.6	151.00
13	407.53	16.94	2.017	0.20(0.07)	0.37	216.6	101.00
14	406.89	17.97	1.950	0.20(0.07)	0.37	225.1	118.00
15	406.58	18.08	1.944	0.20(0.07)	0.37	225.8	136.00
16	402.87	18.62	1.911	0.20(0.07)	0.37	228.2	146.00
17	401.52	18.81	1.900	0.20(0.07)	0.37	228.8	192.00
18	363.02	22.88	1.698	0.20(0.07)	0.37	235.2	112.00
19	342.62	25.35	1.601	0.20(0.07)	0.37	237.1	126.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 408.41 Tc(MIN.) = 14.12
 EFFECTIVE AREA(ACRES) = 190.59 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.36
 TOTAL AREA(ACRES) = 237.1
 LONGEST FLOWPATH FROM NODE 112.00 TO NODE 209.00 = 9190.00 FEET.

=====
 END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 237.1 TC(MIN.) = 14.12
 EFFECTIVE AREA(ACRES) = 190.59 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.360
 PEAK FLOW RATE(CFS) = 408.41

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	305.19	6.35	3.541	0.20(0.07)	0.35	83.5	2011.00
2	333.08	7.82	3.143	0.20(0.07)	0.35	103.4	2001.00
3	344.98	8.54	2.988	0.20(0.07)	0.35	112.9	300.00
4	363.55	9.54	2.803	0.20(0.07)	0.35	129.0	2021.00
5	371.25	9.96	2.735	0.20(0.07)	0.35	135.8	181.00
6	371.70	9.99	2.730	0.20(0.07)	0.35	136.2	170.00
7	376.84	10.39	2.670	0.20(0.07)	0.35	142.1	186.00
8	383.08	10.93	2.593	0.20(0.07)	0.36	149.9	176.00
9	384.29	11.05	2.577	0.20(0.07)	0.36	151.6	203.00
10	404.93	13.41	2.307	0.20(0.07)	0.36	182.1	107.00
11	407.27	13.81	2.268	0.20(0.07)	0.36	187.0	160.00
12	408.41	14.12	2.239	0.20(0.07)	0.36	190.6	151.00
13	407.53	16.94	2.017	0.20(0.07)	0.37	216.6	101.00
14	406.89	17.97	1.950	0.20(0.07)	0.37	225.1	118.00
15	406.58	18.08	1.944	0.20(0.07)	0.37	225.8	136.00
16	402.87	18.62	1.911	0.20(0.07)	0.37	228.2	146.00
17	401.52	18.81	1.900	0.20(0.07)	0.37	228.8	192.00
18	363.02	22.88	1.698	0.20(0.07)	0.37	235.2	112.00
19	342.62	25.35	1.601	0.20(0.07)	0.37	237.1	126.00

DPHOSP2

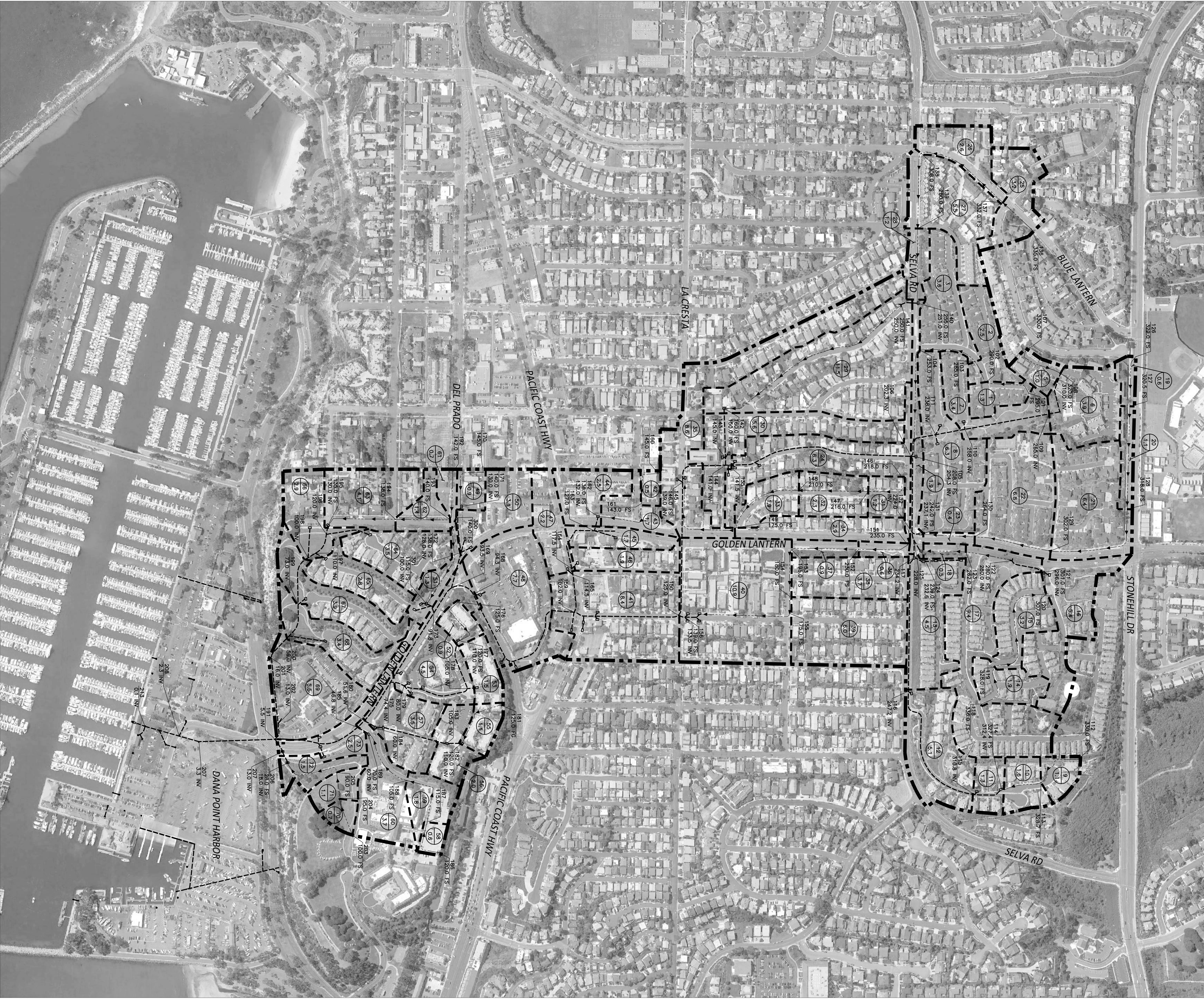
=====
END OF RATIONAL METHOD ANALYSIS

♀

APPENDIX C. HYDROLOGY MAPS

- C.1 EXISTING CONDITION W/O HARBOR
- C.2 EXISTING CONDITION W/ HARBOR
- C.3 PROPOSED CONDITION W/ HARBOR

C.1



LEGEND

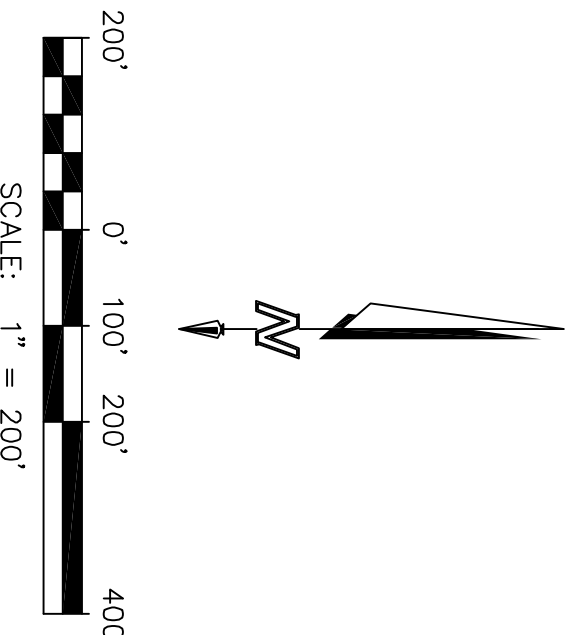
- MAJOR WATERSHED BOUNDARY
- DRAINAGE SUBAREA BOUNDARY
- FLOW PATH
- EXISTING STORM DRAIN
- DRAINAGE AREA DESIGNATION
- AREA (ACRES)
- NODE NUMBER
- FINISHED SURFACE ELEVATION
- PIPE INVERT ELEVATION



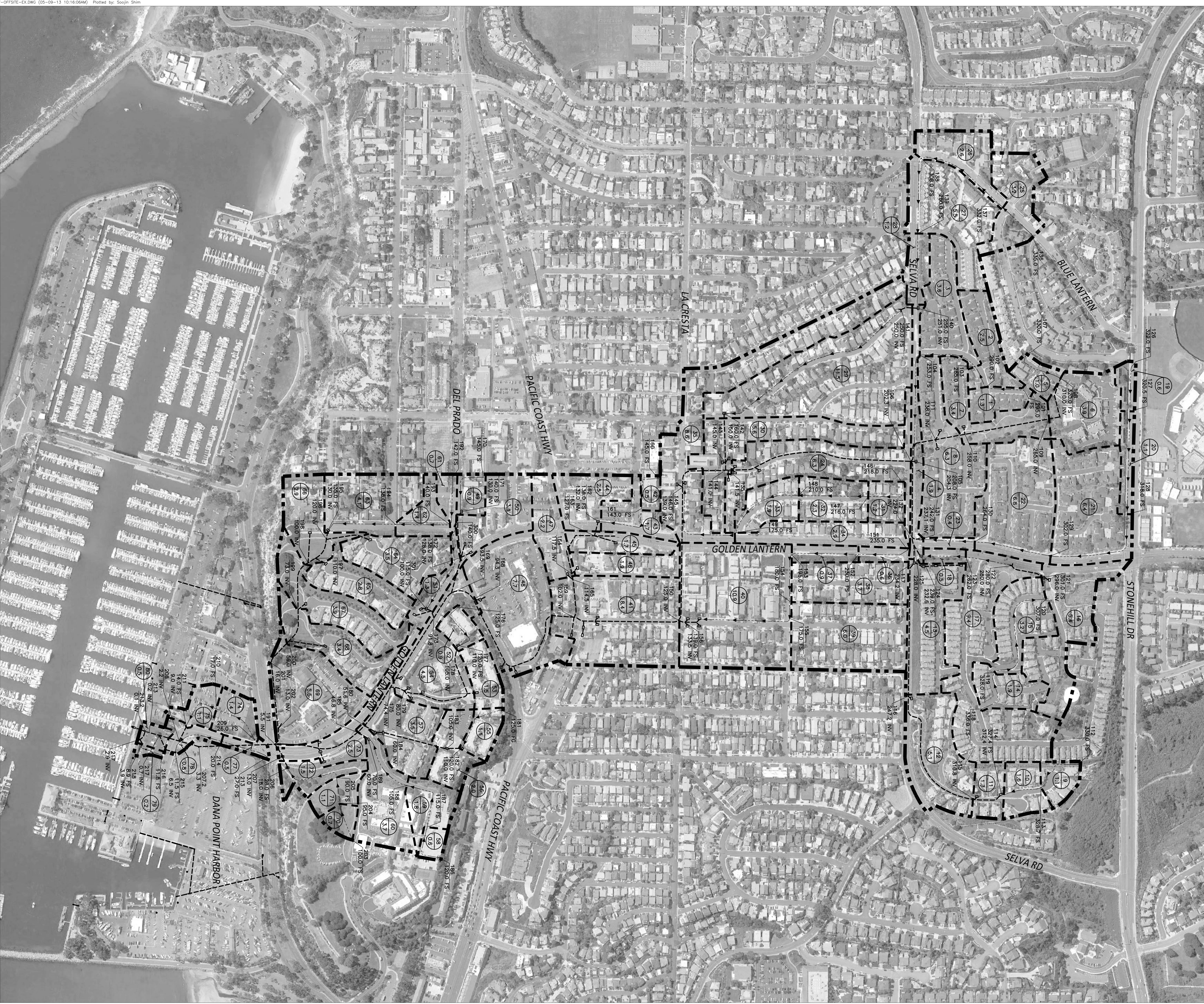
STORM DRAIN LINE L00P01 EXISTING CONDITION HYDROLOGY MAP
 (EXCLUDING TRIBUTARY FROM OC DANA POINT HARBOR)

CITY OF DANA POINT, COUNTY OF ORANGE

EXHIBIT A



C.2



LEGEND

- MAJOR WATERSHED BOUNDARY
- DRAINAGE SUBAREA BOUNDARY
- FLOW PATH
- EXISTING STORM DRAIN
- DRAINAGE AREA DESIGNATION
- AREA (ACRES)
- NODE NUMBER
- FINISHED SURFACE ELEVATION
- PIPE INVERT ELEVATION

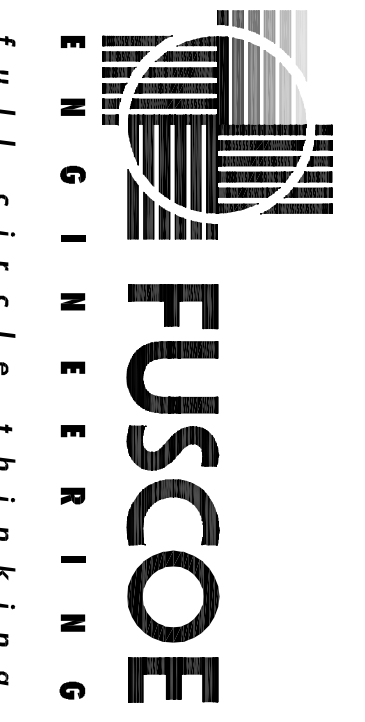
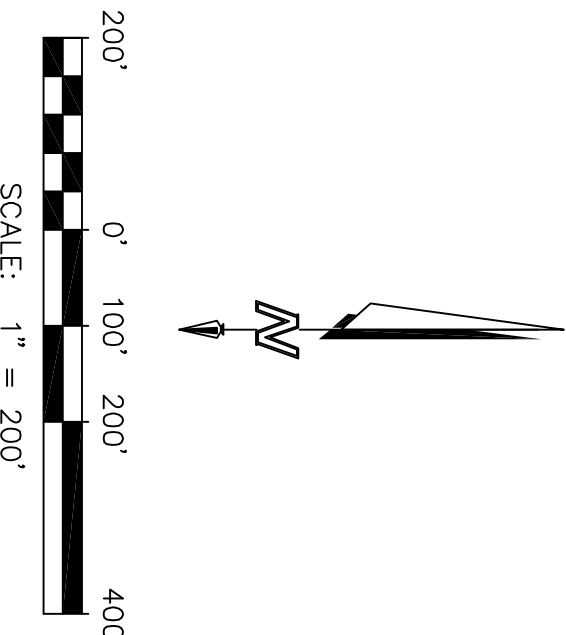


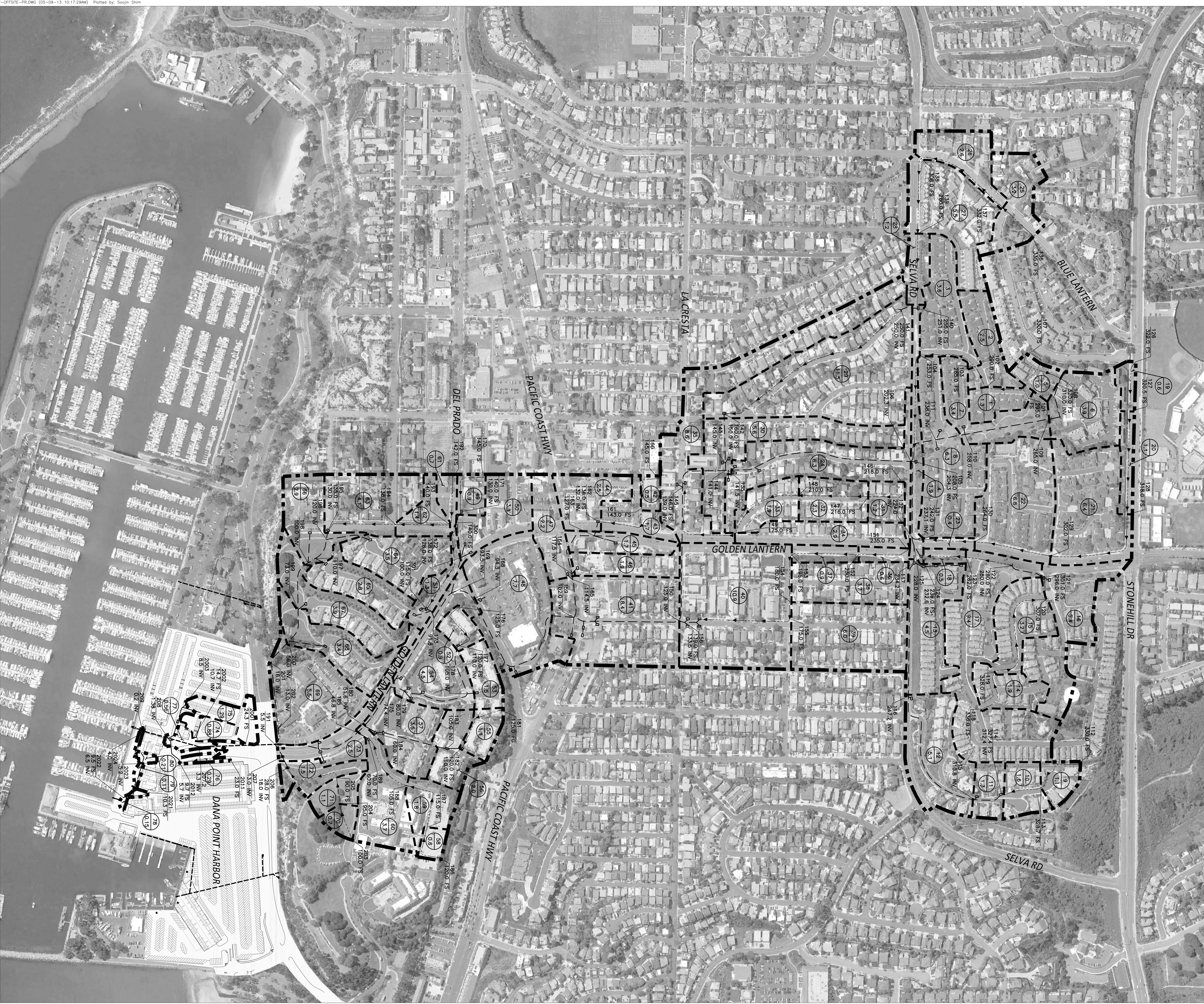
EXHIBIT B

**STORM DRAIN LINE L00P01 EXISTING CONDITION HYDROLOGY MAP
(INCLUDING TRIBUTARY FROM OC DANA POINT HARBOR)**

CITY OF DANA POINT, COUNTY OF ORANGE

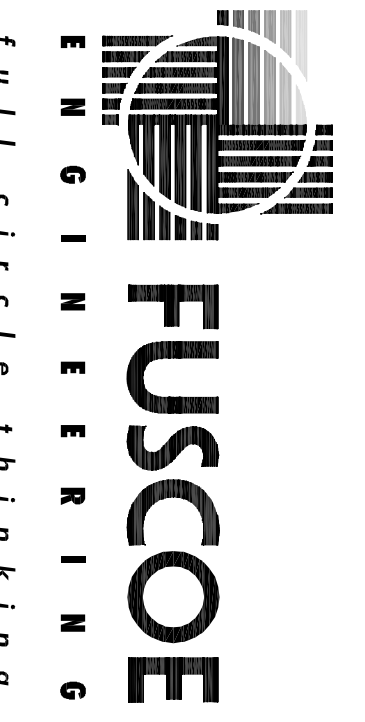


C.3



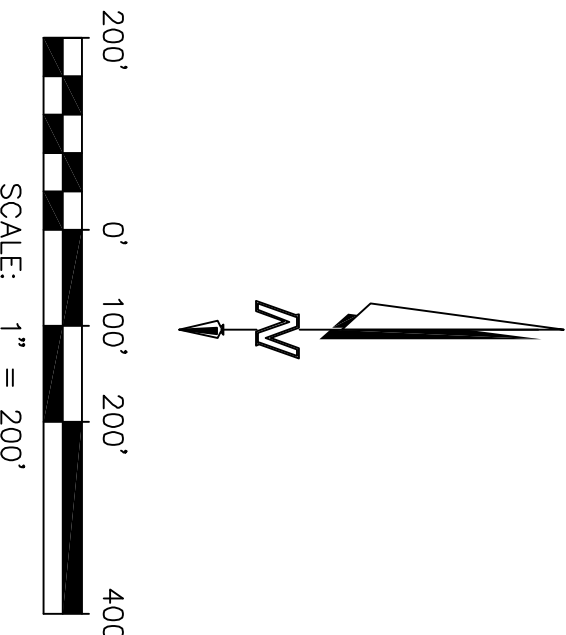
LEGEND

- MAJOR WATERSHED BOUNDARY
- DRAINAGE SUBAREA BOUNDARY
- FLOW PATH
- EXISTING STORM DRAIN
- DRAINAGE AREA DESIGNATION
- AREA (ACRES)
- NODE NUMBER
- FINISHED SURFACE ELEVATION
- PIPE INVERT ELEVATION



**STORM DRAIN LINE L00P01 PROPOSED CONDITION HYDROLOGY MAP
(INCLUDING TRIBUTARY FROM OC DANA POINT HARBOR)**

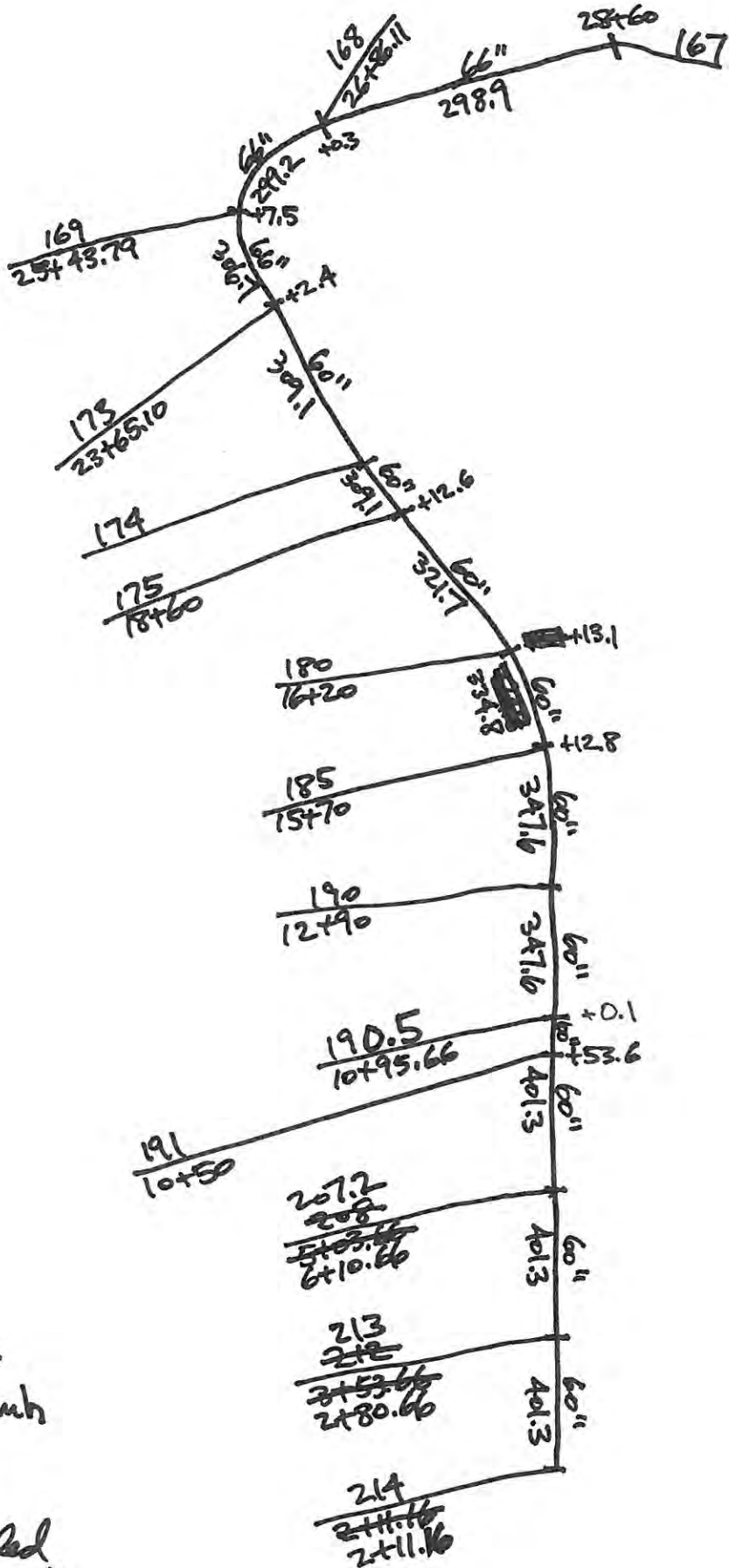
EXHIBIT C



APPENDIX D. WSPG HYDRAULIC MODELS

- D.1 EXISTING CONDITION W/O HARBOR (MODEL 1)
- D.2 EXISTING CONDITION W/ HARBOR (MODEL 2)
- D.3 PROPOSED CONDITION W/ HARBOR (MODEL 3)

D.1



Hydrology: DPHOSR2
 Hydraulics: dphjx60mb

Existing 10-year
 w/o Harbor Included
 (Consistent w/ City MPD)

Exist. 10-yr 60" Hydraulic
w/o Harbor

♀ FILE: dphjx60mh.WSW

dphjx60mh
W S P G W - CIVILDESIGN Version 14.06
Program Package Serial Number: 1863
WATER SURFACE PROFILE LISTING

PAGE 1

Date: 5- 2-2013 Time: 2:42:42

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
199.390	-12.220	17.260	5.040	401.40	8.03	1.00	6.04	.00	3.69	10.00	5.000	10.000	.00	0 .0
11.770	.0518					.0033	.04	17.26	.63	1.58	.015	-.02	.00	BOX
211.160	-11.610	16.689	5.079	401.40	8.03	1.00	6.08	.00	3.69	10.00	5.000	10.000	.00	0 .0
TRANS STR	.0500					.0175	.44	16.69	.63		.015	.00	.00	BOX
236.140	-10.360	11.484	1.124	401.40	20.44	6.49	7.61	.00	4.89	.00	5.000	.000	.00	1 .0
2.211	.2269					.0238	.05	11.48	.00	1.96	.013	.00	.00	PIPE
238.351	-9.858	11.031	1.173	401.40	20.44	6.49	7.66	.00	4.89	.00	5.000	.000	.00	1 .0
HYDRAULIC JUMP														
238.351	-9.858	3.001	-6.857	401.40	32.62	16.52	9.66	.00	4.89	4.90	5.000	.000	.00	1 .0
5.406	.2269					.0505	.27	3.00	3.63	1.96	.013	.00	.00	PIPE
243.758	-8.632	3.084	-5.548	401.40	31.58	15.48	9.93	.00	4.89	4.86	5.000	.000	.00	1 .0
7.057	.2269					.0456	.32	3.08	3.44	1.96	.013	.00	.00	PIPE
250.815	-7.031	3.213	-3.818	401.40	30.11	14.07	10.26	.00	4.89	4.79	5.000	.000	.00	1 .0
6.131	.2269					.0405	.25	3.21	3.18	1.96	.013	.00	.00	PIPE
256.946	-5.640	3.350	-2.290	401.40	28.71	12.80	10.51	.00	4.89	4.70	5.000	.000	.00	1 .0
5.326	.2269					.0360	.19	3.35	2.93	1.96	.013	.00	.00	PIPE
262.272	-4.432	3.497	-.935	401.40	27.37	11.63	10.70	.00	4.89	4.59	5.000	.000	.00	1 .0
4.616	.2269					.0322	.15	3.50	2.70	1.96	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1054.000	5.290	20.952	26.242	347.80	17.71	4.87	31.11	.00	4.80	.00	5.000	.000	.00	1 .0
41.660	.0046					.0178	.74	20.95	.00	5.00	.013	.00	.00	PIPE
1095.660	5.480	21.505	26.985	347.80	17.71	4.87	31.86	.00	4.80	.00	5.000	.000	.00	1 .0
JUNCT STR	.0420					.0178	.09	21.50	.00		.013	.00	.00	PIPE
1100.660	5.690	21.390	27.080	347.70	17.71	4.87	31.95	.00	4.80	.00	5.000	.000	.00	1 .0
24.170	.1080					.0178	.43	21.39	.00	2.22	.013	.00	.00	PIPE
1124.830	8.300	19.210	27.510	347.70	17.71	4.87	32.38	.00	4.80	.00	5.000	.000	.00	1 .0
64.140	.1082					.0178	1.14	.00	.00	2.22	.013	.00	.00	PIPE
1188.970	15.240	13.789	29.029	347.70	17.71	4.87	33.90	.00	4.80	.00	5.000	.000	.00	1 .0
6.007	.0740					.0178	.11	13.79	.00	2.47	.013	.00	.00	PIPE
1194.977	15.684	13.452	29.137	347.70	17.71	4.87	34.01	.00	4.80	.00	5.000	.000	.00	1 .0
HYDRAULIC JUMP														
1194.977	15.684	2.429	18.114	347.70	36.74	20.95	39.07	.00	4.80	5.00	5.000	.000	.00	1 .0
92.523	.0740					.0800	7.40	2.43	4.70	2.47	.013	.00	.00	PIPE
1287.500	22.530	2.405	24.935	347.70	37.22	21.52	46.45	.00	4.80	5.00	5.000	.000	.00	1 .0
JUNCT STR	.0720					.0816	.41	2.40	4.80		.013	.00	.00	PIPE
1292.500	22.890	2.402	25.292	347.60	37.27	21.57	46.86	.00	4.80	5.00	5.000	.000	.00	1 .0
65.970	.0741					.0834	5.50	2.40	4.81	2.47	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
1358.470	27.780	2.375	30.155	347.60	37.82	22.21	52.37	1.47	4.80	4.99	5.000	.000	.00	1 .0
101.230	.0873					.0842	8.52	3.85	4.91	2.36	.013	.00	.00	PIPE
1459.700	36.620	2.388	39.008	347.60	37.54	21.88	60.89	.36	4.80	5.00	5.000	.000	.00	1 .0
107.800	.0924					.0797	8.59	2.75	4.86	2.32	.013	.00	.00	PIPE
1567.500	46.580	2.452	49.032	347.60	36.30	20.46	69.49	.00	4.80	5.00	5.000	.000	.00	1 .0
JUNCT STR	.0920					.0788	.39	2.82	4.62		.013	.00	.00	PIPE
1572.500	47.040	2.353	49.393	334.80	36.86	21.10	70.49	.38	4.78	4.99	5.000	.000	.00	1 .0
45.000	.0924					.0799	3.60	2.73	4.82	2.27	.013	.00	.00	PIPE
1617.500	51.200	2.379	53.579	334.80	36.34	20.51	74.09	.00	4.78	4.99	5.000	.000	.00	1 .0
JUNCT STR	.1600					.0786	.39	2.72	4.72		.013	.00	.00	PIPE
1622.500	52.000	2.322	54.322	321.70	36.03	20.16	74.49	.33	4.74	4.99	5.000	.000	.00	1 .0
87.549	.0936					.0741	6.49	2.65	4.75	2.21	.013	.00	.00	PIPE
1710.049	60.193	2.407	62.600	321.70	34.40	18.38	80.98	.30	4.74	5.00	5.000	.000	.00	1 .0
55.961	.0936					.0654	3.66	2.71	4.43	2.21	.013	.00	.00	PIPE
1766.010	65.430	2.498	67.928	321.70	32.80	16.71	84.64	.00	4.74	5.00	5.000	.000	.00	1 .0
37.405	.0937					.0578	2.16	2.50	4.13	2.21	.013	.00	.00	PIPE
1803.415	68.934	2.588	71.522	321.70	31.37	15.28	86.80	.00	4.74	5.00	5.000	.000	.00	1 .0
30.273	.0937					.0511	1.55	2.59	3.86	2.21	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1833.688	71.769	2.688	74.458	321.70	29.91	13.89	88.34	.00	4.74	4.99	5.000	.000	.00	1 .0
23.812	.0937					.0451	1.07	2.69	3.59	2.21	.013	.00	.00	PIPE
1857.500	74.000	2.794	76.794	321.70	28.51	12.62	89.42	.00	4.74	4.97	5.000	.000	.00	1 .0
JUNCT STR	.1080					.0443	.22	2.79	3.33		.013	.00	.00	PIPE
1862.500	74.540	2.652	77.192	309.10	29.23	13.26	90.46	.00	4.70	4.99	5.000	.000	.00	1 .0
24.422	.0772					.0443	1.08	2.65	3.54	2.28	.013	.00	.00	PIPE
1886.923	76.425	2.725	79.151	309.10	28.25	12.39	91.54	.00	4.70	4.98	5.000	.000	.00	1 .0
27.249	.0772					.0398	1.08	2.73	3.36	2.28	.013	.00	.00	PIPE
1914.172	78.529	2.833	81.361	309.10	26.93	11.26	92.63	.00	4.70	4.96	5.000	.000	.00	1 .0
21.663	.0772					.0352	.76	2.83	3.12	2.28	.013	.00	.00	PIPE
1935.835	80.201	2.946	83.147	309.10	25.68	10.24	93.39	.00	4.70	4.92	5.000	.000	.00	1 .0
17.592	.0772					.0311	.55	2.95	2.89	2.28	.013	.00	.00	PIPE
1953.426	81.559	3.066	84.625	309.10	24.48	9.31	93.93	.00	4.70	4.87	5.000	.000	.00	1 .0
14.480	.0772					.0275	.40	3.07	2.68	2.28	.013	.00	.00	PIPE
1967.906	82.677	3.194	85.870	309.10	23.34	8.46	94.33	.00	4.70	4.80	5.000	.000	.00	1 .0
12.012	.0772					.0244	.29	3.19	2.48	2.28	.013	.00	.00	PIPE
1979.918	83.604	3.329	86.933	309.10	22.26	7.69	94.63	.00	4.70	4.72	5.000	.000	.00	1 .0
9.990	.0772					.0217	.22	3.33	2.29	2.28	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

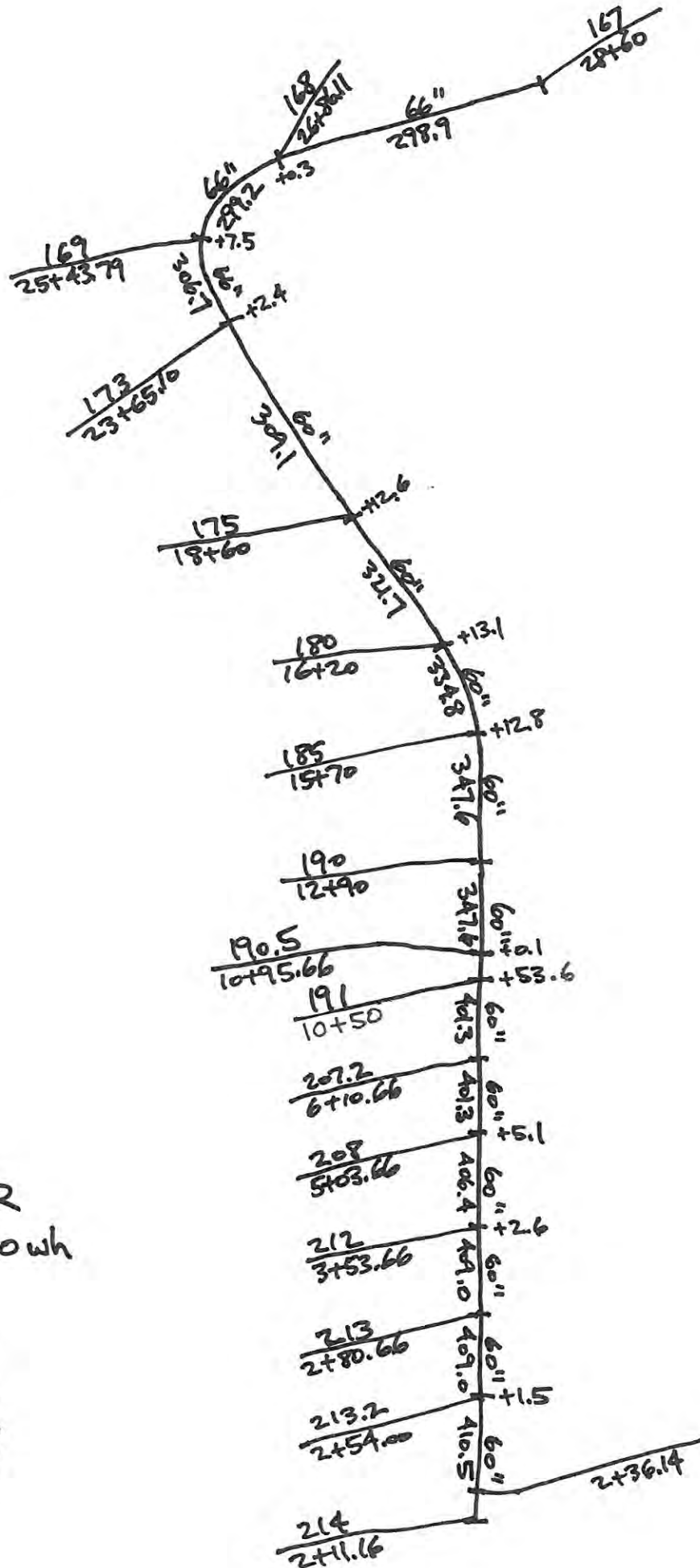
Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1989.908	84.375	3.475	87.850	309.10	21.22	6.99	94.84	.00	4.70	4.60	5.000	.000	.00	1 .0
8.286	.0772					.0194	.16	3.47	2.10	2.28	.013	.00	.00	PIPE
1998.195	85.015	3.632	88.646	309.10	20.24	6.36	95.00	.00	4.70	4.46	5.000	.000	.00	1 .0
6.805	.0772					.0174	.12	3.63	1.93	2.28	.013	.00	.00	PIPE
2005.000	85.540	3.802	89.342	309.10	19.29	5.78	95.12	.00	4.70	4.27	5.000	.000	.00	1 .0
153.531	.0171					.0160	2.46	3.80	1.75	3.74	.013	.00	.00	PIPE
2158.531	88.164	3.886	92.050	309.10	18.88	5.53	97.58	.00	4.70	4.16	5.000	.000	.00	1 .0
139.002	.0171					.0149	2.07	3.89	1.68	3.74	.013	.00	.00	PIPE
2297.533	90.540	4.085	94.625	309.10	18.00	5.03	99.65	.00	4.70	3.87	5.000	.000	.00	1 .0
64.967	.0171					.0136	.88	4.09	1.50	3.74	.013	.00	.00	PIPE
2362.500	91.650	4.314	95.964	309.10	17.16	4.57	100.54	.00	4.70	3.44	5.000	.000	.00	1 .0
JUNCT STR	.1080					.0124	.06	4.31	1.32		.013	.00	.00	PIPE
2367.500	92.190	3.852	96.042	306.70	17.26	4.62	100.67	.00	4.81	5.04	5.500	.000	.00	1 .0
124.250	.0132					.0113	1.40	3.85	1.62	3.70	.013	.00	.00	PIPE
2491.750	93.830	4.021	97.851	306.70	16.48	4.22	102.07	.48	4.81	4.88	5.500	.000	.00	1 .0
49.540	.0131					.0103	.51	4.50	1.49	3.71	.013	.00	.00	PIPE
2541.290	94.480	4.153	98.633	306.70	15.93	3.94	102.58	.00	4.81	4.73	5.500	.000	.00	1 .0
JUNCT STR	.0120					.0106	.05	4.73	1.39		.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
2546.290	94.540	3.840	98.380	299.20	16.89	4.43	102.81	.69	4.76	5.05	5.500	.000	.00	1 .0
83.858	.0133					.0109	.91	4.53	1.59	3.63	.013	.00	.00	PIPE
2630.148	95.651	3.989	99.640	299.20	16.21	4.08	103.72	.62	4.76	4.91	5.500	.000	.00	1 .0
53.462	.0133					.0098	.52	4.61	1.47	3.63	.013	.00	.00	PIPE
2683.610	96.360	4.176	100.536	299.20	15.46	3.71	104.25	.00	4.76	4.70	5.500	.000	.00	1 .0
JUNCT STR	.0100					.0093	.05	4.18	1.34		.013	.00	.00	PIPE
2688.610	96.410	4.162	100.572	298.90	15.50	3.73	104.30	.00	4.76	4.72	5.500	.000	.00	1 .0
94.252	.0100					.0090	.85	4.16	1.35	4.05	.013	.00	.00	PIPE
2782.862	97.350	4.284	101.634	298.90	15.05	3.52	105.15	.00	4.76	4.57	5.500	.000	.00	1 .0
61.405	.0100					.0083	.51	4.28	1.27	4.05	.013	.00	.00	PIPE
2844.267	97.963	4.504	102.467	298.90	14.35	3.20	105.67	.00	4.76	4.24	5.500	.000	.00	1 .0
15.733	.0100					.0076	.12	4.50	1.14	4.05	.013	.00	.00	PIPE
2860.000	98.120	4.758	102.878	298.90	13.68	2.91	105.79	.00	4.76	3.76	5.500	.000	.00	1 .0

D.2



Hydrology : DPHOSR

Hydraulics : dphj x 60 wh

Existing 10-year

/ 3.8 Ac Harbor

+ 0.7 Ac Harbor

Tributary Included

EX. 10-YEAR
60" Hydraulics
w/ Harbor Included

♀ FILE: dphjx60wh.WSW

dphjx60wh
W S P G W - CIVILDESIGN Version 14.06
Program Package Serial Number: 1863
WATER SURFACE PROFILE LISTING

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Dana Point Harbor
60-inch Line L00P01
Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
199.390	-12.220	17.260	5.040	410.60	8.21	1.05	6.09	.00	3.74	10.00	5.000	10.000	.00	0 .0
11.770	.0518					.0035	.04	17.26	.65	1.60	.015	-.02	.00	BOX
211.160	-11.610	16.691	5.081	410.60	8.21	1.05	6.13	.00	3.74	10.00	5.000	10.000	.00	0 .0
TRANS STR	.0500					.0183	.46	16.69	.65		.015	.00	.00	BOX
236.140	-10.360	11.303	.943	410.60	20.91	6.79	7.73	.00	4.90	.00	5.000	.000	.00	1 .0
.577	.2266					.0249	.01	11.30	.00	1.98	.013	.00	.00	PIPE
236.717	-10.229	11.185	.956	410.60	20.91	6.79	7.75	.00	4.90	.00	5.000	.000	.00	1 .0
HYDRAULIC JUMP														
236.717	-10.229	3.028	-7.201	410.60	33.01	16.92	9.72	.00	4.90	4.89	5.000	.000	.00	1 .0
7.792	.2266					.0506	.39	3.03	3.65	1.98	.013	.00	.00	PIPE
244.508	-8.464	3.149	-5.315	410.60	31.52	15.43	10.11	.00	4.90	4.83	5.000	.000	.00	1 .0
6.992	.2266					.0449	.31	3.15	3.38	1.98	.013	.00	.00	PIPE
251.500	-6.880	3.282	-3.598	410.60	30.06	14.03	10.43	.00	4.90	4.75	5.000	.000	.00	1 .0
JUNCT STR	.2280					.0406	.20	3.28	3.12		.013	.00	.00	PIPE
256.500	-5.740	3.372	-2.368	409.10	29.04	13.10	10.73	.00	4.90	4.69	5.000	.000	.00	1 .0
4.757	.2268					.0371	.18	3.37	2.95	1.98	.013	.00	.00	PIPE
261.257	-4.661	3.499	-1.162	409.10	27.88	12.07	10.90	.00	4.90	4.58	5.000	.000	.00	1 .0
4.849	.2268					.0334	.16	3.50	2.75	1.98	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
266.106	-3.561	3.658	.097	409.10	26.58	10.97	11.07	.00	4.90	4.43	5.000	.000	.00	1 .0
4.184	.2268					.0299	.13	3.66	2.51	1.98	.013	.00	.00	PIPE
270.290	-2.612	3.831	1.219	409.10	25.34	9.97	11.19	.00	4.90	4.23	5.000	.000	.00	1 .0
3.575	.2268					.0269	.10	3.83	2.29	1.98	.013	.00	.00	PIPE
273.865	-1.801	4.023	2.222	409.10	24.16	9.07	11.29	.00	4.90	3.97	5.000	.000	.00	1 .0
2.993	.2268					.0244	.07	4.02	2.06	1.98	.013	.00	.00	PIPE
276.858	-1.122	4.241	3.119	409.10	23.04	8.24	11.36	.00	4.90	3.59	5.000	.000	.00	1 .0
2.384	.2268					.0225	.05	4.24	1.82	1.98	.013	.00	.00	PIPE
279.242	-.582	4.504	3.922	409.10	21.97	7.49	11.41	.00	4.90	2.99	5.000	.000	.00	1 .0
1.418	.2268					.0219	.03	4.50	1.55	1.98	.013	.00	.00	PIPE
280.660	-.260	4.895	4.635	409.10	20.94	6.81	11.45	.00	4.90	1.43	5.000	.000	.00	1 .0
2.910	.0108					.0229	.07	4.90	1.00	5.00	.013	.00	.00	PIPE
283.570	-.229	5.000	4.771	409.10	20.84	6.74	11.51	.00	4.90	.00	5.000	.000	.00	1 .0
67.590	.0108					.0242	1.64	5.00	.00	5.00	.013	.00	.00	PIPE
351.160	.500	5.939	6.439	409.10	20.84	6.74	13.18	.00	4.90	.00	5.000	.000	.00	1 .0
JUNCT STR	.0100					.0245	.12	5.94	.00		.013	.00	.00	PIPE
356.160	.550	6.178	6.728	406.50	20.70	6.66	13.38	.00	4.89	.00	5.000	.000	.00	1 .0
145.000	.0107					.0244	3.53	6.18	.00	5.00	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
501.160	2.100	8.161	10.261	406.50	20.70	6.66	16.92	.00	4.89	.00	5.000	.000	.00	1 .0
JUNCT STR	.0120					.0241	.12	8.16	.00		.013	.00	.00	PIPE
506.160	2.160	8.553	10.713	401.40	20.44	6.49	17.20	.00	4.89	.00	5.000	.000	.00	1 .0
104.500	.0107					.0238	2.48	8.55	.00	5.00	.013	.00	.00	PIPE
610.660	3.280	10.454	13.734	401.40	20.44	6.49	20.22	.00	4.89	.00	5.000	.000	.00	1 .0
319.340	.0045					.0238	7.59	10.45	.00	5.00	.013	.00	.00	PIPE
930.000	4.730	16.589	21.319	401.40	20.44	6.49	27.81	.00	4.89	.00	5.000	.000	.00	1 .0
120.000	.0045					.0238	2.85	16.59	.00	5.00	.013	.00	.00	PIPE
1050.000	5.270	18.900	24.170	401.40	20.44	6.49	30.66	.00	4.89	.00	5.000	.000	.00	1 .0
JUNCT STR	.0050					.0208	.08	18.90	.00		.013	.00	.00	PIPE
1054.000	5.290	21.830	27.120	347.80	17.71	4.87	31.99	.00	4.80	.00	5.000	.000	.00	1 .0
41.660	.0046					.0178	.74	21.83	.00	5.00	.013	.00	.00	PIPE
1095.660	5.480	22.383	27.863	347.80	17.71	4.87	32.73	.00	4.80	.00	5.000	.000	.00	1 .0
JUNCT STR	.0420					.0178	.09	22.38	.00		.013	.00	.00	PIPE
1100.660	5.690	22.267	27.957	347.70	17.71	4.87	32.83	.00	4.80	.00	5.000	.000	.00	1 .0
24.170	.1080					.0178	.43	22.27	.00	2.22	.013	.00	.00	PIPE
1124.830	8.300	20.088	28.388	347.70	17.71	4.87	33.26	.00	4.80	.00	5.000	.000	.00	1 .0
64.140	.1082					.0178	1.14	.00	.00	2.22	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1188.970	15.240	14.667	29.907	347.70	17.71	4.87	34.78	.00	4.80	.00	5.000	.000	.00	1 .0
20.877	.0740					.0178	.37	14.67	.00	2.47	.013	.00	.00	PIPE
1209.847	16.785	13.494	30.279	347.70	17.71	4.87	35.15	.00	4.80	.00	5.000	.000	.00	1 .0
HYDRAULIC JUMP														
1209.847	16.785	2.424	19.209	347.70	36.84	21.08	40.28	.00	4.80	5.00	5.000	.000	.00	1 .0
77.653	.0740					.0803	6.24	2.42	4.72	2.47	.013	.00	.00	PIPE
1287.500	22.530	2.405	24.935	347.70	37.22	21.52	46.45	.00	4.80	5.00	5.000	.000	.00	1 .0
JUNCT STR	.0720					.0816	.41	2.40	4.80		.013	.00	.00	PIPE
1292.500	22.890	2.402	25.292	347.60	37.27	21.57	46.86	.00	4.80	5.00	5.000	.000	.00	1 .0
65.970	.0741					.0834	5.50	2.40	4.81	2.47	.013	.00	.00	PIPE
1358.470	27.780	2.375	30.155	347.60	37.82	22.21	52.37	1.47	4.80	4.99	5.000	.000	.00	1 .0
101.230	.0873					.0842	8.52	3.85	4.91	2.36	.013	.00	.00	PIPE
1459.700	36.620	2.388	39.008	347.60	37.54	21.88	60.89	.36	4.80	5.00	5.000	.000	.00	1 .0
107.800	.0924					.0797	8.59	2.75	4.86	2.32	.013	.00	.00	PIPE
1567.500	46.580	2.452	49.032	347.60	36.30	20.46	69.49	.00	4.80	5.00	5.000	.000	.00	1 .0
JUNCT STR	.0920					.0788	.39	2.82	4.62		.013	.00	.00	PIPE
1572.500	47.040	2.353	49.393	334.80	36.86	21.10	70.49	.38	4.78	4.99	5.000	.000	.00	1 .0
45.000	.0924					.0799	3.60	2.73	4.82	2.27	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
1617.500	51.200	2.379	53.579	334.80	36.34	20.51	74.09	.00	4.78	4.99	5.000	.000	.00	1 .0
JUNCT STR	.1600					.0786	.39	2.72	4.72		.013	.00	.00	PIPE
1622.500	52.000	2.322	54.322	321.70	36.03	20.16	74.49	.33	4.74	4.99	5.000	.000	.00	1 .0
87.549	.0936					.0741	6.49	2.65	4.75	2.21	.013	.00	.00	PIPE
1710.049	60.193	2.407	62.600	321.70	34.40	18.38	80.98	.30	4.74	5.00	5.000	.000	.00	1 .0
55.961	.0936					.0654	3.66	2.71	4.43	2.21	.013	.00	.00	PIPE
1766.010	65.430	2.498	67.928	321.70	32.80	16.71	84.64	.00	4.74	5.00	5.000	.000	.00	1 .0
37.405	.0937					.0578	2.16	2.50	4.13	2.21	.013	.00	.00	PIPE
1803.415	68.934	2.588	71.522	321.70	31.37	15.28	86.80	.00	4.74	5.00	5.000	.000	.00	1 .0
30.273	.0937					.0511	1.55	2.59	3.86	2.21	.013	.00	.00	PIPE
1833.688	71.769	2.688	74.458	321.70	29.91	13.89	88.34	.00	4.74	4.99	5.000	.000	.00	1 .0
23.812	.0937					.0451	1.07	2.69	3.59	2.21	.013	.00	.00	PIPE
1857.500	74.000	2.794	76.794	321.70	28.51	12.62	89.42	.00	4.74	4.97	5.000	.000	.00	1 .0
JUNCT STR	.1080					.0443	.22	2.79	3.33		.013	.00	.00	PIPE
1862.500	74.540	2.652	77.192	309.10	29.23	13.26	90.46	.00	4.70	4.99	5.000	.000	.00	1 .0
24.422	.0772					.0443	1.08	2.65	3.54	2.28	.013	.00	.00	PIPE
1886.923	76.425	2.725	79.151	309.10	28.25	12.39	91.54	.00	4.70	4.98	5.000	.000	.00	1 .0
27.249	.0772					.0398	1.08	2.73	3.36	2.28	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
1914.172	78.529	2.833	81.361	309.10	26.93	11.26	92.63	.00	4.70	4.96	5.000	.000	.00	1 .0
21.663	.0772					.0352	.76	2.83	3.12	2.28	.013	.00	.00	PIPE
1935.835	80.201	2.946	83.147	309.10	25.68	10.24	93.39	.00	4.70	4.92	5.000	.000	.00	1 .0
17.592	.0772					.0311	.55	2.95	2.89	2.28	.013	.00	.00	PIPE
1953.426	81.559	3.066	84.625	309.10	24.48	9.31	93.93	.00	4.70	4.87	5.000	.000	.00	1 .0
14.480	.0772					.0275	.40	3.07	2.68	2.28	.013	.00	.00	PIPE
1967.906	82.677	3.194	85.870	309.10	23.34	8.46	94.33	.00	4.70	4.80	5.000	.000	.00	1 .0
12.012	.0772					.0244	.29	3.19	2.48	2.28	.013	.00	.00	PIPE
1979.918	83.604	3.329	86.933	309.10	22.26	7.69	94.63	.00	4.70	4.72	5.000	.000	.00	1 .0
9.990	.0772					.0217	.22	3.33	2.29	2.28	.013	.00	.00	PIPE
1989.908	84.375	3.475	87.850	309.10	21.22	6.99	94.84	.00	4.70	4.60	5.000	.000	.00	1 .0
8.286	.0772					.0194	.16	3.47	2.10	2.28	.013	.00	.00	PIPE
1998.195	85.015	3.632	88.646	309.10	20.24	6.36	95.00	.00	4.70	4.46	5.000	.000	.00	1 .0
6.805	.0772					.0174	.12	3.63	1.93	2.28	.013	.00	.00	PIPE
2005.000	85.540	3.802	89.342	309.10	19.29	5.78	95.12	.00	4.70	4.27	5.000	.000	.00	1 .0
153.531	.0171					.0160	2.46	3.80	1.75	3.74	.013	.00	.00	PIPE
2158.531	88.164	3.886	92.050	309.10	18.88	5.53	97.58	.00	4.70	4.16	5.000	.000	.00	1 .0
139.002	.0171					.0149	2.07	3.89	1.68	3.74	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

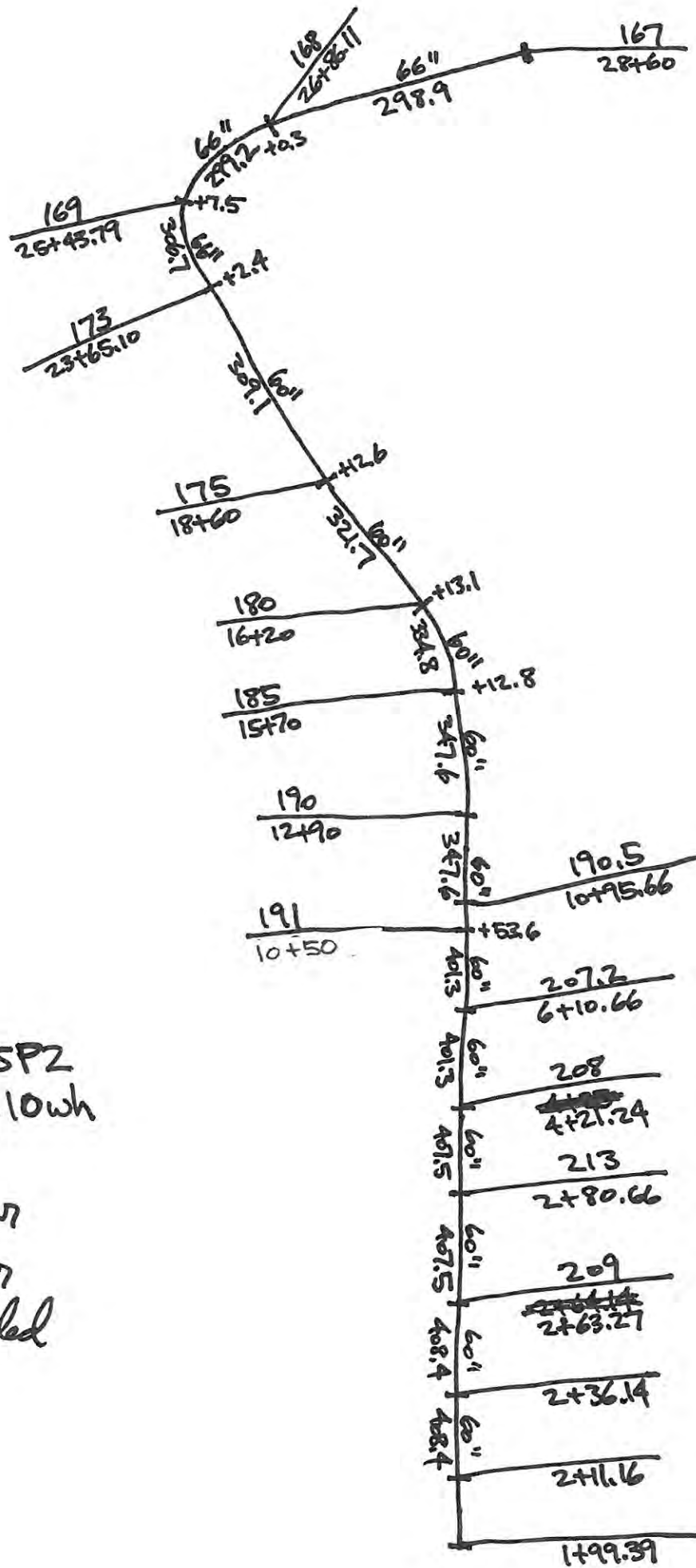
Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
2297.533	90.540	4.085	94.625	309.10	18.00	5.03	99.65	.00	4.70	3.87	5.000	.000	.00	1 .0
64.967	.0171					.0136	.88	4.09	1.50	3.74	.013	.00	.00	PIPE
2362.500	91.650	4.314	95.964	309.10	17.16	4.57	100.54	.00	4.70	3.44	5.000	.000	.00	1 .0
JUNCT STR	.1080					.0124	.06	4.31	1.32		.013	.00	.00	PIPE
2367.500	92.190	3.852	96.042	306.70	17.26	4.62	100.67	.00	4.81	5.04	5.500	.000	.00	1 .0
124.250	.0132					.0113	1.40	3.85	1.62	3.70	.013	.00	.00	PIPE
2491.750	93.830	4.021	97.851	306.70	16.48	4.22	102.07	.48	4.81	4.88	5.500	.000	.00	1 .0
49.540	.0131					.0103	.51	4.50	1.49	3.71	.013	.00	.00	PIPE
2541.290	94.480	4.153	98.633	306.70	15.93	3.94	102.58	.00	4.81	4.73	5.500	.000	.00	1 .0
JUNCT STR	.0120					.0106	.05	4.73	1.39		.013	.00	.00	PIPE
2546.290	94.540	3.840	98.380	299.20	16.89	4.43	102.81	.69	4.76	5.05	5.500	.000	.00	1 .0
83.858	.0133					.0109	.91	4.53	1.59	3.63	.013	.00	.00	PIPE
2630.148	95.651	3.989	99.640	299.20	16.21	4.08	103.72	.62	4.76	4.91	5.500	.000	.00	1 .0
53.462	.0133					.0098	.52	4.61	1.47	3.63	.013	.00	.00	PIPE
2683.610	96.360	4.176	100.536	299.20	15.46	3.71	104.25	.00	4.76	4.70	5.500	.000	.00	1 .0
JUNCT STR	.0100					.0093	.05	4.18	1.34		.013	.00	.00	PIPE
2688.610	96.410	4.162	100.572	298.90	15.50	3.73	104.30	.00	4.76	4.72	5.500	.000	.00	1 .0
94.252	.0100					.0090	.85	4.16	1.35	4.05	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Existing Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
2782.862	97.350	4.284	101.634	298.90	15.05	3.52	105.15	.00	4.76	4.57	5.500	.000	.00	1 .0
61.405	.0100					.0083	.51	4.28	1.27	4.05	.013	.00	.00	PIPE
2844.267	97.963	4.504	102.467	298.90	14.35	3.20	105.67	.00	4.76	4.24	5.500	.000	.00	1 .0
15.733	.0100					.0076	.12	4.50	1.14	4.05	.013	.00	.00	PIPE
2860.000	98.120	4.758	102.878	298.90	13.68	2.91	105.79	.00	4.76	3.76	5.500	.000	.00	1 .0

D.3



Hydrology: DPHOSP2
 Hydraulics: dphjplowh

Proposed 10-year
 w/ 3.5 Ac Harbor
 Tributary Included

PROP. 10-YR 60" HYDRAULICS
w/ Harbor Included

♀ FILE: dphjp10wh.WSW

dphjp10wh
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Program Package Serial Number: 1863
WATER SURFACE PROFILE LISTING

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Dana Point Harbor
60-inch Line L00P01

Proposed Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
199.390	-12.220	17.260	5.040	408.50	8.17	1.04	6.08	.00	3.73	10.00	5.000	10.000	.00	0 .0
11.770	.0518					.0034	.04	17.26	.64	1.60	.015	-.02	.00	BOX
211.160	-11.610	16.690	5.080	408.50	8.17	1.04	6.12	.00	3.73	10.00	5.000	10.000	.00	0 .0
TRANS STR	.0500					.0181	.45	16.69	.64		.015	.00	.00	BOX
236.140	-10.360	11.345	.985	408.50	20.80	6.72	7.71	.00	4.89	.00	5.000	.000	.00	1 .0
.621	.2351					.0246	.02	11.34	.00	1.96	.013	.00	.00	PIPE
236.761	-10.214	11.210	.996	408.50	20.80	6.72	7.72	.00	4.89	.00	5.000	.000	.00	1 .0
HYDRAULIC JUMP														
236.761	-10.214	3.014	-7.200	408.50	33.02	16.93	9.73	.00	4.89	4.89	5.000	.000	.00	1 .0
5.900	.2351					.0514	.30	3.01	3.66	1.96	.013	.00	.00	PIPE
242.661	-8.827	3.107	-5.720	408.50	31.86	15.76	10.04	.00	4.89	4.85	5.000	.000	.00	1 .0
6.898	.2351					.0463	.32	3.11	3.45	1.96	.013	.00	.00	PIPE
249.559	-7.205	3.237	-3.968	408.50	30.37	14.33	10.36	.00	4.89	4.78	5.000	.000	.00	1 .0
5.998	.2351					.0411	.25	3.24	3.19	1.96	.013	.00	.00	PIPE
255.557	-5.796	3.376	-2.420	408.50	28.96	13.02	10.60	.00	4.89	4.68	5.000	.000	.00	1 .0
5.213	.2351					.0366	.19	3.38	2.94	1.96	.013	.00	.00	PIPE
260.770	-4.570	3.525	-1.045	408.50	27.61	11.84	10.79	.00	4.89	4.56	5.000	.000	.00	1 .0
JUNCT STR	.1860					.0331	.17	3.52	2.70		.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Proposed Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
423.740	1.270	7.322	8.592	401.40	20.44	6.49	15.08	.00	4.89	.00	5.000	.000	.00	1 .0
186.920	.0108					.0238	4.44	7.32	.00	5.00	.013	.00	.00	PIPE
610.660	3.280	10.290	13.570	401.40	20.44	6.49	20.06	.00	4.89	.00	5.000	.000	.00	1 .0
439.340	.0045					.0238	10.44	10.29	.00	5.00	.013	.00	.00	PIPE
1050.000	5.270	18.736	24.006	401.40	20.44	6.49	30.50	.00	4.89	.00	5.000	.000	.00	1 .0
JUNCT STR	.0050					.0208	.08	18.74	.00		.013	.00	.00	PIPE
1054.000	5.290	21.666	26.956	347.80	17.71	4.87	31.83	.00	4.80	.00	5.000	.000	.00	1 .0
41.660	.0046					.0178	.74	21.67	.00	5.00	.013	.00	.00	PIPE
1095.660	5.480	22.219	27.699	347.80	17.71	4.87	32.57	.00	4.80	.00	5.000	.000	.00	1 .0
JUNCT STR	.0420					.0178	.09	22.22	.00		.013	.00	.00	PIPE
1100.660	5.690	22.104	27.794	347.70	17.71	4.87	32.66	.00	4.80	.00	5.000	.000	.00	1 .0
24.170	.1080					.0178	.43	22.10	.00	2.22	.013	.00	.00	PIPE
1124.830	8.300	19.925	28.225	347.70	17.71	4.87	33.09	.00	4.80	.00	5.000	.000	.00	1 .0
64.140	.1082					.0178	1.14	.00	.00	2.22	.013	.00	.00	PIPE
1188.970	15.240	14.504	29.744	347.70	17.71	4.87	34.61	.00	4.80	.00	5.000	.000	.00	1 .0
18.110	.0740					.0178	.32	14.50	.00	2.47	.013	.00	.00	PIPE
1207.080	16.580	13.486	30.066	347.70	17.71	4.87	34.94	.00	4.80	.00	5.000	.000	.00	1 .0

HYDRAULIC JUMP

Dana Point Harbor
60-inch Line L00P01

Proposed Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1207.080	16.580	2.427	19.007	347.70	36.79	21.02	40.02	.00	4.80	5.00	5.000	.000	.00	1 .0
80.420	.0740					.0802	6.45	2.43	4.71	2.47	.013	.00	.00	PIPE
1287.500	22.530	2.405	24.935	347.70	37.22	21.52	46.45	.00	4.80	5.00	5.000	.000	.00	1 .0
JUNCT STR	.0720					.0816	.41	2.40	4.80		.013	.00	.00	PIPE
1292.500	22.890	2.402	25.292	347.60	37.27	21.57	46.86	.00	4.80	5.00	5.000	.000	.00	1 .0
65.970	.0741					.0834	5.50	2.40	4.81	2.47	.013	.00	.00	PIPE
1358.470	27.780	2.375	30.155	347.60	37.82	22.21	52.37	1.47	4.80	4.99	5.000	.000	.00	1 .0
101.230	.0873					.0842	8.52	3.85	4.91	2.36	.013	.00	.00	PIPE
1459.700	36.620	2.388	39.008	347.60	37.54	21.88	60.89	.36	4.80	5.00	5.000	.000	.00	1 .0
107.800	.0924					.0797	8.59	2.75	4.86	2.32	.013	.00	.00	PIPE
1567.500	46.580	2.452	49.032	347.60	36.30	20.46	69.49	.00	4.80	5.00	5.000	.000	.00	1 .0
JUNCT STR	.0920					.0788	.39	2.82	4.62		.013	.00	.00	PIPE
1572.500	47.040	2.353	49.393	334.80	36.86	21.10	70.49	.38	4.78	4.99	5.000	.000	.00	1 .0
45.000	.0924					.0799	3.60	2.73	4.82	2.27	.013	.00	.00	PIPE
1617.500	51.200	2.379	53.579	334.80	36.34	20.51	74.09	.00	4.78	4.99	5.000	.000	.00	1 .0
JUNCT STR	.1600					.0786	.39	2.72	4.72		.013	.00	.00	PIPE
1622.500	52.000	2.322	54.322	321.70	36.03	20.16	74.49	.33	4.74	4.99	5.000	.000	.00	1 .0
87.549	.0936					.0741	6.49	2.65	4.75	2.21	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Proposed Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1710.049	60.193	2.407	62.600	321.70	34.40	18.38	80.98	.30	4.74	5.00	5.000	.000	.00	1 .0
55.961	.0936					.0654	3.66	2.71	4.43	2.21	.013	.00	.00	PIPE
1766.010	65.430	2.498	67.928	321.70	32.80	16.71	84.64	.00	4.74	5.00	5.000	.000	.00	1 .0
37.405	.0937					.0578	2.16	2.50	4.13	2.21	.013	.00	.00	PIPE
1803.415	68.934	2.588	71.522	321.70	31.37	15.28	86.80	.00	4.74	5.00	5.000	.000	.00	1 .0
30.273	.0937					.0511	1.55	2.59	3.86	2.21	.013	.00	.00	PIPE
1833.688	71.769	2.688	74.458	321.70	29.91	13.89	88.34	.00	4.74	4.99	5.000	.000	.00	1 .0
23.812	.0937					.0451	1.07	2.69	3.59	2.21	.013	.00	.00	PIPE
1857.500	74.000	2.794	76.794	321.70	28.51	12.62	89.42	.00	4.74	4.97	5.000	.000	.00	1 .0
JUNCT STR	.1080					.0443	.22	2.79	3.33		.013	.00	.00	PIPE
1862.500	74.540	2.652	77.192	309.10	29.23	13.26	90.46	.00	4.70	4.99	5.000	.000	.00	1 .0
24.422	.0772					.0443	1.08	2.65	3.54	2.28	.013	.00	.00	PIPE
1886.923	76.425	2.725	79.151	309.10	28.25	12.39	91.54	.00	4.70	4.98	5.000	.000	.00	1 .0
27.249	.0772					.0398	1.08	2.73	3.36	2.28	.013	.00	.00	PIPE
1914.172	78.529	2.833	81.361	309.10	26.93	11.26	92.63	.00	4.70	4.96	5.000	.000	.00	1 .0
21.663	.0772					.0352	.76	2.83	3.12	2.28	.013	.00	.00	PIPE
1935.835	80.201	2.946	83.147	309.10	25.68	10.24	93.39	.00	4.70	4.92	5.000	.000	.00	1 .0
17.592	.0772					.0311	.55	2.95	2.89	2.28	.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Proposed Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1953.426	81.559	3.066	84.625	309.10	24.48	9.31	93.93	.00	4.70	4.87	5.000	.000	.00	1 .0
14.480	.0772					.0275	.40	3.07	2.68	2.28	.013	.00	.00	PIPE
1967.906	82.677	3.194	85.870	309.10	23.34	8.46	94.33	.00	4.70	4.80	5.000	.000	.00	1 .0
12.012	.0772					.0244	.29	3.19	2.48	2.28	.013	.00	.00	PIPE
1979.918	83.604	3.329	86.933	309.10	22.26	7.69	94.63	.00	4.70	4.72	5.000	.000	.00	1 .0
9.990	.0772					.0217	.22	3.33	2.29	2.28	.013	.00	.00	PIPE
1989.908	84.375	3.475	87.850	309.10	21.22	6.99	94.84	.00	4.70	4.60	5.000	.000	.00	1 .0
8.286	.0772					.0194	.16	3.47	2.10	2.28	.013	.00	.00	PIPE
1998.195	85.015	3.632	88.646	309.10	20.24	6.36	95.00	.00	4.70	4.46	5.000	.000	.00	1 .0
6.805	.0772					.0174	.12	3.63	1.93	2.28	.013	.00	.00	PIPE
2005.000	85.540	3.802	89.342	309.10	19.29	5.78	95.12	.00	4.70	4.27	5.000	.000	.00	1 .0
153.531	.0171					.0160	2.46	3.80	1.75	3.74	.013	.00	.00	PIPE
2158.531	88.164	3.886	92.050	309.10	18.88	5.53	97.58	.00	4.70	4.16	5.000	.000	.00	1 .0
139.002	.0171					.0149	2.07	3.89	1.68	3.74	.013	.00	.00	PIPE
2297.533	90.540	4.085	94.625	309.10	18.00	5.03	99.65	.00	4.70	3.87	5.000	.000	.00	1 .0
64.967	.0171					.0136	.88	4.09	1.50	3.74	.013	.00	.00	PIPE
2362.500	91.650	4.314	95.964	309.10	17.16	4.57	100.54	.00	4.70	3.44	5.000	.000	.00	1 .0
JUNCT STR	.1080					.0124	.06	4.31	1.32		.013	.00	.00	PIPE

Dana Point Harbor
60-inch Line L00P01

Proposed Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
2367.500	92.190	3.852	96.042	306.70	17.26	4.62	100.67	.00	4.81	5.04	5.500	.000	.00	1 .0
124.250	.0132					.0113	1.40	3.85	1.62	3.70	.013	.00	.00	PIPE
2491.750	93.830	4.021	97.851	306.70	16.48	4.22	102.07	.48	4.81	4.88	5.500	.000	.00	1 .0
49.540	.0131					.0103	.51	4.50	1.49	3.71	.013	.00	.00	PIPE
2541.290	94.480	4.153	98.633	306.70	15.93	3.94	102.58	.00	4.81	4.73	5.500	.000	.00	1 .0
JUNCT STR	.0120					.0106	.05	4.73	1.39		.013	.00	.00	PIPE
2546.290	94.540	3.840	98.380	299.20	16.89	4.43	102.81	.69	4.76	5.05	5.500	.000	.00	1 .0
83.858	.0133					.0109	.91	4.53	1.59	3.63	.013	.00	.00	PIPE
2630.148	95.651	3.989	99.640	299.20	16.21	4.08	103.72	.62	4.76	4.91	5.500	.000	.00	1 .0
53.462	.0133					.0098	.52	4.61	1.47	3.63	.013	.00	.00	PIPE
2683.610	96.360	4.176	100.536	299.20	15.46	3.71	104.25	.00	4.76	4.70	5.500	.000	.00	1 .0
JUNCT STR	.0100					.0093	.05	4.18	1.34		.013	.00	.00	PIPE
2688.610	96.410	4.162	100.572	298.90	15.50	3.73	104.30	.00	4.76	4.72	5.500	.000	.00	1 .0
94.252	.0100					.0090	.85	4.16	1.35	4.05	.013	.00	.00	PIPE
2782.862	97.350	4.284	101.634	298.90	15.05	3.52	105.15	.00	4.76	4.57	5.500	.000	.00	1 .0
61.405	.0100					.0083	.51	4.28	1.27	4.05	.013	.00	.00	PIPE
2844.267	97.963	4.504	102.467	298.90	14.35	3.20	105.67	.00	4.76	4.24	5.500	.000	.00	1 .0
15.733	.0100					.0076	.12	4.50	1.14	4.05	.013	.00	.00	PIPE

Dana Point Harbor
 60-inch Line L00P01

Proposed Condition Hydraulic Model

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
2860.000	98.120	4.758	102.878	298.90	13.68	2.91	105.79	.00	4.76	3.76	5.500	.000	.00	1 .0
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